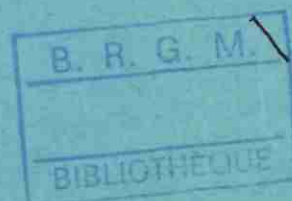
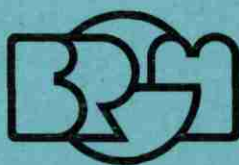


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BUREAU DE RECHERCHES GÉOLOGIQUES ET MINIÈRES

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**CATALOGUE D'ABAQUES POUR L'INTERPRÉTATION
DE POMPAGES EN NAPPE LIBRE**



Département hydrogéologie

79 SGN 682 HYD

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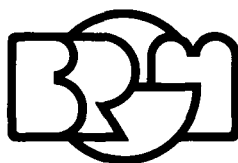
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CATALOGUE D'ABAQUES POUR L'INTERPRÉTATION DE POMPAGES EN NAPPE LIBRE

par

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RESUME

Présentation d'un catalogue de fonctions calculées pour une grande variété de dispositifs de captage et d'observation pénétrant partiellement une nappe libre anisotrope.

Les calculs ont utilisé les formules mises au point en 1975 par Boulton et Streltsova pour traiter des nappes captives, semi-captives ou libres. Seul le cas de la nappe libre, selon la conception de Neuman (1974) est présenté ici.

Ces fonctions, et les abaques qui devront être construits, rendent possible une meilleure détermination des paramètres hydrodynamiques caractérisant les nappes libres (T , K' , S , S'). Lorsque les puits et piézomètres ont des caractéristiques non prévues dans le présent catalogue, on peut obtenir des déterminations approchées de ces paramètres de façon à encadrer les valeurs réelles.

Lors de la conception d'une opération de pompage, on peut, moyennant des hypothèses sur l'ordre de grandeur des paramètres cherchés, déterminer le dispositif le plus sensible à de faibles variations de ces paramètres.

Ce rapport est édité dans le cadre des travaux propres du département hydrogéologique.

Dans une précédente note (R. Degallier, 1976) nous présentions des abaques (Stallman, 1965) destinées à montrer l'importance que peut avoir, tout spécialement dans des nappes libres, la pénétration incomplète des puits de pompage ou des piézomètres de mesure du niveau.

Mais il ne suffisait pas de mettre en garde les hydrogéologues contre une utilisation abusive de fonctions trop simplistes, encore fallait-il leur donner la possibilité de faire mieux.

Le présent catalogue répond, au moins partiellement, à ce souci, ce qui rend possible maintenant:

- une meilleure détermination des paramètres hydrauliques de puits ou de systèmes de puits et piézomètres où la disposition des orifices et crépines correspond aux fonctions disponibles.

- lorsque la disposition des ouvertures des puits et piézomètres correspond mal aux fonctions disponibles une détermination approchée de ces paramètres. Dans ce cas la fourchette de précision peut être donnée si l'on encadre la situation réelle par les fonctions calculées pour les dispositifs les plus proches.

- lors de la conception d'un dispositif de pompage, une évaluation de sa sensibilité à la disposition des ouvertures des puits et piézomètres, à la distance entre ces derniers, aux contrastes des paramètres d'écoulement vertical et horizontal.

La formule la plus employée jusqu'ici pour traiter les nappes libres était celle de Boulton (1955, 1963) mais elle n'était valable, dans une nappe homogène isotrope pénétrée complètement par le puits de pompage et par le piézomètre, que comme une approximation. Le débit retardé venant de la surface

de la nappe était introduit au moyen d'un coefficient empirique.

Les erreurs auxquelles pouvait conduire cette formule ont été mises en évidence (Boulton, 1973 ; Streltsova, 1972, 1973) et apparaissent dans le schéma ci-dessous (Figure 1) pour le cas d'une pénétration complète et en ne considérant que la partie de la courbe de Boulton sous l'influence prépondérante du débit dit " retardé " provenant de la surface libre de la nappe (courbe type B, selon Boulton).

On voit que pour de faibles valeurs de r/B la formule de Boulton surestime très fortement les rabattements. Pour $r/B = 0.1$ par exemple, les rabattements calculés sont plus du double de ce qu'ils devraient être. En cas de pénétration partielle du piézomètre seulement, et, a fortiori, du puits de pompage, les écarts peuvent augmenter bien plus fortement.

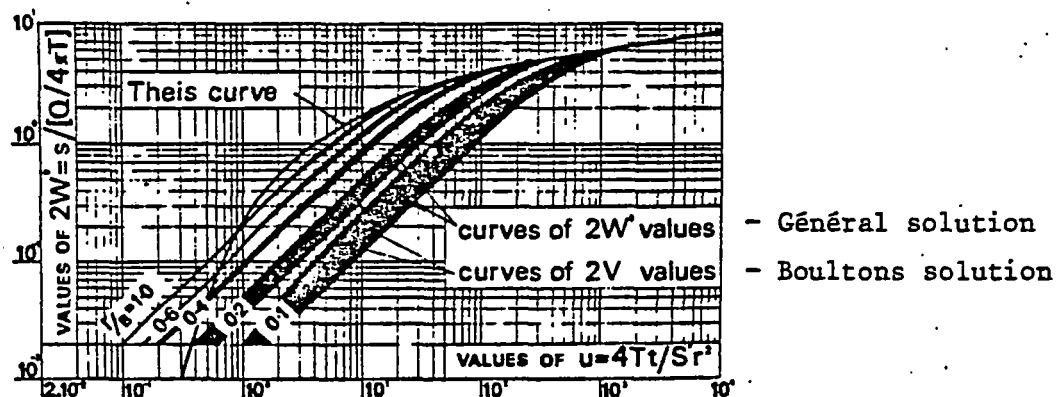
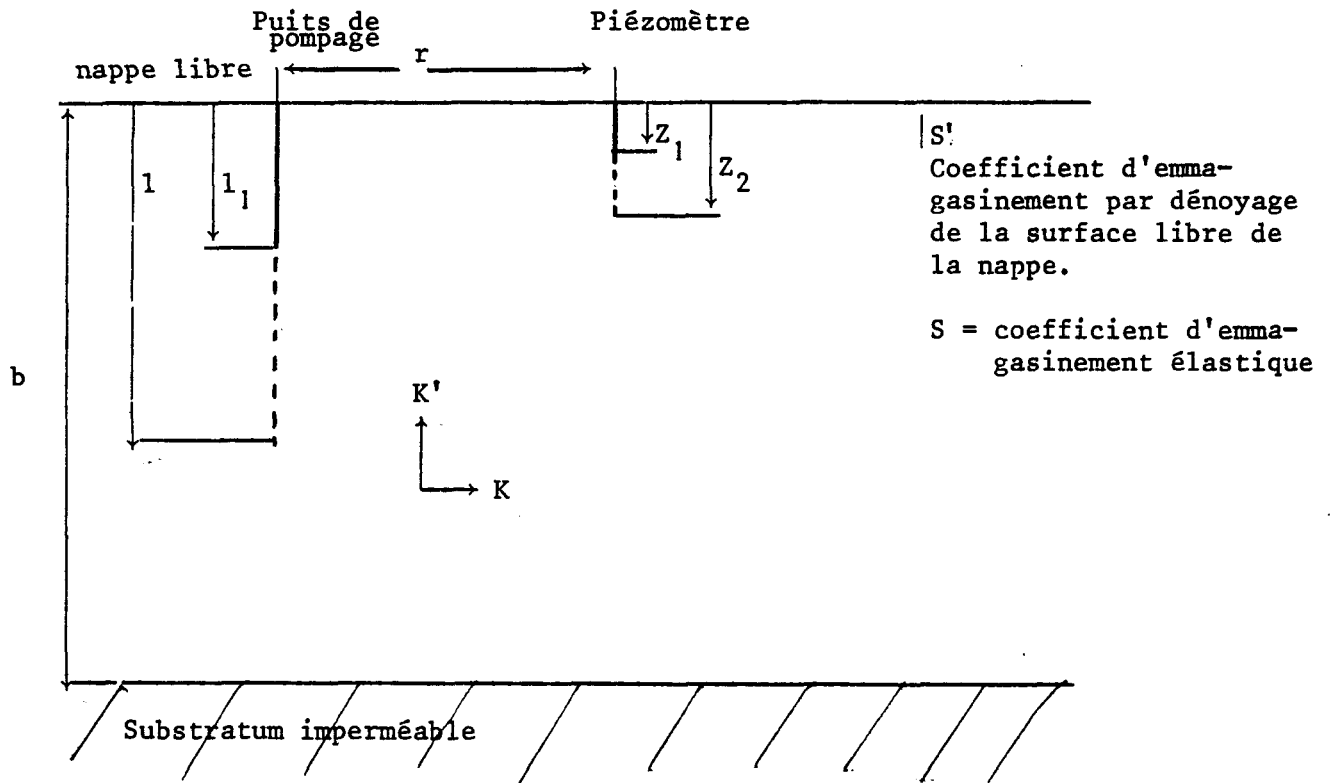


Fig. 1. Comparison of W^* and V functions.

Les formules utilisées ici pour le calcul des abaques sont celles qui ont été mises au point plus récemment par Boulton et Streltsova (1975) pour le cas traité vers la même époque par Neuman (1974) d'une nappe libre anisotrope pénétrée partiellement ou totalement par le puits de pompage et par le piézomètre . Tous les coefficients y sont explicités en termes de paramètres hydrauliques, définis selon le schéma suivant: (figure 2) :

FIGURE 2 - DISPOSITIF DE POMPAGE



Les 10 paramètres de cette figure et les deux variables temps et rabattement se combinent en 8 grandeurs sans dimension:

$L = 1 - 1/b$	Cote réduite de la base des crépines du puits
$L_1 = 1 - 1_1/b$	Cote réduite du sommet des crépines du puits
$Z_1 = 1 - z_1/b$	Cote réduite de la base des crépines du piézomètre
$Z_2 = 1 - z_2/b$	Cote réduite du sommet des crépines du piézomètre
$\nu = 1/\sigma = S'/S$	Contraste des capacités en eau ou des coefficients d'emmagasinement élastique et de la surface libre de la nappe
$\rho = \sqrt{\beta} = \frac{r}{b} \sqrt{\frac{K'}{K}}$	Coefficient d'anisotropie
$\tau = \rho^2 \theta / 4 = Tt / 2^2 S$	Temps réduit
$F = 4\pi Ts(L_1 - L) / Q$	Rabattement réduit

La transmissivité T est un paramètre auxiliaire non nécessaire et qui peut remplacer Kb.

Les notations θ, β, σ ont été utilisées notamment par Neuman (1974).

La formule tabulée est donc la suivante:

$$F = \int_0^\infty x J_0(\rho x) \left[\psi_0(x) + \sum_{m=1}^\infty \psi_m(x) \right] dx \quad (1)$$

dans laquelle :

$$\psi_0(x) = \frac{\{1 - \exp[-\tau(x^2 - \beta_0^2)]\} [\sinh(\beta_0 L_1) \sinh(\beta_0 L)] [\sinh(\beta_0 Z_2) - \sinh(\beta_0 Z_1)]}{(Z_2 - Z_1) \beta_0 (x^2 - \beta_0^2) \cosh \beta_0 \{[1 - \nu(x^2 - \beta_0^2)] \sinh \beta_0 + (1 + 2\nu) \beta_0 \cosh \beta_0\}} \quad (2)$$

$$\psi_m(v) = \frac{\{1 - \exp[-\tau(x^2 + \beta_m^2)]\} [\sin(\beta_m L_1) - \sin(\beta_m L)] [\sin(\beta_m Z_2) - \sin(\beta_m Z)]}{(Z_2 - Z_1) \beta_m (x^2 + \beta_m^2) \cos \beta_m \{[1 - \nu(x^2 + \beta_m^2)] \sin \beta_m + (1 + 2\nu) \beta_m \cos \beta_m\}} \quad (3)$$

β_0 est la racine positive de

$$\beta_0 \sinh \beta_0 - \nu (x^2 - \beta_0^2) \cosh \beta_0 = 0 \quad (4)$$

pour $\beta_0^2 < x^2$

β_m est la $m^{\text{ième}}$ racine positive de

$$\beta_m \sin \beta_m + \nu (x^2 + \beta_m^2) \cos \beta_m = 0 \quad (5)$$

pour $(2m - 1) \pi / 2 < \beta_m < m\pi$

J_0 est la fonction de Bessel de première espèce et d'ordre zéro.

Le nombre de combinaisons des valeurs possibles des 7 paramètres de la fonction F était tel -- une multiple infinité -- qu'un choix était nécessaire, pour chaque paramètre, d'un nombre de valeurs limité dans un intervalle de variation: atteignant les cas extrêmes auxquels l'on peut s'attendre sur le terrain.

Après de nombreux essais et travaux préparatoires destinés à éviter le calcul d'abaques peu différents les uns des autres, les compromis suivants furent adoptés:

- les paramètres hydrodynamiques croissent en progression géométrique:

- . $\tau = Tt/r^2S$ de 10^{-1} à 10^4
- . $\sigma = S/S' = 1/v$ de 10^{-3} à 10^{-1}
- . $\beta = K'r^2/Kb^2$ de 10^{-7} à 10

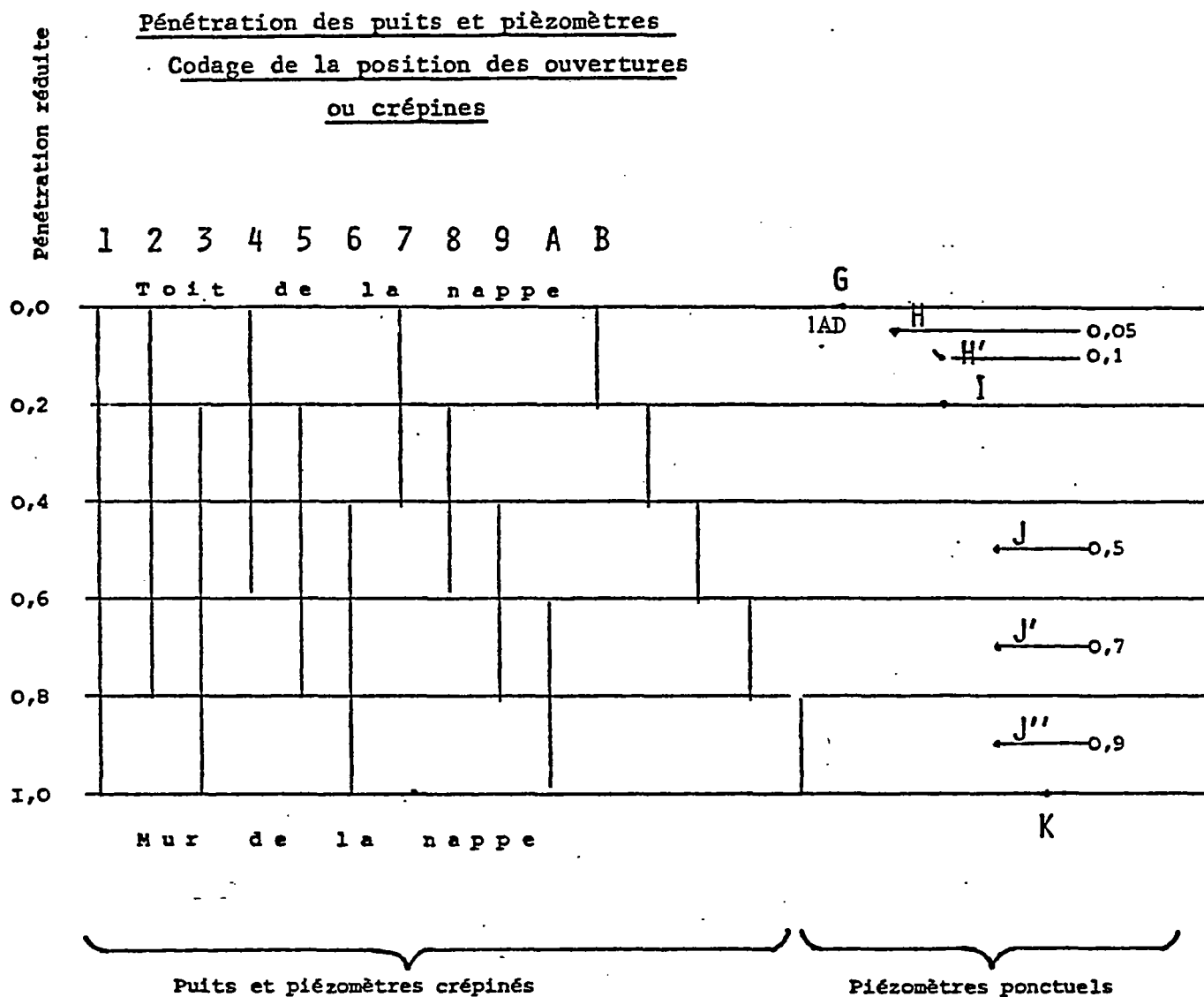
- les paramètres géométriques sont définis par les codes de la Figure 3.

Au départ on a pensé calculer des abaques pour les 15 dispositifs de puits 1 à F et les 20 dispositifs de piézomètres 1 à K, selon le schéma de la Figure 3, ce qui eût conduit à 300 abaques pour ne tenir compte que de la disposition géométrique des systèmes de pompage et de mesure. Chaque abaque devait contenir une famille de courbes différant par leur paramètre $\beta = K'r^2/Kb^2$ dont en général 9 valeurs étaient retenues.

Ensuite un tel catalogue de 300 abaques devait être calculé pour un certain nombre de valeurs du paramètre $\sigma = S/S'$.

Pour ce paramètre σ , cinq valeurs étaient retenues, considérant que la fourchette des valeurs usuelles s'ouvrait de 10^{-3} à 10^{-1} , ce qui correspond à des valeurs de S comprises entre 10^{-4} et 10^{-3} et de S' entre 10^{-2} et 10^{-1} .

FIGURE 3



Exemple: Dans une nappe de 100 m d'épaisseur un puits crépiné de 40 à 100 m sous la limite supérieure sera noté " 6 6 " s'il n'y a pas de piézomètre ou si le piézomètre est ouvert aux mêmes profondeurs que le puits. Si le piézomètre est ouvert jusqu'à 20 m sous le toit de la nappe on aura le code " 6 B ".

Ceci eût conduit à un catalogue peu maniable de 1500 abaques de 9 courbes. Finalement on ne retint que 69 dispositifs de puits et piézomètres, ce qui réduisit à 345 le nombre d'abaques. Les dispositifs retenus sont ceux du Tableau 1 ci-dessous, signalés aussi Figure 3 par les codes des piézomètres associés à chaque forage (chiffre à droite du figuré de la crépine du puits), ainsi que par les codes des forages associés à chaque position de piézomètre (chiffre à gauche du figuré de l'ouverture du piézomètre).

Les fonctions du catalogue ci-annexé sont classées par valeurs croissantes du " code de pénétration " du dispositif pour lequel elles ont été calculées, puis dans chaque tableau par valeurs croissantes de $\sigma = S/S'$. Chaque colonne correspond à une valeur particulière de $\beta = K'2^2/Kb^2$ et donnera lieu au tracé d'une courbe de F en fonction de $\tau = Tt/2^2S$.

TABLEAU 1

Code des fonctions disponibles

PUITS	PIEZOMETRES
1	1467ABDFGHIJK
4	1467BDF
6	1467BDF
7	167ADJK
A	147ABCDGHI
B	1467ABCDF
C	CD
D	1467ABCDF
E	AC
F	17ABEF

Ce catalogue de fonctions rend maintenant possible à chacun de tracer les abaques correspondant au dispositif dont il veut interpréter les mesures.

Ces fonctions sont toutes établies dans l'hypothèse d'un débit constant. Ainsi, les abaques peuvent être utilisés directement et les paramètres déterminés à partir du décalage des échelles des abscisses et des ordonnées des courbes théoriques et expérimentales, après avoir obtenu leur meilleure coïncidence.

Dans le cas où le pourcentage de pénétration du puits de pompage $L_1 - L$ ne correspond pas exactement à celui de l'abaque, les rabattements devront être corrigés proportionnellement, sachant que le rabattement minimal est obtenu avec la pénétration maximale codée " 1 ". Par exemple, si le puits est crépiné de 0.43 à 0.58 et que l'on utilise l'abaque D prévu pour un puits de 0.4 à 0.6, les rabattements mesurés seront plus forts que ce qui conviendrait et devront donc être divisés $(0,6 - 0,4)/(0,58 - 0,43)$.

Lorsque le débit n'a pas été constant pendant la durée du pompage, ou que l'on veut tirer parti de pompages intermittents pendant une large période, ou encore qu'un fort effet de capacité se fait sentir dans le puits, l'effet de tous les paliers de débit devront être additionnés, par exemple selon des procédés présentés par ailleurs (R.Degallier, 1978, 1979), afin d'obtenir les abaques de l'évolution piézométrique correspondante.

Le dessin des abaques $F(\tau, \beta)$ de toutes les tables ci-annexées fera l'objet d'un fascicule complémentaire. Il pourra être utilisé avec avantage pour l'interprétation directe de pompages à débit constant, ou lors de la conception d'une opération de pompage pour l'évaluation de la sensibilité à la distance entre puits et piézomètres.

D'autres fascicules d'abaques sont aussi envisagés pour des abaques $F(\tau, L)$ et $F(\tau, Z)$ pour l'étude de la sensibilité à la position des crépines et ouvertures des puits et piézomètres.

Une telle étude est particulièrement indiquée lorsque les paramètres doivent être déterminés de façon très sûre car souvent il arrive que des combinaisons différentes de paramètres conduisent à des courbes semblables. Il y a lieu alors de construire des piézomètres dans des situations où ils peuvent lever des ambiguïtés ou indéterminations.

Enfin d'autres catalogues de fonctions devront être calculés pour que d'autres types de nappes puissent être traitées avec la même rigueur en cas de pénétration partielle des ouvrages, notamment les nappes totalement captives, ou qui peuvent être considérées comme telles pendant la durée d'une opération de pompage, et surtout les nappes semi-captives, vraisemblablement les plus nombreuses.

CONCLUSION

Les méthodes et formules disponibles jusqu'ici avaient de nombreuses limitations. Quand on le pouvait, on cherchait à s'affranchir des effets d'anisotropie du terrain, de pénétration partielle des ouvrages ou de la nature non captive de la nappe, soit en plaçant les piézomètres loin du puits de pompage, soit en augmentant la durée de ce pompage. On pouvait alors appliquer des méthodes classiques avec rigueur, à condition d'avoir prédit avec succès l'ordre de grandeur des paramètres que l'on cherchait à déterminer.

Mais le plus souvent la durée du pompage est limitée par des exigences techniques ou économiques, ou par des phénomènes naturels tels que la pluie; souvent aussi les pompes font partie de procédures standardisées qui ne sont pas paramétrées en fonction de la constante de temps des systèmes à étudier. Comme on ne connaissait pas la portée des libertés que l'on prenait à l'égard des limitations d'application des méthodes disponibles, on pouvait admettre que les résultats obtenus étaient les moins mauvais possibles.

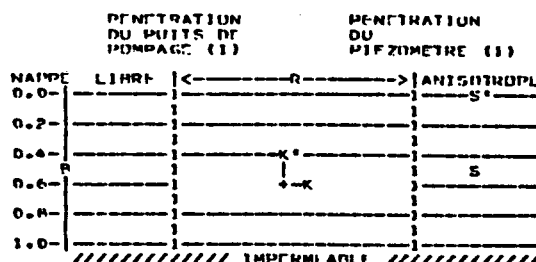
Mais maintenant qu'on dispose de techniques de calcul des écoulements dans les situations les plus variées, une telle attitude n'est plus justifiée.

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ANNEXE

ADAPTE POUR L'INTERPRETATION DE POMPAGES EN NAIRT LIGRE ANISOTROPE.
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE DOULTIN - STRELLISWA



LOG S/S' = -3.0

LOG K'R2/KR2	-7.0	-6.5	-6.0	-5.5	-5.0	-4.5	-4.0	-3.5	-3.0	-2.5	-2.0	
TT/R2S	R A D A T T E M E N T S						R E D U I T S					
1.000E-01	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	
2.154E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	
4.642E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	
1.000E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	
2.154E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	
4.642E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	
1.000E+01	3.121E+00	3.120E+00	3.120E+00	3.118E+00	3.114E+00	3.104E+00	3.087E+00	3.042E+00	2.968E+00	2.830E+00	2.605E+00	
2.154E+01	3.871E+00	3.870E+00	3.869E+00	3.866E+00	3.851E+00	3.840E+00	3.738E+00	3.619E+00	3.407E+00	3.032E+00	2.500E+00	
4.642E+01	4.629E+00	4.627E+00	4.625E+00	4.617E+00	4.604E+00	4.574E+00	4.514E+00	4.412E+00	4.227E+00	3.894E+00	3.315E+00	
1.000E+02	5.388E+00	5.387E+00	5.382E+00	5.371E+00	5.346E+00	5.298E+00	5.209E+00	5.050E+00	4.765E+00	4.259E+00	3.436E+00	
2.154E+02	6.150E+00	6.146E+00	6.138E+00	6.118E+00	6.079E+00	6.005E+00	5.870E+00	5.629E+00	5.170E+00	4.460E+00	3.402E+00	
4.642E+02	6.911E+00	6.904E+00	6.889E+00	6.857E+00	6.797E+00	6.685E+00	6.482E+00	6.121E+00	5.484E+00	4.522E+00	3.476E+00	
1.000E+03	7.671E+00	7.659E+00	7.634E+00	7.584E+00	7.492E+00	7.324E+00	7.023E+00	6.486E+00	5.600E+00	4.537E+00	3.503E+00	
2.154E+03	8.427E+00	8.407E+00	8.368E+00	8.292E+00	8.154E+00	7.904E+00	7.457E+00	6.680E+00	5.638E+00	4.561E+00	3.561E+00	
4.642E+03	9.179E+00	9.148E+00	9.088E+00	8.973E+00	8.767E+00	8.397E+00	7.784E+00	6.752E+00	5.657E+00	4.600E+00	3.677E+00	
1.000E+04	9.924E+00	9.874E+00	9.773E+00	9.614E+00	9.309E+00	8.763E+00	7.868E+00	6.771E+00	5.695E+00	4.704E+00	3.877E+00	
2.154E+04	1.067E+01	1.059E+01	1.046E+01	1.020E+01	9.750E+00	9.048E+00	7.900E+00	6.801E+00	5.771E+00	4.848E+00	4.061E+00	
4.642E+04	1.142E+01	1.130E+01	1.109E+01	1.072E+01	1.005E+01	9.076E+00	7.923E+00	6.861E+00	5.916E+00	5.089E+00	4.290E+00	
1.000E+05	1.207E+01	1.187E+01	1.157E+01	1.104E+01	1.016E+01	9.059E+00	7.969E+00	6.973E+00	6.145E+00	5.447E+00	4.655E+00	
2.154E+05	1.277E+01	1.208E+01	1.173E+01	1.113E+01	1.019E+01	9.093E+00	8.055E+00	7.188E+00	6.545E+00	6.255E+00	6.197E+00	

LOG S/S' = -3.0

LOG K'R2/KR2	-1.5	-1.0	-0.5	0.0	0.5	1.0	1.5	2.0	2.5	3.0	
TT/R2S	R A D A T T E M E N T S					R E D U I T S					
1.000E-01	2.350E-02	2.241E-02	2.049E-02	1.703E-02	1.095E-02	3.065E-03	9.549E-05	0.0	7.758E-04	0.0	
2.154E-01	1.678E-01	1.456E-01	1.277E-01	9.583E-02	4.409E-02	6.001E-03	1.035E-04	0.0	1.449E-04	0.0	
4.642E-01	4.624E-01	4.211E-01	3.477E-01	2.204E-01	6.871E-02	6.334E-03	1.118E-04	0.0	1.251E-07	0.0	
1.000E+00	9.023E-01	7.919E-01	5.943E-01	3.004E-01	7.242E-02	6.551E-03	1.303E-04	0.0	9.549E-09	0.0	
2.154E+00	1.380E+00	1.155E+00	7.622E-01	3.182E-01	7.343E-02	7.075E-03	1.745E-04	7.020E-08	1.543E-07	0.0	
4.642E+00	1.842E+00	1.417E+00	8.160E-01	3.212E-01	7.595E-02	6.081E-03	2.905E-04	1.507E-06	4.470E-06	0.0	
1.000E+01	2.197E+00	1.533E+00	8.238E-01	2.263E-01	1.052E-01	1.052E-02	1.440E-04	1.005E-07	1.256E-07	0.0	
2.154E+01	2.790E+00	1.554E+00	8.309E-01	3.374E-01	9.240E-02	6.455E-02	2.045E-03	933E-06	2.000E-05	3.743E-06	
4.642E+01	3.450E+00	1.564E+00	8.457E-01	3.612E-01	1.142E-01	3.275E-02	6.877E-03	2.446E-03	1.328E-03	4.063E-04	
1.000E+02	4.261E+00	1.540E+00	8.775E-01	4.121E-01	1.705E-01	8.079E-02	4.452E-02	3.142E-02	2.696E-02	2.551E-02	
2.154E+02	5.274E+00	1.614E+00	9.446E-01	5.199E-01	3.004E-01	2.701E-01	1.857E-01	1.740E-01	1.702E-01	1.644E-01	
4.642E+02	6.509E+00	1.605E+00	1.003E+00	7.385E-01	5.903E-01	5.283E-01	5.222E-01	5.172E-01	5.154E-01	5.151E-01	
1.000E+03	7.747E+00	1.629E+00	1.350E+00	1.134E+00	1.047E+00	1.050E+00	1.046E+00	1.044E+00	1.044E+00	1.044E+00	
2.154E+03	9.208E+00	1.629E+00	1.601E+00	1.712E+00	1.694E+00	1.690E+00	1.689E+00	1.689E+00	1.689E+00	1.689E+00	
4.642E+03	1.067E+01	1.557E+00	2.425E+00	2.401E+00	2.398E+00	2.397E+00	2.396E+00	2.396E+00	2.396E+00	2.396E+00	
1.000E+04	1.207E+01	1.579E+00	3.141E+00	3.137E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	
2.154E+04	1.380E+01	1.579E+00	3.899E+00	3.890E+00	3.890E+00	3.890E+00	3.890E+00	3.890E+00	3.890E+00	3.890E+00	
4.642E+04	1.605E+01	1.557E+00	4.651E+00	4.651E+00	4.651E+00	4.651E+00	4.651E+00	4.651E+00	4.651E+00	4.651E+00	
1.000E+05	1.842E+01	1.544E+00	5.414E+00	5.416E+00	5.416E+00	5.416E+00	5.416E+00	5.416E+00	5.416E+00	5.416E+00	
2.154E+05	2.197E+01	1.544E+00	6.182E+00	6.182E+00	6.182E+00	6.182E+00	6.182E+00	6.182E+00	6.182E+00	6.182E+00	

LOG S/S' = -2.5

LOG K'R2/KR2	-7.0	-6.5	-6.0	-5.5	-5.0	-4.5	-4.0	-3.5	-3.0	-2.5	-2.0	
TT/R2S	R A D A T T E M E N T S						R E D U I T S					
1.000E-01	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	2.477E-02	
2.154E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	1.678E-01	
4.642E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	5.129E-01	
1.000E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	1.039E+00	
2.154E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	1.678E+00	
4.642E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	5.129E+00	
1.000E+01	3.121E+00	3.120E+00	3.120E+00	3.118E+00	3.114E+00	3.104E+00	3.087E+00	3.042E+00	2.968E+00	2.830E+00	2.605E+00	
2.154E+01	3.871E+00	3.870E+00	3.869E+00	3.866E+00	3.851E+00	3.840E+00	3.738E+00	3.619E+00	3.407E+00	3.032E+00	2.500E+00	
4.642E+01	4.629E+00	4.627E+00	4.625E+00	4.617E+00	4.604E+00	4.574E+00	4.514E+00	4.412E+00	4.227E+00	3.894E+00	3.315E+00	
1.000E+02	5.388E+00	5.387E+00	5.382E+00	5.371E+00	5.346E+00	5.298E+00	5.209E+00	5.050E+00	4.765E+00	4.259E+00	3.436E+00	
2.154E+02	6.150E+00	6.146E+00	6.138E+00	6.118E+00	6.079E+00	6.005E+00	5.870E+00	5.629E+00	5.170E+00	4.460E+00	3.402E+00	
4.642E+02	6.911E+00	6.904E+00	6.889E+00	6.857E+00	6.797E+00	6.685E+00	6.482E+00	6.121E+00	5.484E+00	4.522E+00	3.476E+00	
1.000E+03	7.671E+00	7.659E+00	7.634E+00	7.584E+00	7.492E+00	7.324E+00	7.023E+00	6.486E+00	5.600E+00	4.537E+00	3.503E+00	
2.154E+03	8.427E+00	8.407E+00	8.368E+00	8.292E+00	8.154E+00	7.904E+00	7.457E+00	6.680E+00	5.638E+00	4.561E+00	3.561E+00	
4.642E+03	9.179E+00	9.148E+00	9.088E+00	8.973E+00	8.767E+00	8.397E+00	7.784E+00	6.752E+00	5.657E+00	4.600E+00	3.677E+00	
1.000E+04	9.924E+00	9.874E+00	9.773E+00	9.614E+00	9.309E+00	8.763E+00	7.868E+00	6.771E+00	5.695E+00	4.704E+00	3.877E+00	
2.154E+04	1.067E+01	1.059E+01	1.046E+01	1.020E+01	9.750E+00	9.048E+00	7.900E+00	6.801E+00	5.771E+00	4.848E+00	4.061E+00	
4.642E+04	1.142E+01	1.130E+01	1.109E+01	1.072E+01	1.005E+01	9.076E+00	7.923E+00	6.861E+00	5.916E+00	5.089E+00	4.290E+00	
1.000E+05	1.207E+01	1.187E+01	1.157E+01	1.104E+01	1.016E+01	9.059E+00	7.969E+00	6.973E+00	6.145E+00	5.447E+00	4.655E+00	
2.154E+05	1.277E+01	1.208E+01	1.173E+01	1.113E+01	1.019E+01	9.093E+00	8.055E+00	7.188E+00	6.545E+00	6.255E+00	6.197E+00	

LOG S/S' = -2.5

LOG K'R2/KR2	-1.5	-1.0	-0.5	0.0	0.5	1.0	1.5	2.0	2.5	3.0
TT/RPS	R A D I A T I O N S				R E D U I T S					
1.000E-01	2.350E-02	2.241E-02	2.047E-02	1.703E-02	1.094E-02	3.073E-03	9.064E-05	0.0	5.654E-08	1.894E-07
2.154E-01	1.557E-01	1.456E-01	1.277E-01	9.585E-02	4.494E-02	6.079E-03	1.140E-04	0.0	1.022E-07	2.364E-07
4.642E-01	4.624E-01	4.211E-01	3.477E-01	2.204E-01	6.915E-02	6.462E-03	1.419E-04	0.0	1.048E-09	2.555E-07
1.000E+00	9.023E-01	7.919E-01	5.994E-01	3.014E-01	7.352E-02	7.328E-03	2.110E-04	2.312E-07	9.406E-08	3.607E-07
2.154E+00	1.399E+00	1.156E+00	7.637E-01	3.215E-01	7.740E-02	8.913E-03	4.066E-04	4.737E-06	1.547E-07	4.673E-08
4.642E+00	1.443E+00	1.149E+00	8.204E-01	3.296E-01	8.514E-02	1.266E-02	1.083E-03	5.235E-05	2.051E-06	1.044E-07
1.000E+01	2.195E+00	1.537E+00	4.351E-01	3.454E-01	1.022E-01	2.236E-02	4.070E-03	7.315E-04	1.791E-04	7.144E-05
2.154E+01	2.794E+00	1.584E+00	8.597E-01	3.808E-01	1.407E-01	4.494E-02	1.974E-02	1.007E-02	6.999E-03	6.020E-03
4.642E+01	2.941E+00	1.592E+00	1.454E+00	4.454E-01	2.917E-01	1.737E-01	6.999E-02	1.007E-02	7.994E-02	7.444E-02
1.000E+02	2.487E+00	1.644E+00	9.499E-01	6.094E-01	4.252E-01	3.519E-01	3.265E-01	3.183E-01	4.574E-01	4.114E-01
2.154E+02	2.533E+00	1.747E+00	1.104E+00	9.095E-01	6.037E-01	7.721E-01	7.630E-01	7.602E-01	7.544E-01	7.501E-01
4.642E+02	2.622E+00	1.944E+00	1.549E+00	1.402E+00	1.366E+00	1.357E+00	1.355E+00	1.354E+00	1.354E+00	1.354E+00
1.000E+03	2.811E+00	2.304E+00	2.064E+00	2.046E+00	2.038E+00	2.036E+00	2.035E+00	2.035E+00	2.035E+00	2.035E+00
2.154E+03	3.147E+00	2.849E+00	2.774E+00	2.764E+00	2.762E+00	2.761E+00	2.761E+00	2.761E+00	2.761E+00	2.761E+00
4.642E+03	3.653E+00	3.530E+00	3.512E+00	3.510E+00	3.509E+00	3.509E+00	3.509E+00	3.509E+00	3.509E+00	3.509E+00
1.000E+04	4.304E+00	4.271E+00	4.269E+00	4.268E+00	4.268E+00	4.268E+00	4.268E+00	4.268E+00	4.268E+00	4.268E+00
2.154E+04	5.039E+00	5.032E+00	5.031E+00	5.031E+00	5.031E+00	5.031E+00	5.031E+00	5.031E+00	5.031E+00	5.031E+00
4.642E+04	5.794E+00	5.797E+00	5.796E+00	5.797E+00	5.797E+00	5.796E+00	5.796E+00	5.796E+00	5.796E+00	5.796E+00
1.000E+05	6.544E+00	6.545E+00	6.545E+00	6.545E+00	6.545E+00	6.545E+00	6.545E+00	6.545E+00	6.545E+00	6.545E+00
2.154E+05	7.330E+00	7.330E+00	7.330E+00	7.330E+00	7.330E+00	7.330E+00	7.330E+00	7.330E+00	7.330E+00	7.330E+00

The diagram illustrates a cross-section of a dam. On the left, the water level is labeled 'LIERE'. On the right, the water level is labeled 'ANISOTROPE'. The dam body is divided into two main regions: 'PENETRATION DU FUIST DE FCMFAGE (1)' on the left and 'PENETRATION DU PIEZOMETRE (4)' on the right. The flow paths are indicated by arrows, showing water entering from the left and exiting to the right. The material properties are labeled as 'K' (permeability) and 'S' (storage coefficient). The bottom of the dam is labeled 'IMPERMEABLE' (impermeable).

	LOG K'R2/KB2		-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.C	1.0
TT/R2S	R	A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.467E-02	2.448E-02	2.354E-02	2.071E-02	1.275E-02	2.120E-C3		
3.162E-01	3.133E-01	3.133E-01	3.132E-01	3.124E-01	3.076E-01	2.895E-01	2.326E-01	1.109E-01	4.351E-C3		
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.112E-01	6.411E-01	2.066E-01	4.676E-C3		
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.998E+00	1.915E+00	1.651E+00	9.997E-01	2.226E-01	5.687E-C3		
1.000E+01	2.110E+00	3.109E+00	3.099E+00	3.046E+00	2.856E+00	2.275E+00	1.158E+00	2.285E-01	9.053E-C3		
1.000E+02	5.370E+00	5.359E+00	5.299E+00	5.071E+00	4.355E+00	2.855E+00	1.197E+00	3.067E-01	2.025E-C2		
1.000E+03	7.640E+00	7.578E+00	7.342E+00	6.585E+00	4.945E+00	2.914E+00	1.421E+00	9.713E-01	1.010E+C0		
1.000E+04	5.862E+00	5.625E+00	5.655E+00	7.176E+00	5.023E+00	3.290E+00	2.650E+00	2.656E+00	2.040E+C0		

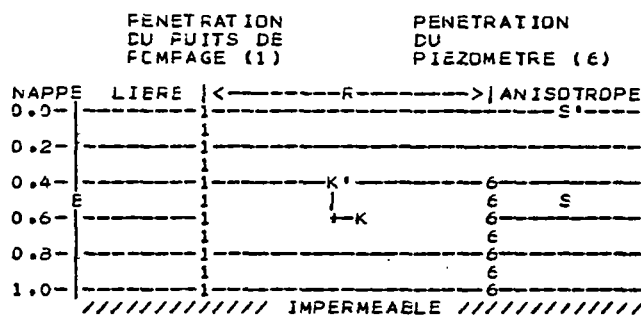
[illegible]

LOG K [*] R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.469E-02	2.467E-02	2.447E-02	2.352E-02	2.063E-02	1.265E-02	2.261E-03									
3.162E-01	3.133E-01	3.133E-01	3.133E-01	3.132E-01	3.124E-01	3.075E-01	2.894E-01	2.324E-01	1.111E-01	5.280E-03									
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.111E-01	6.411E-01	2.127E-01	6.618E-03									
3.162E+00	2.021E+00	2.020E+00	2.018E+00	2.018E+00	1.998E+00	1.915E+00	1.651E+00	1.003E+00	2.425E-01	2.117E-02									
1.000E+01	3.110E+00	3.109E+00	3.099E+00	3.099E+00	3.046E+00	2.856E+00	2.277E+00	1.175E+00	3.016E-01	7.600E-02									
1.000E+02	5.370E+00	5.359E+00	5.299E+00	5.299E+00	5.071E+00	4.359E+00	2.892E+00	1.423E+00	5.648E-01	1.003E+00									
1.000E+03	7.640E+00	7.578E+00	7.343E+00	7.343E+00	6.590E+00	4.999E+00	3.282E+00	2.682E+00	2.864E+00	3.032E+00									
1.000E+04	9.862E+00	9.626E+00	8.666E+00	8.666E+00	7.246E+00	5.465E+00	4.743E+00	4.782E+00	5.062E+00	5.209E+00									

LOG K ¹ R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.466E-02	2.446E-02	2.347E-02	2.045E-02	1.256E-02	2.555E-03	
3.162E-01	3.133E-01	3.133E-01	3.132E-01	3.124E-01	3.075E-01	2.893E-01	2.319E-01	1.116E-01	7.546E-03	
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.103E-01	6.410E-01	2.215E-01	1.544E-02	
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.997E+00	1.915E+00	1.651E+00	1.309E+00	2.905E-01	7.477E-02	
1.000E+01	3.110E+00	3.110E+00	3.099E+00	3.046E+00	2.856E+00	2.280E+00	1.217E+00	4.708E-01	3.250E-01	
1.000E+02	5.370E+00	5.359E+00	5.299E+00	5.072E+00	4.366E+00	2.974E+00	1.950E+00	1.795E+00	1.939E+00	
1.000E+03	7.640E+00	7.575E+00	7.343E+00	6.602E+00	5.113E+00	3.838E+00	3.681E+00	3.523E+00	4.133E+00	
1.000E+04	9.863E+00	9.627E+00	8.881E+00	7.373E+00	6.048E+00	5.761E+00	5.871E+00	6.190E+00	6.425E+00	

LOG K'P2/KB2	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0			1.0			
TT/R2S	F	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S									
1.000E-01	2.470E-02	2.455E-12	2.469E-12	2.466E-02	2.443E-02	2.332E-02	1.969E-02	1.221E-02	3.574E-03																			
3.162E-01	1.133E-01	3.132E-01	3.132E-01	3.124E-01	3.074E-01	2.888E-01	2.305E-01	1.132E-01	1.461E-02																			
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.093E-01	6.411E-01	2.501E-01	6.375E-02																			
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.997E+00	1.915E+00	1.653E+00	1.053E+00	4.335E-01	2.013E-01																			
1.000E+01	3.110E+00	3.109E+00	3.109E+00	3.046E+00	2.856E+00	2.289E+00	1.337E+00	5.033E-01	9.420E-01																			
1.000E+02	5.370E+00	5.355E+00	5.295E+00	5.073E+00	4.388E+00	3.187E+00	2.601E+00	2.772E+00	2.958E+00																			
1.000E+03	7.640E+00	7.578E+00	7.346E+00	6.634E+00	5.368E+00	4.657E+00	4.695E+00	4.590E+00	5.220E+00																			
1.000E+04	9.863E+00	9.631E+00	8.517E+00	7.637E+00	6.872E+00	6.793E+00	6.939E+00	7.275E+00	7.521E+00																			

ÉLECTRONIQUE - CIRCE
CNRS - CENTRE INTER RÉGIONAL DE CALCUL ÉLECTRONIQUE - CIRCE
CNRS - CENTRE INTER RÉGIONAL DE CALCUL ÉLECTRONIQUE - CIRCE
UNIVERS - CENTRE INTER

[illegible][illegible]

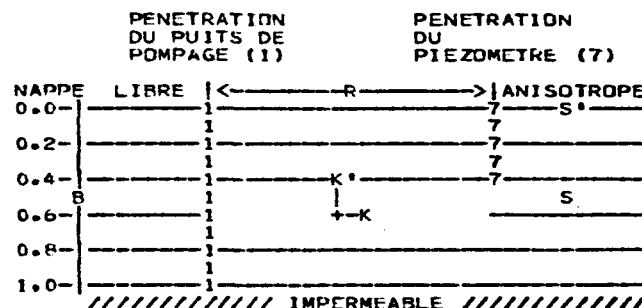
LOG K ¹ R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.485E-02	2.201E-02	4.285E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.134E-01	2.111E-01	9.601E-02	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.859E-01	4.055E-01	1.352E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.032E+00	1.671E+00	4.471E-01	2.949E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.051E+00	1.986E+00	5.048E-01	9.472E-02	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.328E+00	4.171E+00	2.160E+00	1.108E+00	1.015E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.628E+00	6.462E+00	4.361E+00	3.061E+00	2.862E+00	3.031E+00	
1.000E+04	1.002E+01	1.002E+01	9.932E+00	8.762E+00	6.655E+00	5.311E+00	5.002E+00	5.080E+00	5.287E+00	

	LOG K [*] R2/KB2		-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R	A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.489E-02	2.475E-02	2.177E-02	4.613E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.131E-01	2.109E-01	1.236E-02	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.851E-01	4.127E-01	2.726E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	4.512E-01	9.035E-02		
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.051E+00	2.005E+00	6.607E-01	3.509E-01	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.416E+00	5.327E+00	4.192E+00	2.432E+00	1.665E+00	1.942E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.717E+00	7.627E+00	6.482E+00	4.655E+00	3.941E+00	3.544E+00	4.131E+00	
1.000E+04	1.002E+01	1.002E+01	1.002E+01	1.002E+01	8.794E+00	6.949E+00	6.205E+00	6.077E+00	6.205E+00	6.423E+00	

LOG K*F2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	2.491E-02	2.493E-02	2.493E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.485E-02	2.445E-02	2.104E-02	5.551E-03								
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.158E-01	3.121E-01	2.104E-01	2.115E-02								
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.823E-01	4.335E-01	7.763E-02								
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.037E+00	1.674E+00	6.171E-01	3.221E-01								
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.048E+00	2.058E+00	1.041E+00	9.540E-01								
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.417E+00	5.416E+00	5.416E+00	5.325E+00	4.254E+00	2.978E+00	2.205E+00	2.957E+00								
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.716E+00	7.625E+00	6.545E+00	5.225E+00	4.918E+00	5.006E+00	5.218E+00	7.515E+00								
1.000E+04	1.002E+01	1.002E+01	1.002E+01	9.629E+00	8.847E+00	7.521E+00	7.185E+00	7.140E+00	7.289E+00	7.515E+00	7.515E+00								

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE DOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R ² /KB ²	-7.0	-5.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.459E-02	2.458E-02	2.459E-02	2.455E-02	2.421E-02	2.288E-02	1.863E-02	9.306E-03	1.485E-03	
3.162E-01	3.119E-01	3.119E-01	3.118E-01	3.107E-01	3.033E-01	2.763E-01	1.942E-01	7.803E-02	3.067E-03	
1.000E+00	1.031E+00	1.031E+00	1.030E+00	1.022E+00	9.811E-01	8.447E-01	5.000E-01	1.462E-01	3.397E-03	
3.162E+00	2.012E+00	2.012E+00	2.007E+00	1.977E+00	1.854E+00	1.465E+00	7.521E-01	1.563E-01	4.434E-03	
1.000E+01	3.097E+00	3.095E+00	3.081E+00	3.001E+00	2.716E+00	1.935E+00	8.624E-01	1.620E-01	7.911E-03	
1.000E+02	5.346E+00	5.330E+00	5.240E+00	4.899E+00	3.919E+00	2.343E+00	8.967E-01	2.372E-01	7.867E-02	
1.000E+03	7.601E+00	7.509E+00	7.155E+00	6.113E+00	4.334E+00	2.397E+00	1.126E+00	8.800E-01	9.896E-01	
1.000E+04	9.783E+00	9.427E+00	8.372E+00	6.530E+00	4.407E+00	2.768E+00	2.354E+00	2.715E+00	2.994E+00	

LOG S/S' = -2.5

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.459E-02	2.458E-02	2.459E-02	2.455E-02	2.426E-02	2.287E-02	1.860E-02	9.291E-03	1.531E-03	
3.162E-01	3.119E-01	3.119E-01	3.118E-01	3.107E-01	3.034E-01	2.762E-01	1.941E-01	7.808E-02	3.312E-03	
1.000E+00	1.031E+00	1.031E+00	1.030E+00	1.022E+00	9.811E-01	8.446E-01	5.000E-01	1.472E-01	4.352E-03	
3.162E+00	2.012E+00	2.012E+00	2.007E+00	1.977E+00	1.854E+00	1.465E+00	7.527E-01	1.610E-01	7.810E-03	
1.000E+01	3.097E+00	3.095E+00	3.081E+00	3.001E+00	2.716E+00	1.935E+00	8.665E-01	1.791E-01	2.068E-02	
1.000E+02	5.346E+00	5.330E+00	5.240E+00	4.899E+00	3.919E+00	2.351E+00	9.526E-01	4.116E-01	3.346E-01	
1.000E+03	7.601E+00	7.509E+00	7.155E+00	6.114E+00	4.347E+00	2.495E+00	1.561E+00	1.706E+00	1.928E+00	
1.000E+04	9.783E+00	9.427E+00	8.373E+00	6.548E+00	4.537E+00	3.332E+00	3.342E+00	3.788E+00	4.105E+00	

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.459E-02	2.458E-02	2.459E-02	2.455E-02	2.425E-02	2.284E-02	1.851E-02	9.243E-03	1.679E-03	
3.162E-01	3.119E-01	3.119E-01	3.118E-01	3.107E-01	3.033E-01	2.761E-01	1.939E-01	7.824E-02	4.093E-03	
1.000E+00	1.031E+00	1.031E+00	1.030E+00	1.022E+00	9.810E-01	8.444E-01	4.998E-01	1.501E-01	7.502E-03	
3.162E+00	2.012E+00	2.012E+00	2.007E+00	1.977E+00	1.854E+00	1.465E+00	7.547E-01	1.760E-01	2.018E-02	
1.000E+01	3.097E+00	3.095E+00	3.081E+00	3.001E+00	2.716E+00	1.936E+00	8.797E-01	2.329E-01	7.713E-02	
1.000E+02	5.346E+00	5.330E+00	5.240E+00	4.899E+00	3.921E+00	2.378E+00	1.118E+00	8.739E-01	9.834E-01	
1.000E+03	7.601E+00	7.509E+00	7.155E+00	6.118E+00	4.388E+00	2.759E+00	2.346E+00	2.707E+00	2.986E+00	
1.000E+04	9.783E+00	9.427E+00	8.378E+00	6.599E+00	4.844E+00	4.187E+00	4.390E+00	4.892E+00	5.232E+00	

LOG S/S' = -1.5

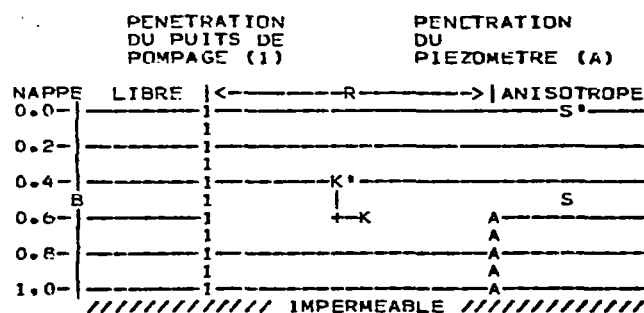
LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.459E-02	2.458E-02	2.459E-02	2.455E-02	2.423E-02	2.275E-02	1.821E-02	9.101E-03	2.139E-03
3.162E-01	3.119E-01	3.119E-01	3.118E-01	3.107E-01	3.033E-01	2.759E-01	1.931E-01	7.875E-02	6.587E-03
1.000E+00	1.031E+00	1.031E+00	1.030E+00	1.022E+00	9.809E-01	8.437E-01	4.992E-01	1.593E-01	1.867E-02
3.162E+00	2.012E+00	2.012E+00	2.007E+00	1.977E+00	1.853E+00	1.464E+00	7.609E-01	2.228E-01	7.355E-02
1.000E+01	3.097E+00	3.095E+00	3.081E+00	3.001E+00	2.716E+00	1.938E+00	9.202E-01	3.963E-01	3.229E-01
1.000E+02	5.346E+00	5.330E+00	5.240E+00	4.899E+00	3.928E+00	2.459E+00	1.536E+00	1.684E+00	1.905E+00
1.000E+03	7.601E+00	7.509E+00	7.155E+00	6.128E+00	4.499E+00	3.304E+00	3.315E+00	3.765E+00	4.081E+00
1.000E+04	9.783E+00	9.428E+00	8.392E+00	6.725E+00	5.414E+00	5.176E+00	5.461E+00	6.013E+00	6.367E+00

LOG S/S' = -1.0

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A R A T T E M E N T S					R E D U I T S				
1.000E-01	2.459E-02	2.458E-02	2.458E-02	2.454E-02	2.418E-02	2.246E-02	1.726E-02	8.745E-03	3.492E-03	
3.162E-01	3.119E-01	3.119E-01	3.118E-01	3.107E-01	3.031E-01	2.750E-01	1.907E-01	8.056E-02	1.459E-02	
1.000E+00	1.031E+00	1.031E+00	1.030E+00	1.022E+00	9.804E-01	8.417E-01	4.974E-01	1.879E-01	6.329E-02	
3.162E+00	2.012E+00	2.012E+00	2.007E+00	1.977E+00	1.852E+00	1.462E+00	7.801E-01	3.622E-01	2.964E-01	
1.000E+01	3.097E+00	3.095E+00	3.081E+00	3.001E+00	2.714E+00	1.944E+00	1.038E+00	8.168E-01	9.244E-01	
1.000E+02	5.346E+00	5.330E+00	5.240E+00	4.898E+00	3.946E+00	2.668E+00	2.267E+00	2.637E+00	2.915E+00	
1.000E+03	7.601E+00	7.509E+00	7.157E+00	6.157E+00	4.750E+00	4.102E+00	4.310E+00	4.825E+00	5.166E+00	
1.000E+04	9.784E+00	9.431E+00	8.424E+00	6.984E+00	6.218E+00	6.172E+00	6.519E+00	7.098E+00	7.463E+00	

ABAUQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.336E-02	4.523E-03
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.156E-01	2.285E-01	9.548E-03
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.018E+00	4.374E-01	9.721E-03
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.037E+00	1.759E+00	4.645E-01	1.120E-02
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.100E+00	2.094E+00	4.700E-01	1.607E-02
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.379E+00	4.302E+00	2.137E+00	5.406E-01	1.019E-01
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.679E+00	6.595E+00	4.347E+00	2.257E+00	1.094E+00	1.005E+00
1.000E+04	1.002E+01	1.002E+01	9.983E+00	8.897E+00	6.640E+00	4.476E+00	3.034E+00	2.778E+00	2.990E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.488E-02	2.333E-02	4.567E-03
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.155E-01	2.285E-01	9.548E-03
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.018E+00	4.380E-01	1.105E-02
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.037E+00	1.759E+00	4.686E-01	1.590E-02
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.100E+00	2.095E+00	4.859E-01	3.305E-02
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.378E+00	4.304E+00	2.165E+00	6.960E-01	3.653E-01
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.678E+00	6.597E+00	4.377E+00	2.499E+00	1.821E+00	1.930E+00
1.000E+04	1.002E+01	1.002E+01	9.983E+00	8.898E+00	6.670E+00	4.732E+00	3.863E+00	3.833E+00	4.100E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.484E-02	2.320E-02	4.705E-03
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.155E-01	2.282E-01	1.055E-02
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.017E+00	4.396E-01	1.535E-02
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.037E+00	1.759E+00	4.815E-01	3.229E-02
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.099E+00	2.099E+00	5.347E-01	1.000E-01
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.378E+00	4.308E+00	2.248E+00	1.087E+00	9.990E-01
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.678E+00	6.602E+00	4.467E+00	3.025E+00	2.770E+00	2.983E+00
1.000E+04	1.002E+01	1.002E+01	9.983E+00	8.903E+00	6.763E+00	5.276E+00	4.853E+00	4.930E+00	5.226E+00

LOG S/S' = -1.5

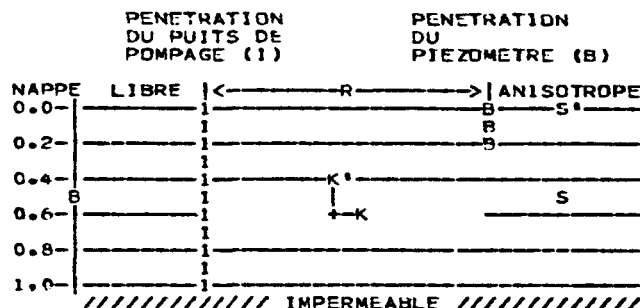
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.488E-02	2.472E-02	2.283E-02	5.140E-03
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.151E-01	2.275E-01	1.371E-02
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.016E+00	4.447E-01	2.999E-02
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.037E+00	1.757E+00	5.208E-01	9.560E-02
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.098E+00	2.110E+00	6.765E-01	3.529E-01
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.377E+00	4.321E+00	2.472E+00	1.797E+00	1.907E+00
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.677E+00	6.614E+00	4.704E+00	3.835E+00	3.808E+00	4.075E+00
1.000E+04	1.002E+01	1.002E+01	9.991E+00	8.916E+00	6.999E+00	6.098E+00	5.903E+00	6.048E+00	6.361E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.489E-02	2.484E-02	2.434E-02	2.171E-02	6.456E-03
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.157E-01	3.139E-01	2.255E-01	2.367E-02
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.013E+00	4.605E-01	8.290E-02
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.035E+00	1.754E+00	6.326E-01	3.251E-01
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.094E+00	2.144E+00	1.022E+00	9.400E-01
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.373E+00	4.358E+00	2.942E+00	2.694E+00	2.912E+00
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.673E+00	6.651E+00	5.190E+00	4.769E+00	4.858E+00	5.161E+00
1.000E+04	1.002E+01	1.002E+01	9.977E+00	8.953E+00	7.487E+00	7.034E+00	6.953E+00	7.129E+00	7.457E+00

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.420E-02	2.357E-02	2.093E-02	1.318E-02	4.954E-03	7.774E-04
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.055E-01	2.907E-01	2.368E-01	1.198E-01	4.039E-02	1.637E-03
1.000E+00	1.018E+00	1.018E+00	1.016E+00	9.999E-01	9.179E-01	6.586E-01	2.860E-01	7.556E-02	1.966E-03
3.162E+00	1.986E+00	1.985E+00	1.977E+00	1.917E+00	1.670E+00	1.043E+00	4.164E-01	8.151E-02	3.013E-03
1.000E+01	3.057E+00	3.054E+00	3.025E+00	2.866E+00	2.315E+00	1.299E+00	4.737E-01	8.705E-02	6.511E-03
1.000E+02	5.276E+00	5.245E+00	5.063E+00	4.400E+00	3.025E+00	1.511E+00	5.029E-01	1.597E-01	7.648E-02
1.000E+03	7.486E+00	7.301E+00	6.612E+00	5.117E+00	3.241E+00	1.560E+00	7.278E-01	7.841E-01	9.695E-01
1.000E+04	9.546E+00	8.852E+00	7.331E+00	5.336E+00	3.309E+00	1.927E+00	1.931E+00	2.574E+00	2.949E+00

LOG S/S' = -2.5

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.420E-02	2.357E-02	2.091E-02	1.314E-02	4.942E-03	8.375E-04
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.055E-01	2.907E-01	2.367E-01	1.197E-01	4.046E-02	1.904E-03
1.000E+00	1.018E+00	1.018E+00	1.016E+00	9.999E-01	9.179E-01	6.585E-01	2.859E-01	7.652E-02	2.949E-03
3.162E+00	1.986E+00	1.985E+00	1.977E+00	1.917E+00	1.670E+00	1.043E+00	4.170E-01	8.620E-02	6.430E-03
1.000E+01	3.057E+00	3.054E+00	3.025E+00	2.866E+00	2.315E+00	1.299E+00	4.779E-01	1.037E-01	1.928E-02
1.000E+02	5.276E+00	5.245E+00	5.063E+00	4.400E+00	3.025E+00	1.520E+00	5.579E-01	3.289E-01	3.273E-01
1.000E+03	7.486E+00	7.301E+00	6.612E+00	5.118E+00	3.255E+00	1.658E+00	1.155E+00	1.589E+00	1.894E+00
1.000E+04	9.546E+00	8.852E+00	7.332E+00	5.354E+00	3.438E+00	2.483E+00	2.893E+00	3.631E+00	4.053E+00

LOG S/S' = -2.0

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.419E-02	2.356E-02	2.085E-02	1.300E-02	4.908E-03	1.026E-03
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.055E-01	2.907E-01	2.366E-01	1.193E-01	4.068E-02	2.751E-03
1.000E+00	1.018E+00	1.018E+00	1.016E+00	9.999E-01	9.178E-01	6.581E-01	2.855E-01	7.957E-02	6.179E-03
3.162E+00	1.986E+00	1.985E+00	1.977E+00	1.917E+00	1.670E+00	1.042E+00	4.188E-01	1.010E-01	1.885E-02
1.000E+01	3.057E+00	3.054E+00	3.025E+00	2.866E+00	2.314E+00	1.300E+00	4.909E-01	1.559E-01	7.505E-02
1.000E+02	5.276E+00	5.245E+00	5.063E+00	4.400E+00	3.027E+00	1.547E+00	7.205E-01	7.786E-01	9.636E-01
1.000E+03	7.486E+00	7.301E+00	6.612E+00	5.121E+00	3.295E+00	1.918E+00	1.923E+00	2.567E+00	2.941E+00
1.000E+04	9.546E+00	8.852E+00	7.337E+00	5.404E+00	3.742E+00	3.322E+00	3.918E+00	4.723E+00	5.177E+00

LOG S/S' = -1.5

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.419E-02	2.352E-02	2.067E-02	1.256E-02	4.809E-03	1.612E-03
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.055E-01	2.906E-01	2.360E-01	1.182E-01	4.138E-02	5.443E-03
1.000E+00	1.018E+00	1.018E+00	1.016E+00	9.999E-01	9.175E-01	6.569E-01	2.845E-01	8.916E-02	1.753E-02
3.162E+00	1.986E+00	1.985E+00	1.977E+00	1.917E+00	1.669E+00	1.041E+00	4.247E-01	1.471E-01	7.175E-02
1.000E+01	3.057E+00	3.054E+00	3.025E+00	2.866E+00	2.313E+00	1.301E+00	5.313E-01	3.152E-01	3.162E-01
1.000E+02	5.276E+00	5.245E+00	5.063E+00	4.399E+00	3.031E+00	1.626E+00	1.132E+00	1.569E+00	1.872E+00
1.000E+03	7.486E+00	7.301E+00	6.612E+00	5.130E+00	3.406E+00	2.456E+00	2.868E+00	3.609E+00	4.030E+00
1.000E+04	9.546E+00	8.853E+00	7.349E+00	5.529E+00	4.304E+00	4.283E+00	4.972E+00	5.839E+00	6.310E+00

LOG S/S' = -1.0

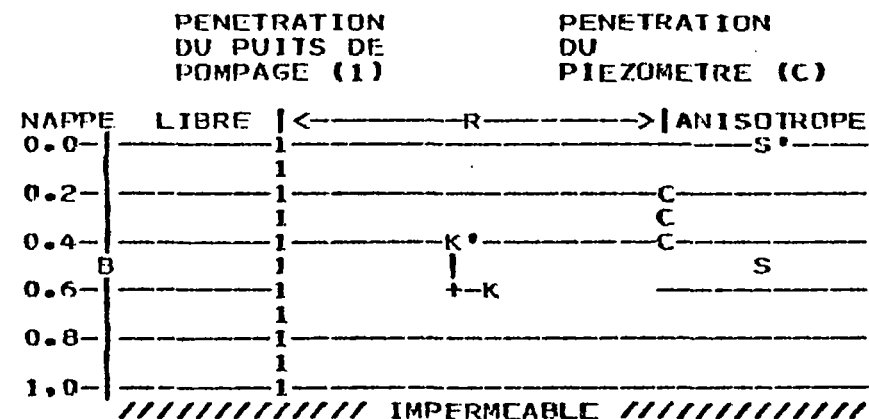
LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.417E-02	2.340E-02	2.012E-02	1.123E-02	4.620E-03	3.332E-03
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.054E-01	2.902E-01	2.344E-01	1.149E-01	4.387E-02	1.400E-02
1.000E+00	1.018E+00	1.018E+00	1.016E+00	9.997E-01	9.165E-01	6.530E-01	2.814E-01	1.191E-01	6.224E-02
3.162E+00	1.986E+00	1.985E+00	1.977E+00	1.916E+00	1.667E+00	1.035E+00	4.431E-01	2.849E-01	2.910E-01
1.000E+01	3.057E+00	3.054E+00	3.025E+00	2.865E+00	2.309E+00	1.303E+00	6.488E-01	7.267E-01	9.069E-01
1.000E+02	5.276E+00	5.244E+00	5.062E+00	4.396E+00	3.045E+00	1.833E+00	1.849E+00	2.502E+00	2.872E+00
1.000E+03	7.486E+00	7.300E+00	6.610E+00	5.154E+00	3.653E+00	3.237E+00	3.842E+00	4.662E+00	5.113E+00
1.000E+04	9.545E+00	8.852E+00	7.376E+00	5.784E+00	5.091E+00	5.256E+00	6.022E+00	6.924E+00	7.406E+00

PUITS A PENETRATION COMPLETE ET PIEZOMETRE OUVERT DE 0.20 A 0.40

TABLEAU 1 C

ABaque POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



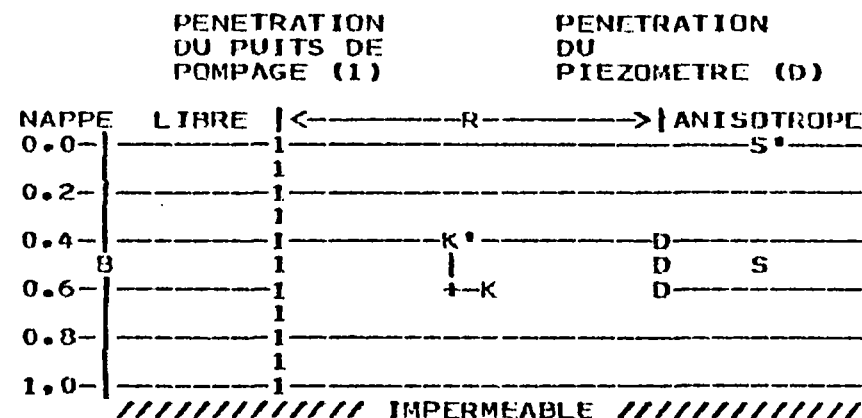
LOG S/S' = -2.0

LOG K'R²/KB² -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A D A T T E M E N T S					R E D U I T S				
1.000E-01	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.487E-02	2.392E-02	1.349E-02	2.444E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.030E+00	7.132E-01	2.200E-01	9.907E-03	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.117E+00	2.570E+00	1.261E+00	3.029E-01	8.623E-02	
1.000E+02	5.416E+00	5.416E+00	5.416E+00	5.397E+00	4.812E+00	3.186E+00	1.443E+00	8.837E-01	9.707E-01	
1.000E+03	7.716E+00	7.716E+00	7.697E+00	7.108E+00	5.436E+00	3.406E+00	2.402E+00	2.595E+00	2.938E+00	
1.000E+04	1.002E+01	1.000E+01	9.411E+00	7.733E+00	5.663E+00	4.449E+00	4.285E+00	4.739E+00	5.172E+00	

PUITS A PENETRATION COMPLETE ET PIEZOMETRE OUVERT DE 0.40 A 0.60
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 1 D

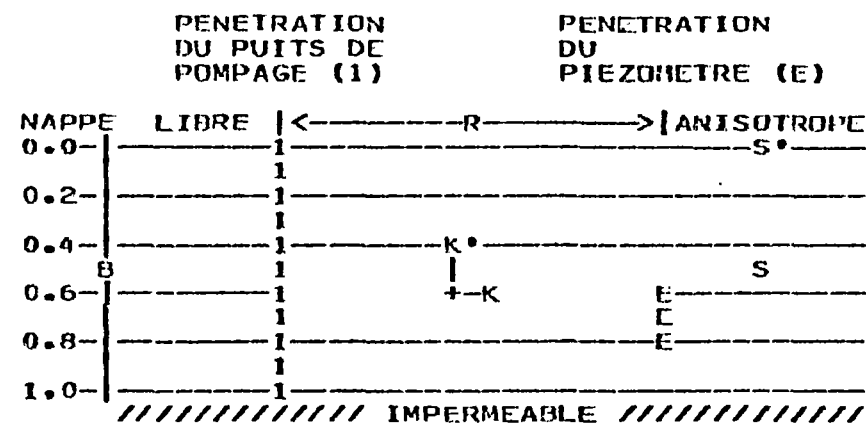


LOG S/S' = -2.0

LOG K*R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.489E-02	2.474E-02	1.939E-02	3.646E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.223E-01	3.362E-01	1.300E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	2.955E+00	1.753E+00	4.233E-01	9.485E-02	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.227E+00	3.885E+00	1.906E+00	9.695E-01	9.760E-01	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.526E+00	6.169E+00	4.054E+00	2.717E+00	2.625E+00	2.936E+00	
1.000E+04	1.002E+01	1.002E+01	9.830E+00	8.469E+00	6.341E+00	4.911E+00	4.523E+00	4.759E+00	5.169E+00	

PUITS A PENETRATION COMPLETE ET PIEZOMETRE OUVERT DE 0.60 A 0.80
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 1 E



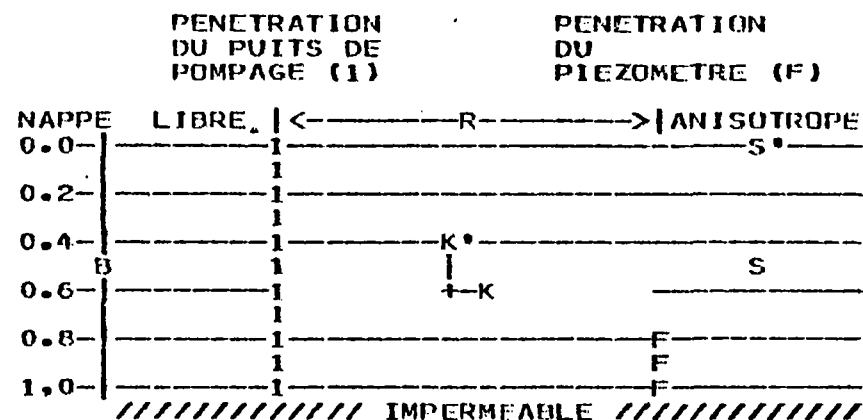
LOG S/S' = -2.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.489E-02	2.482E-02	2.253E-02	4.522E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.004E+00	4.181E-01	1.522E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.081E+00	2.034E+00	5.077E-01	1.007E-01	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.359E+00	4.232E+00	2.173E+00	1.030E+00	9.795E-01	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.659E+00	6.524E+00	4.379E+00	2.899E+00	2.649E+00	2.935E+00	
1.000E+04	1.002E+01	1.002E+01	9.963E+00	8.824E+00	6.674E+00	5.137E+00	4.654E+00	4.777E+00	5.167E+00	

PUITS A PENETRATION COMPLETE ET PIEZOMETRE OUVERT DE 0.80 A 1.00
 ARAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABEAU 1 F



LOG S/S* = -2.0

LOG K*R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

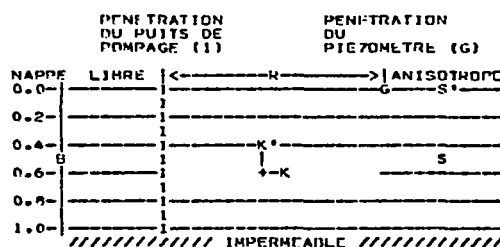
TT/R2S	R A B A T T E M E N T S								R E D U I T S	
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.483E-02	2.377E-02	4.980E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.030E+00	4.600E-01	1.637E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.117E+00	2.161E+00	5.510E-01	1.037E-01	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.416E+00	5.397E+00	4.381E+00	2.294E+00	1.060E+00	9.813E-01	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.697E+00	6.676E+00	4.521E+00	2.982E+00	2.662E+00	2.934E+00	
1.000E+04	1.002E+01	1.002E+01	1.000E+01	8.977E+00	6.818E+00	5.235E+00	4.713E+00	4.786E+00	5.166E+00	

PUITS A PENETRATION COMPLETE ET PIEZOMETRIE PONCTUEL AU SOMMET DE LA NAPPE

TABLEAU 1 G

ABAIQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIMBE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE HOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K ₁ R ₂ /K ₂ R ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	2.0	3.0	
TT/R ₂ S	R A B A T T E M E N T S					R E D U I T S						
1.000E-01	7.237E-07	4.526E-07	1.279E-06	2.036E-06	2.047E-06	0.0	3.307E-07	1.115E-06	1.947E-06	0.0	0.0	
3.162E-01	8.576E-06	3.937E-05	1.010E-05	1.211E-05	1.051E-05	6.823E-06	1.708E-05	5.239E-05	3.161E-05	0.0	0.0	
1.000E+00	2.031E-05	2.957E-05	3.278E-05	3.707E-05	3.646E-05	5.072E-05	1.701E-04	4.044E-04	1.307E-04	0.0	0.0	
3.162E+00	5.699E-05	5.988E-05	6.939E-05	8.448E-05	1.272E-04	3.259E-04	1.014E-03	2.216E-03	4.045E-04	0.0	0.0	
1.000E+01	4.733E-05	1.015E-04	1.317E-04	2.055E-04	4.658E-04	1.387E-03	4.261E-03	7.730E-03	1.850E-03	6.914E-03	0.0	
3.162E+01	1.327E-04	1.711E-04	2.746E-04	5.008E-04	1.660E-03	5.154E-03	1.497E-02	2.543E-02	8.350E-03	5.200E-04	6.931E-05	
1.000E+02	2.051E-04	3.200E-04	6.915E-04	1.863E-03	5.674E-03	1.774E-02	4.843E-02	0.370E-02	5.101E-02	2.867E-02	2.524E-02	
3.162E+02	3.686E-04	7.569E-04	2.012E-03	6.014E-03	1.877E-02	5.796E-02	1.864E-01	2.826E-01	3.040E-01	3.145E-01	3.154E-01	
1.000E+03	8.211E-04	2.119E-03	4.241E-03	1.938E-02	6.093E-02	1.850E-01	4.914E-01	8.861E-01	1.024E+00	1.042E+00	1.043E+00	
3.162E+03	2.194E-03	6.354E-03	1.074E-02	4.205E-02	1.044E-01	5.783E-01	1.377E+00	1.945E+00	2.020E+00	2.036E+00	2.037E+00	
1.000E+04	6.504E-03	1.997E-02	6.267E-02	1.974E-01	6.076E-01	1.630E+00	2.704E+00	3.103E+00	3.132E+00	3.125E+00	3.135E+00	
3.162E+04	2.017E-02	6.303E-02	1.945E-01	6.170E-01	1.719E+00	3.357E+00	4.160E+00	4.257E+00	4.269E+00	4.270E+00	4.270E+00	
1.000E+05	6.327E-02	1.991E-01	6.202E-01	1.748E+00	3.604E+00	5.057E+00	5.382E+00	5.412E+00	5.415E+00	5.416E+00	5.416E+00	
3.162E+05	1.994E-01	6.211E-01	1.758E+00	3.693E+00	5.616E+00	6.454E+00	7.545E+00	6.564E+00	6.565E+00	6.565E+00	6.565E+00	
1.000E+06	6.215E-01	1.750E+00	3.722E+00	5.863E+00	7.354E+00	7.642E+00	7.713E+00	7.716E+00	7.716E+00	7.716E+00	7.716E+00	

LOG S/S' = -2.5

LOG K ₁ R ₂ /K ₂ R ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ₂ S	R A B A T T E M E N T S						R E D U I T S		
1.000E-01	4.567E-07	1.253E-06	2.262E-06	3.350E-06	5.184E-07	5.491E-07	1.259E-06	3.569E-06	6.464E-06
3.162E-01	9.576E-06	1.024E-05	1.338E-05	1.676E-05	1.185E-05	1.876E-05	5.331E-05	1.564E-04	1.000E-04
1.000E+00	2.031E-05	3.356E-05	4.321E-05	5.539E-05	7.228E-05	1.813E-04	5.610E-04	1.563E-03	4.562E-03
3.162E+00	6.021E-05	7.249E-05	1.020E-04	1.613E-04	3.440E-04	1.020E-03	3.204E-03	7.023E-03	1.743E-03
1.000E+01	1.027E-04	1.614E-04	2.420E-04	5.114E-04	1.407E-03	4.372E-03	1.347E-02	2.469E-02	8.240E-02
1.000E+02	3.184E-04	7.337E-04	1.929E-03	5.728E-03	1.787E-02	5.606E-02	1.548E-01	2.814E-01	3.081E-01
1.000E+03	2.161E-03	6.313E-03	1.045E-02	4.109E-02	1.023E-01	5.763E-01	1.305E+00	1.944E+00	2.020E+00
1.000E+04	2.005E-02	6.275E-02	1.976E-01	6.150E-01	1.717E+00	3.355E+00	4.158E+00	4.257E+00	4.267E+00

LOG S/S' = -2.0

LOG K ₁ R ₂ /K ₂ R ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	2.0	3.0	
TT/R ₂ S	R A B A T T E M E N T S						R E D U I T S					
1.000E-01	1.273E-06	2.450E-06	4.947E-06	4.906E-06	1.290E-06	1.367E-06	3.659E-06	1.127E-05	2.033E-05	0.0	0.0	
3.162E-01	1.031E-05	1.040E-05	2.195E-05	2.448E-05	2.387E-05	5.482E-05	1.672E-04	5.226E-04	3.272E-04	0.0	0.0	
1.000E+00	3.380E-05	4.554E-05	7.105E-05	1.001E-04	1.039E-04	5.400E-04	1.771E-03	4.947E-03	1.617E-03	5.806E-03	0.0	
3.162E+00	7.335E-05	1.055E-04	1.964E-04	3.871E-04	1.028E-03	3.212E-03	1.013E-02	2.237E-02	7.840E-02	4.863E-02	6.456E-02	
1.000E+01	1.442E-04	2.624E-04	5.690E-04	1.442E-03	4.392E-03	1.381E-02	4.259E-02	0.222E-02	4.945E-02	2.788E-02	2.450E-02	
3.162E+01	3.064E-04	6.845E-04	1.788E-03	5.241E-03	1.637E-02	5.150E-02	1.497E-01	2.779E-01	3.050E-01	3.105E-01	3.113E-01	
1.000E+02	7.189E-04	1.984E-03	5.816E-03	1.707E-02	5.644E-02	1.770E-01	4.843E-01	8.704E-01	1.017E+00	1.036E+00	1.036E+00	
3.162E+02	2.115E-03	6.149E-03	1.804E-02	5.941E-02	1.873E-01	5.700E-01	1.379E+00	1.937E+00	2.070E+00	2.028E+00	2.029E+00	
1.000E+03	6.340E-03	1.955E-02	6.120E-02	1.977E-01	5.920E-01	1.621E+00	2.795E+00	3.045E+00	3.124E+00	3.126E+00	3.127E+00	
3.162E+03	1.991E-02	6.223E-02	1.959E-01	6.094E-01	1.710E+00	3.344E+00	4.151E+00	4.250E+00	4.260E+00	4.261E+00	4.261E+00	
1.000E+04	6.285E-02	1.977E-01	6.155E-01	1.734E+00	3.595E+00	5.040E+00	5.373E+00	5.403E+00	5.406E+00	5.407E+00	5.407E+00	
3.162E+04	1.987E-01	6.144E-01	1.750E+00	3.644E+00	5.407E+00	6.445E+00	6.546E+00	6.555E+00	6.556E+00	6.556E+00	6.556E+00	
1.000E+05	6.205E-01	1.756E+00	3.714E+00	5.054E+00	7.345E+00	7.345E+00	7.704E+00	7.707E+00	7.707E+00	7.707E+00	7.707E+00	
3.162E+05	1.789E+00	3.723E+00	5.044E+00	7.066E+00	9.747E+00	8.847E+00	8.857E+00	8.858E+00	8.858E+00	8.858E+00	8.858E+00	
1.000E+06	3.724E+00	5.061E+00	6.152E+00	9.651E+00	9.974E+00	1.001E+01	1.001E+01	1.001E+01	1.001E+01	1.001E+01	1.001E+01	

LOG S/S' = -1.5

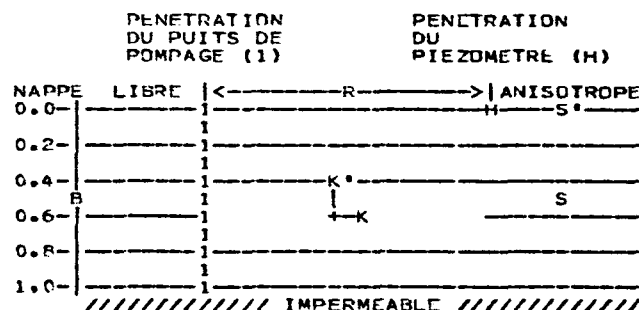
LOG K ₁ R ₂ /K ₂ R ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ₂ S	R A B A T T E M E N T S						R E D U I T S		
1.000E-01	2.565E-06	6.045E-06	1.195E-05	1.030E-05	3.060E-06	3.020E-06	1.128E-05	3.532E-05	6.339E-05
3.162E-01	1.440E-05	2.541E-05	4.476E-05	4.918E-05	6.114E-05	1.601E-04	5.275E-04	1.652E-03	1.111E-03
1.000E+00	4.674E-05	8.160E-05	1.486E-04	2.405E-04	5.778E-04	1.774E-03	5.598E-03	1.568E-02	6.859E-02
3.162E+00	1.147E-04	2.254E-04	4.739E-04	1.101E-03	3.232E-03	1.015E-02	3.202E-02	7.213E-02	4.650E-02
1.000E+01	2.737E-04	6.322E-04	1.579E-03	4.467E-03	1.383E-02	4.365E-02	1.345E-01	2.671E-01	2.955E-01
1.000E+02	2.900E-03	5.954E-03	1.808E-02	5.652E-02	1.781E-01	5.508E-01	1.308E+00	1.918E+00	2.000E+00
1.000E+03	1.969E-02	6.137E-02	1.928E-01	6.002E-01	1.689E+00	3.327E+00	4.130E+00	4.230E+00	4.240E+00
1.000E+04	1.979E-01	6.157E-01	1.741E+00	3.664E+00	5.588E+00	6.424E+00	6.535E+00	6.545E+00	6.536E+00

LOG S/S' = -1.0

LOG K ₁ R ₂ /K ₂ R ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	2.0	3.0	
TT/R ₂ S	R A H A T T E M E N T S						R E D U I T S					
1.000E-01	6.595E-06	1.604E-05	3.189E-05	3.140E-05	7.763E-06	1.123E-05	3.518E-05	1.058E-04	1.629E-04	0.0	0.0	
3.162E-01	2.714E-05	5.962E-05	1.111E-04	1.325E-04	1.781E-04	5.207E-04	1.665E-03	5.204E-03	4.158E-03	2.078E-03	1.929E-03	
1.000E+00	8.704E-05	1.906E-04	3.824E-04	6.900E-04	1.741E-03	5.600E-03	1.769E-02	4.904E-02	3.754E-02	2.044E-02	1.788E-02	
3.162E+00	2.414E-04	5.765E-04	1.336E-03	3.363E-03	1.017E-02	3.206E-02	1.010E-01	2.353E-01	2.673E-01	4.717E-01	2.733E-01	
1.000E+01	6.777E-04	1.780E-03	4.700E-03	1.397E-02	4.367E-02	1.377E-01	4.180E-01	8.161E-01	9.512E-01	9.673E-01	9.688E-01	
3.162E+01	2.002E-03	5.680E-03	1.672E-02	5.119E-02	1.026E-01	5.043E-01	1.303E+00	1.881E+00	1.942E+00	1.950E+00	1.950E+00	
1.000E+02	6.162E-03	1.844E-02	5.684E-02	1.782E-01	5.542E-01	1.540E+00	2.711E+00	3.011E+00	3.044E+00	3.047E+00	3.048E+00	
3.162E+02	1.941E-02	5.995E-02	1.877E-01	5.834E-01	1.640E+00	3.263E+00	4.064E+00	4.167E+00	4.162E+00	4.164E+00	4.164E+00	
1.000E+03	6.174E-02	1.932E-01	6.005E-01	1.693E+00	3.511E+00	4.961E+00	5.286E+00	5.323E+00	5.331E+00	5.331E+00	5.331E+00	
3.162E+03	1.965E-01	6.103E-01	1.723E+00	3.513E+00	5.521E+00	6.356E+00	6.441E+00	6.478E+00	6.485E+00	6.487E+00	6.487E+00	
1.000E+04	6.160E-01	1.741E+00	3.647E+00	5.770E+00	7.258E+00	7.625E+00	7.625E+00	7.625E+00	7.625E+00	7.625E+00	7.625E+00	
3.162E+04	1.751E+00	3.689E+00	5.873E+00	7.819E+00	8.655E+00	8.767E+00	8.767E+00	8.767E+00	8.767E+00	8.767E+00	8.767E+00	
1.000E+05	3.710E+00	9.927E+00	2.773E+01	9.563E+00	9.189E+00	9.125E+00	9.125E+00	9.046E+00	9.055E+00	9.054E+00	9.054E+00	
3.162E+05	5.953E+00	8.150E+00	1.012E+01	1.008E+01	1.109E+01	1.110E+01	1.111E+01	1.112E+01	1.113E+01	1.113E+01	1.113E+01	
1.000E+06	1.025E+00	1.025E+01	1.177E+01	1.216E+01	1.221E+01	1.222E+01	1.223E+01	1.224E+01	1.225E+01	1.225E+01	1.225E+01	

ABRAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.248E-02	2.248E-02	2.251E-02	2.278E-02	2.433E-02	1.972E-02	7.798E-03	2.528E-03	3.799E-04
3.162E-01	2.852E-01	2.853E-01	2.862E-01	2.941E-01	3.092E-01	1.846E-01	6.512E-02	2.044E-02	7.998E-04
1.000E+00	9.428E-01	9.435E-01	9.506E-01	9.980E-01	9.269E-01	4.453E-01	1.506E-01	3.840E-02	9.320E-04
3.162E+00	1.840E+00	1.843E+00	1.874E+00	1.974E+00	1.519E+00	6.542E-01	2.171E-01	4.233E-02	1.365E-03
1.000E+01	2.833E+00	2.845E+00	2.934E+00	2.915E+00	1.921E+00	7.868E-01	2.484E-01	4.812E-02	2.952E-03
1.000E+02	4.905E+00	5.004E+00	5.031E+00	4.015E+00	2.301E+00	9.062E-01	2.953E-01	1.271E-01	5.517E-02
1.000E+03	7.083E+00	7.120E+00	6.142E+00	4.400E+00	2.436E+00	1.054E+00	7.231E-01	9.236E-01	1.028E+00
1.000E+04	9.202E+00	8.234E+00	6.528E+00	4.540E+00	2.709E+00	2.194E+00	2.864E+00	3.108E+00	3.133E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.248E-02	2.248E-02	2.251E-02	2.278E-02	2.433E-02	1.976E-02	7.798E-03	2.530E-03	3.848E-04
3.162E-01	2.852E-01	2.853E-01	2.862E-01	2.941E-01	3.092E-01	1.846E-01	6.515E-02	2.055E-02	8.819E-04
1.000E+00	9.428E-01	9.435E-01	9.506E-01	9.980E-01	9.269E-01	4.454E-01	1.510E-01	3.949E-02	1.312E-03
3.162E+00	1.840E+00	1.843E+00	1.874E+00	1.974E+00	1.519E+00	6.548E-01	2.193E-01	4.734E-02	2.884E-03
1.000E+01	2.833E+00	2.845E+00	2.934E+00	2.915E+00	1.921E+00	7.893E-01	2.574E-01	6.583E-02	1.010E-02
1.000E+02	4.905E+00	5.004E+00	5.031E+00	4.015E+00	2.307E+00	9.398E-01	3.995E-01	3.278E-01	3.145E-01
1.000E+03	7.083E+00	7.120E+00	6.143E+00	4.407E+00	2.502E+00	1.377E+00	1.548E+00	1.959E+00	2.027E+00
1.000E+04	9.202E+00	8.234E+00	6.535E+00	4.617E+00	3.239E+00	3.584E+00	4.175E+00	4.259E+00	4.267E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.248E-02	2.248E-02	2.251E-02	2.278E-02	2.433E-02	1.976E-02	7.800E-03	2.538E-03	4.000E-04
3.162E-01	2.852E-01	2.853E-01	2.862E-01	2.941E-01	3.092E-01	1.846E-01	6.526E-02	2.091E-02	1.149E-03
1.000E+00	9.428E-01	9.435E-01	9.506E-01	9.980E-01	9.269E-01	4.457E-01	1.522E-01	4.295E-02	2.673E-03
3.162E+00	1.840E+00	1.843E+00	1.874E+00	1.974E+00	1.520E+00	6.566E-01	2.260E-01	6.328E-02	9.715E-03
1.000E+01	2.833E+00	2.845E+00	2.934E+00	2.915E+00	1.922E+00	7.974E-01	2.861E-01	1.233E-01	5.374E-02
1.000E+02	4.905E+00	5.004E+00	5.031E+00	4.017E+00	2.325E+00	1.044E+00	7.157E-01	9.168E-01	1.021E+00
1.000E+03	7.083E+00	7.121E+00	6.144E+00	4.429E+00	2.698E+00	2.185E+00	2.855E+00	3.099E+00	3.124E+00
1.000E+04	9.202E+00	8.236E+00	6.557E+00	4.840E+00	4.316E+00	5.112E+00	5.378E+00	5.404E+00	5.407E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.248E-02	2.248E-02	2.251E-02	2.278E-02	2.433E-02	1.977E-02	7.807E-03	2.562E-03	4.479E-04
3.162E-01	2.852E-01	2.853E-01	2.862E-01	2.941E-01	3.092E-01	1.847E-01	6.560E-02	2.204E-02	2.061E-03
1.000E+00	9.428E-01	9.435E-01	9.506E-01	9.980E-01	9.269E-01	4.466E-01	1.559E-01	5.389E-02	8.557E-03
3.162E+00	1.840E+00	1.843E+00	1.874E+00	1.974E+00	1.520E+00	6.523E-01	2.474E-01	1.146E-01	5.044E-02
1.000E+01	2.833E+00	2.845E+00	2.934E+00	2.915E+00	1.922E+00	8.226E-01	3.757E-01	3.128E-01	3.018E-01
1.000E+02	4.905E+00	5.004E+00	5.031E+00	4.021E+00	2.382E+00	1.349E+00	1.523E+00	1.933E+00	2.002E+00
1.000E+03	7.083E+00	7.121E+00	6.149E+00	4.496E+00	3.209E+00	3.557E+00	4.147E+00	4.231E+00	4.240E+00
1.000E+04	9.203E+00	8.240E+00	6.626E+00	5.400E+00	5.827E+00	6.441E+00	6.537E+00	6.546E+00	6.536E+00

LOG S/S' = -1.0

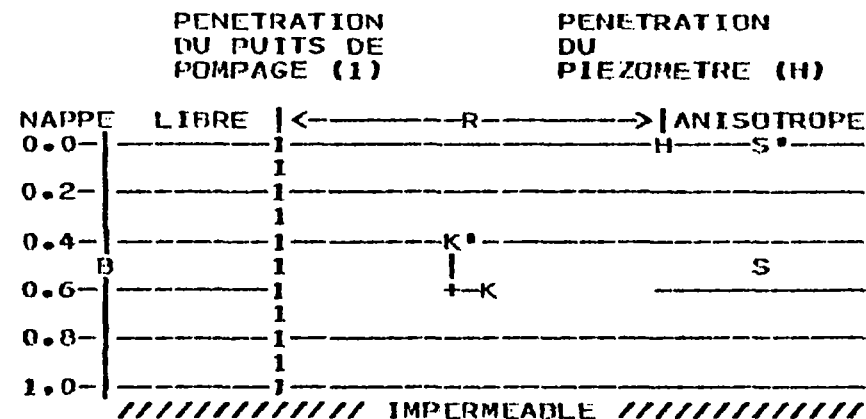
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.248E-02	2.248E-02	2.251E-02	2.278E-02	2.432E-02	1.977E-02	7.828E-03	2.634E-03	5.614E-04
3.162E-01	2.852E-01	2.853E-01	2.862E-01	2.941E-01	3.092E-01	1.849E-01	6.668E-02	2.558E-02	5.494E-03
1.000E+00	9.428E-01	9.435E-01	9.506E-01	9.980E-01	9.271E-01	4.495E-01	1.675E-01	8.851E-02	4.100E-02
3.162E+00	1.840E+00	1.843E+00	1.874E+00	1.974E+00	1.522E+00	6.800E-01	3.139E-01	2.794E-01	2.732E-01
1.000E+01	2.833E+00	2.845E+00	2.934E+00	2.915E+00	1.937E+00	9.002E-01	6.447E-01	8.526E-01	9.549E-01
1.000E+02	4.905E+00	5.004E+00	5.031E+00	4.036E+00	2.549E+00	2.101E+00	2.771E+00	3.016E+00	3.044E+00
1.000E+03	7.083E+00	7.121E+00	6.164E+00	4.689E+00	4.229E+00	5.025E+00	5.291E+00	5.324E+00	5.332E+00
1.000E+04	9.203E+00	8.255E+00	6.823E+00	5.465E+00	7.321E+00	7.591E+00	7.623E+00	7.634E+00	7.640E+00

PUITS A PENETRATION COMPLETE ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.10

TABLEAU 1 H

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



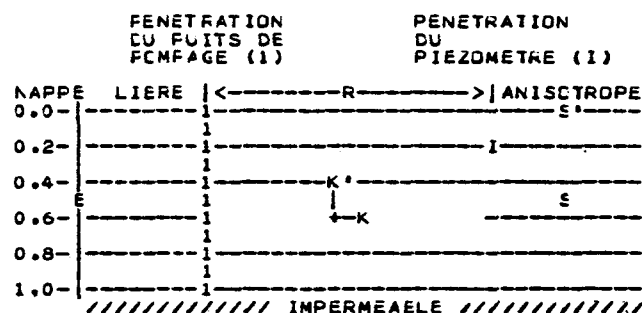
LOG S/S' = -2.0

LOG K'R2/KR2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.365E-02	2.365E-02	2.367E-02	2.380E-02	2.456E-02	2.457E-02	1.440E-02	5.021E-03	7.771E-04	
1.000E+00	9.918E-01	9.922E-01	9.957E-01	1.019E+00	1.038E+00	7.479E-01	2.956E-01	8.062E-02	3.716E-03	
1.000E+01	2.980E+00	2.986E+00	3.029E+00	3.101E+00	2.647E+00	1.418E+00	5.207E-01	1.656E-01	5.768E-02	
1.000E+02	5.152E+00	5.201E+00	5.299E+00	4.871E+00	3.393E+00	1.735E+00	9.296E-01	9.519E-01	1.025E+00	
1.000E+03	7.386E+00	7.490E+00	7.086E+00	5.625E+00	3.753E+00	2.619E+00	2.911E+00	3.104E+00	3.125E+00	
1.000E+04	9.679E+00	9.280E+00	7.842E+00	5.991E+00	4.819E+00	5.171E+00	5.383E+00	5.404E+00	5.407E+00	

TABLEAU 1.1

DANS L'HYPOTHESE DE NEUMAN. SELON FORMULES DE BOULTON - STRELTSEVA



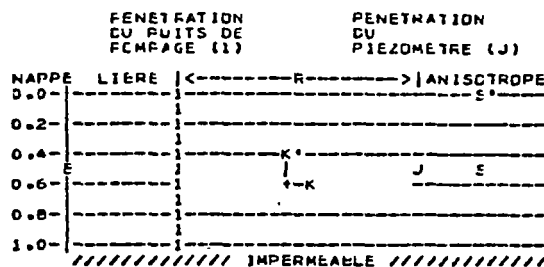
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.427E-02	2.426E-02	2.427E-02	2.434E-02	2.472E-02	2.490E-02	2.212E-02	5.763E-03	1.489E-03
3.162E-01	3.078E-01	3.078E-01	3.081E-01	3.100E-01	3.154E-01	3.149E-01	2.188E-01	7.583E-02	3.055E-03
1.000E+00	1.017E+00	1.018E+00	1.019E+00	1.031E+00	1.044E+00	9.892E-01	5.414E-01	1.491E-01	3.259E-03
3.162E+00	1.986E+00	1.987E+00	1.994E+00	2.023E+00	2.035E+00	1.691E+00	7.993E-01	1.596E-01	3.596E-03
1.000E+01	3.056E+00	3.059E+00	3.081E+00	3.121E+00	3.058E+00	2.168E+00	9.125E-01	1.660E-01	6.143E-03
1.000E+02	5.281E+00	5.306E+00	5.359E+00	5.321E+00	4.382E+00	2.606E+00	9.604E-01	2.111E-01	6.665E-02
1.000E+03	7.547E+00	7.604E+00	7.579E+00	6.658E+00	4.807E+00	2.685E+00	1.306E+00	1.023E+00	1.038E+00
1.000E+04	5.849E+00	5.627E+00	6.619E+00	7.083E+00	4.894E+00	3.250E+00	3.025E+00	3.121E+00	5.134E+00

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.427E-02	2.426E-02	2.427E-02	2.434E-02	2.472E-02	2.490E-02	2.212E-02	5.705E-03	1.455E-03
3.162E-01	3.078E-01	3.078E-01	3.081E-01	3.100E-01	3.154E-01	3.149E-01	2.189E-01	7.594E-02	3.173E-03
1.000E+00	1.017E+00	1.018E+00	1.019E+00	1.031E+00	1.044E+00	9.892E-01	5.416E-01	1.504E-01	3.614E-03
3.162E+00	1.986E+00	1.987E+00	1.994E+00	2.023E+00	2.035E+00	1.691E+00	8.309E-01	1.650E-01	6.043E-03
1.000E+01	3.056E+00	3.059E+00	3.081E+00	3.121E+00	3.058E+00	2.168E+00	9.197E-01	1.653E-01	1.540E-02
1.000E+02	5.281E+00	5.306E+00	5.359E+00	5.321E+00	4.383E+00	2.621E+00	1.047E+00	4.257E-01	3.217E-01
1.000E+03	7.547E+00	7.624E+00	7.579E+00	6.659E+00	4.823E+00	2.837E+00	1.944E+00	2.000E+00	2.031E+00
1.000E+04	5.849E+00	5.627E+00	5.520E+00	7.100E+00	5.062E+00	4.093E+00	4.220E+00	4.263E+00	4.267E+00

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.427E-02	2.426E-02	2.427E-02	2.434E-02	2.472E-02	2.493E-02	2.212E-02	6.712E-03	1.514E-03
3.162E-01	3.078E-01	3.078E-01	3.081E-01	3.100E-01	3.154E-01	3.149E-01	2.189E-01	6.028E-02	3.554E-02
1.000E+00	1.017E+00	1.018E+00	1.019E+00	1.031E+00	1.044E+00	9.893E-01	5.542E-01	1.535E-01	5.734E-02
3.162E+00	1.986E+00	1.987E+00	1.994E+00	2.023E+00	2.035E+00	1.692E+00	8.040E-01	1.821E-01	1.489E-02
1.000E+01	3.056E+00	3.059E+00	3.081E+00	3.121E+00	3.058E+00	2.191E+00	9.428E-01	2.466E-01	6.503E-02
1.000E+02	5.281E+00	5.306E+00	5.359E+00	5.321E+00	4.386E+00	2.666E+00	1.300E+00	1.016E+00	1.031E+00
1.000E+03	7.548E+00	7.604E+00	7.579E+00	6.663E+00	4.875E+00	3.241E+00	3.010E+00	2.113E+00	2.125E+00
1.000E+04	9.849E+00	9.827E+00	8.223E+00	7.152E+00	5.496E+00	5.276E+00	5.351E+00	5.405E+00	5.407E+00

LOG K'R2/KB2	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0			1.0								
TT/R2S	R	A	B	A	T	E	M	E	N	T	S	R	E	C	U	I	T	S	R	E	C	U	I	T	S	R	E	C	U	I	T	S	
1.000E-01	2.427E-02			2.426E-02			2.427E-02			2.434E-02			2.472E-02			2.490E-02			2.212E-02			5.732E-03			1.573E-03								
3.162E-01	3.078E-01			3.078E-01			3.081E-01			3.100E-01			3.154E-01			3.149E-01			2.191E-01			6.133E-02			4.619E-02								
1.000E+00	1.017E+00			1.018E+00			1.019E+00			1.031E+00			1.044E+00			9.893E-01			5.449E-01			1.655E-01			1.338E-01								
3.162E+00	1.986E+00			1.987E+00			1.994E+00			2.023E+00			2.035E+00			1.693E+00			8.220E-01			2.360E-01			6.126E-02								
1.000E+01	3.056E+00			3.059E+00			3.081E+00			3.121E+00			3.058E+00			2.199E+00			1.014E+00			4.589E-01			2.187E-01								
1.000E+02	5.281E+00			5.306E+00			5.359E+00			5.321E+00			4.396E+00			2.801E+00			1.918E+00			1.574E+00			2.006E+00								
1.000E+03	7.547E+00			7.604E+00			7.579E+00			6.672E+00			5.024E+00			4.065E+00			4.193E+00			4.235E+00			4.240E+00								
1.000E+04	5.849E+00			5.827E+00			5.933E+00			7.303E+00			6.353E+00			6.486E+00			6.541E+00			6.546E+00			6.546E+00								

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				F E C U I T S				
1.000E-01	2.427E-02	2.426E-02	2.427E-02	2.434E-02	2.472E-02	2.490E-02	2.213E-02	6.752E-03	1.724E-03
3.162E-01	3.678E-01	3.678E-01	3.681E-01	3.100E-01	3.154E-01	3.149E-01	2.196E-01	6.463E-02	9.310E-03
1.000E+00	1.017E+00	1.018E+00	1.019E+00	1.031E+00	1.044E+00	9.856E-01	5.525E-01	1.696E-01	5.057E-02
3.162E+00	1.986E+00	1.987E+00	1.994E+00	2.023E+00	2.035E+00	1.996E+00	8.707E-01	4.012E-01	2.853E-01
1.000E+01	3.056E+00	3.059E+00	3.081E+00	3.121E+00	3.059E+00	2.223E+00	1.217E+00	5.453E-01	9.650E-01
1.000E+02	5.281E+00	5.306E+00	5.359E+00	5.321E+00	4.425E+00	3.150E+00	2.926E+00	2.025E+00	3.042E+00
1.000E+03	7.548E+00	7.604E+00	7.575E+00	6.702E+00	5.402E+00	5.168E+00	5.305E+00	5.325E+00	5.332E+00
1.000E+04	5.849E+00	6.828E+00	6.563E+00	7.685E+00	7.466E+00	7.604E+00	7.624E+00	7.634E+00	7.640E+00



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.463E-02	2.462E-02	2.463E-02	2.466E-02	2.482E-02	2.490E-02	2.490E-02	1.576E-02	3.403E-03
3.162E-01	3.124E-01	3.124E-01	3.125E-01	3.133E-01	3.157E-01	3.159E-01	3.105E-01	1.774E-01	6.947E-03
1.000E+00	1.033E+00	1.033E+00	1.033E+00	1.038E+00	1.044E+00	1.044E+00	9.282E-01	3.255E-01	7.263E-03
3.162E+00	2.015E+00	2.015E+00	2.019E+00	2.031E+00	2.038E+00	2.024E+00	1.503E+00	3.565E-01	5.224E-03
1.000E+01	3.101E+00	3.103E+00	3.112E+00	3.130E+00	3.136E+00	2.965E+00	1.757E+00	3.637E-01	1.551E-02
1.000E+02	5.357E+00	5.366E+00	5.391E+00	5.410E+00	5.238E+00	3.892E+00	1.803E+00	4.517E-01	6.440E-02
1.000E+03	7.643E+00	7.667E+00	7.692E+00	7.531E+00	6.176E+00	3.944E+00	2.318E+00	1.165E+00	1.054E+00
1.000E+04	9.946E+00	9.972E+00	9.816E+00	8.470E+00	6.228E+00	4.198E+00	3.229E+00	3.141E+00	2.126E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.463E-02	2.462E-02	2.463E-02	2.466E-02	2.482E-02	2.490E-02	2.490E-02	1.576E-02	3.413E-03
3.162E-01	3.124E-01	3.124E-01	3.125E-01	3.133E-01	3.157E-01	3.159E-01	3.105E-01	1.774E-01	7.121E-03
1.000E+00	1.033E+00	1.033E+00	1.033E+00	1.038E+00	1.044E+00	1.044E+00	9.282E-01	3.255E-01	6.966E-03
3.162E+00	2.015E+00	2.015E+00	2.019E+00	2.031E+00	2.038E+00	2.024E+00	1.503E+00	3.624E-01	1.135E-02
1.000E+01	3.101E+00	3.103E+00	3.112E+00	3.130E+00	3.136E+00	2.965E+00	1.757E+00	3.637E-01	2.461E-02
1.000E+02	5.357E+00	5.366E+00	5.391E+00	5.410E+00	5.238E+00	3.892E+00	1.803E+00	4.517E-01	6.440E-02
1.000E+03	7.643E+00	7.667E+00	7.692E+00	7.531E+00	6.181E+00	4.007E+00	2.430E+00	2.055E+00	2.027E+00
1.000E+04	9.946E+00	9.972E+00	9.817E+00	8.475E+00	6.292E+00	4.659E+00	4.266E+00	4.266E+00	4.266E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	2.0	3.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S						
1.000E-01	2.463E-02	2.462E-02	2.463E-02	2.466E-02	2.482E-02	2.490E-02	2.490E-02	1.576E-02	3.437E-03	0.0	0.0
3.162E-01	3.124E-01	3.124E-01	3.125E-01	3.133E-01	3.157E-01	3.159E-01	3.105E-01	1.774E-01	7.678E-03	0.755E-08	0.0
1.000E+00	1.033E+00	1.033E+00	1.033E+00	1.038E+00	1.044E+00	1.044E+00	9.282E-01	3.255E-01	1.069E-02	1.515E-05	0.0
3.162E+00	2.015E+00	2.015E+00	2.019E+00	2.031E+00	2.038E+00	2.024E+00	1.503E+00	3.797E-01	2.232E-02	7.225E-04	6.990E-05
1.000E+01	3.101E+00	3.103E+00	3.112E+00	3.130E+00	3.136E+00	2.965E+00	1.757E+00	4.462E-01	8.256E-02	3.088E-02	2.480E-02
3.162E+01	4.223E+00	4.227E+00	4.246E+00	4.264E+00	4.255E+00	3.629E+00	1.849E+00	6.455E-01	3.541E-01	3.155E-01	3.111E-01
1.000E+02	5.357E+00	5.356E+00	5.391E+00	5.410E+00	5.238E+00	3.912E+00	2.010E+00	1.156E+00	1.047E+00	1.037E+00	1.037E+00
3.162E+02	6.457E+00	6.517E+00	6.541E+00	6.544E+00	5.911E+00	4.000E+00	2.244E+00	2.053E+00	2.031E+00	2.025E+00	2.025E+00
1.000E+03	7.643E+00	7.667E+00	7.692E+00	7.531E+00	6.196E+00	4.169E+00	3.220E+00	2.132E+00	2.127E+00	2.127E+00	2.127E+00
3.162E+03	8.763E+00	8.819E+00	8.828E+00	8.205E+00	6.285E+00	4.279E+00	4.262E+00	4.262E+00	4.262E+00	4.262E+00	4.262E+00
1.000E+04	9.946E+00	9.972E+00	9.817E+00	8.491E+00	6.478E+00	5.455E+00	5.411E+00	5.407E+00	5.407E+00	5.407E+00	5.407E+00
3.162E+04	1.112E+01	1.113E+01	1.051E+01	8.581E+00	6.947E+00	6.574E+00	6.558E+00	6.557E+00	6.556E+00	6.556E+00	6.556E+00
1.000E+05	1.220E+01	1.207E+01	1.075E+01	8.773E+00	7.795E+00	7.711E+00	7.707E+00	7.707E+00	7.707E+00	7.707E+00	7.707E+00
3.162E+05	1.249E+01	1.225E+01	1.086E+01	9.244E+00	8.876E+00	8.853E+00	8.853E+00	8.853E+00	8.853E+00	8.853E+00	8.853E+00
1.000E+06	1.249E+01	1.227E+01	1.104E+01	1.010E+01	1.002E+01	1.001E+01	1.001E+01	1.001E+01	1.001E+01	1.001E+01	1.001E+01

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.463E-02	2.462E-02	2.463E-02	2.466E-02	2.482E-02	2.490E-02	2.490E-02	1.577E-02	3.512E-03
3.162E-01	3.124E-01	3.124E-01	3.125E-01	3.133E-01	3.157E-01	3.159E-01	3.105E-01	1.785E-01	9.492E-03
1.000E+00	1.033E+00	1.033E+00	1.033E+00	1.038E+00	1.044E+00	1.044E+00	9.285E-01	3.495E-01	2.125E-02
3.162E+00	2.015E+00	2.015E+00	2.019E+00	2.031E+00	2.038E+00	2.024E+00	1.511E+00	4.332E-01	7.610E-03
1.000E+01	3.101E+00	3.103E+00	3.112E+00	3.130E+00	3.136E+00	2.965E+00	1.805E+00	4.314E-01	3.436E-02
1.000E+02	5.357E+00	5.366E+00	5.391E+00	5.410E+00	5.238E+00	3.892E+00	2.403E+00	3.333E+00	1.011E+00
1.000E+03	7.643E+00	7.667E+00	7.692E+00	7.532E+00	6.299E+00	4.631E+00	4.258E+00	4.247E+00	4.241E+00
1.000E+04	9.946E+00	9.972E+00	9.816E+00	8.538E+00	6.931E+00	6.553E+00	6.548E+00	6.547E+00	6.537E+00

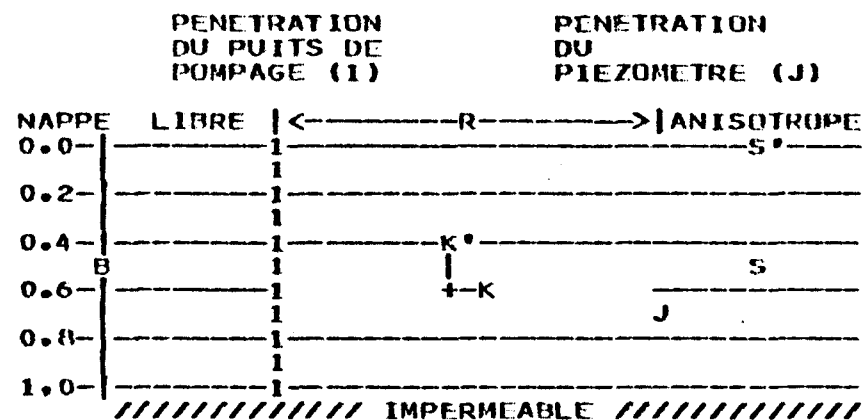
LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.463E-02	2.462E-02	2.463E-02	2.466E-02	2.482E-02	2.490E-02	2.490E-02	1.580E-02	3.713E-03
3.162E-01	3.124E-01	3.124E-01	3.125E-01	3.133E-01	3.157E-01	3.159E-01	3.105E-01	1.800E-01	1.540E-02
1.000E+00	1.033E+00	1.033E+00	1.033E+00	1.038E+00	1.044E+00	1.044E+00	9.305E-01	3.606E-01	6.547E-02
3.162E+00	2.015E+00	2.015E+00	2.019E+00	2.031E+00	2.038E+00	2.024E+00	1.527E+00	4.582E-01	3.132E-02
1.000E+01	3.101E+00	3.103E+00	3.112E+00	3.130E+00	3.136E+00	2.969E+00	1.913E+00	4.085E-01	5.600E-02
1.000E+02	5.357E+00	5.366E+00	5.391E+00	5.410E+00	5.242E+00	4.083E+00	3.135E+00	3.045E+00	3.047E+00
1.000E+03	7.643E+00	7.667E+00	7.692E+00	7.535E+00	6.374E+00	5.409E+00	5.325E+00	5.327E+00	5.322E+00
1.000E+04	9.946E+00	9.972E+00	9.821E+00	8.569E+00	7.708E+00	7.625E+00	7.626E+00	7.633E+00	7.640E+00

PUITS A PENETRATION COMPLETE ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.70

TABEAU 1 J

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



$\text{LOG } S/S^* = -2.0$

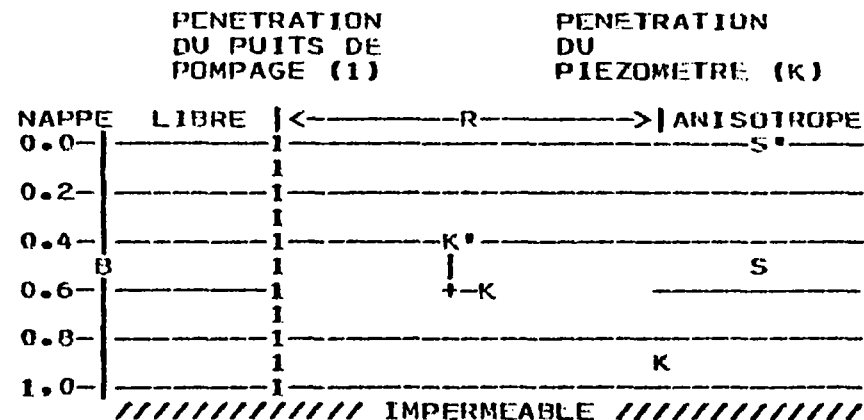
LOG K *R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	2.468E-02	2.468E-02	2.469E-02	2.471E-02	2.484E-02	2.490E-02	2.490E-02	2.289E-02	4.327E-03
1.000E+00	1.035E+00	1.035E+00	1.036E+00	1.040E+00	1.044E+00	1.044E+00	1.007E+00	4.221E-01	1.323E-02
1.000E+01	3.109E+00	3.110E+00	3.117E+00	3.131E+00	3.136E+00	3.085E+00	2.048E+00	5.324E-01	8.992E-02
1.000E+02	5.370E+00	5.378E+00	5.397E+00	5.411E+00	5.363E+00	4.248E+00	2.250E+00	1.215E+00	1.053E+00
1.000E+03	7.658E+00	7.677E+00	7.697E+00	7.658E+00	6.540E+00	4.469E+00	3.300E+00	3.140E+00	3.128E+00
1.000E+04	9.961E+00	9.982E+00	9.947E+00	8.837E+00	6.763E+00	5.579E+00	5.420E+00	5.408E+00	5.407E+00

PUITS A PENETRATION COMPLETE ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.90

TABLFAU 1 K

ABAUUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



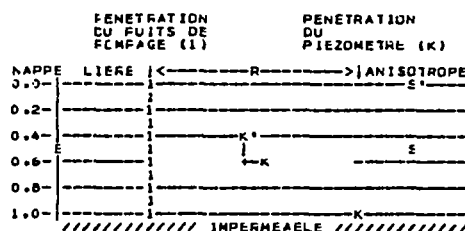
LOG S/S* = -2.0

LOG K*R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.471E-02	2.470E-02	2.471E-02	2.473E-02	2.484E-02	2.490E-02	2.490E-02	2.410E-02	4.773E-03	
1.000E+00	1.036E+00	1.036E+00	1.036E+00	1.040E+00	1.044E+00	1.044E+00	1.032E+00	4.642E-01	1.445E-02	
1.000E+01	3.111E+00	3.112E+00	3.119E+00	3.132E+00	3.136E+00	3.120E+00	2.173E+00	5.761E-01	9.369E-02	
1.000E+02	5.374E+00	5.382E+00	5.399E+00	5.412E+00	5.399E+00	4.394E+00	2.360E+00	1.243E+00	1.056E+00	
1.000E+03	7.664E+00	7.681E+00	7.699E+00	7.695E+00	6.688E+00	4.595E+00	3.339E+00	3.144E+00	3.128E+00	
1.000E+04	9.967E+00	9.986E+00	9.986E+00	8.986E+00	6.890E+00	5.619E+00	5.424E+00	5.408E+00	5.407E+00	

PUITS A PENETRATION COMPLETE ET PIEZOMETRE FONCTIONNEL A LA BASE DE LA NAPPE
 ABAQUE POUR L'INTERPRETATION DE FCMAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTEN - STRELETSCVA

TABLEAU 1 K



LOG S/S' = -2.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0 2.0 3.0

TT/R25	R A B A T T E M E N T S					R E C U I T S									
1.000E-01	2.471E-02	2.473E-02	2.471E-02	2.473E-02	2.484E-02	2.493E-02	2.490E-02	2.490E-02	2.424E-02	4.617E-03	0.0				0.0
3.162E-01	2.134E-01	3.134E-01	3.135E-01	3.141E-01	3.158E-01	3.159E-01	3.159E-01	3.159E-01	2.425E-01	9.611E-03	0.0				0.0
1.000E+00	1.036E+00	1.036E+00	1.037E+00	1.040E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	4.655E-01	1.021E-02	0.0				0.0
3.162E+00	2.022E+00	2.022E+00	2.024E+00	2.033E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	5.031E-01	1.135E-02	6.514E-07				0.0
1.000E+01	3.112E+00	3.112E+00	3.119E+00	3.132E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	2.016E-01	1.535E-02	2.136E-05				0.0
3.162E+01	4.237E+00	4.240E+00	4.253E+00	4.266E+00	4.270E+00	4.270E+00	4.270E+00	4.270E+00	2.215E+00	3.022E-02	8.555E-04	7.752E-05			0.0
1.000E+02	5.375E+00	5.382E+00	5.395E+00	5.412E+00	5.432E+00	5.432E+00	5.432E+00	5.432E+00	2.222E+00	5.624E-02	3.225E-02	2.555E-02			0.0
3.162E+02	6.518E+00	6.531E+00	6.548E+00	6.561E+00	6.570E+00	6.570E+00	6.570E+00	6.570E+00	2.266E+00	3.720E-01	3.215E-01	3.161E-01			0.0
1.000E+03	7.664E+00	7.682E+00	7.699E+00	7.724E+00	7.746E+00	7.746E+00	7.746E+00	7.746E+00	2.322E+00	1.042E+00	1.042E+00	1.042E+00			0.0
3.162E+03	8.815E+00	8.833E+00	8.850E+00	8.866E+00	8.873E+00	8.873E+00	8.873E+00	8.873E+00	2.382E+00	2.042E+00	2.042E+00	2.042E+00			0.0
1.000E+04	9.968E+00	9.986E+00	9.999E+00	1.000E+01	1.000E+01	1.000E+01	1.000E+01	1.000E+01	2.432E+00	3.137E+00	3.137E+00	3.137E+00			0.0
3.162E+04	1.115E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	2.482E+00	4.270E+00	4.270E+00	4.270E+00			0.0
1.000E+05	1.222E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	2.532E+00	5.416E+00	5.416E+00	5.416E+00			0.0
3.162E+05	1.351E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	2.582E+00	6.566E+00	6.566E+00	6.566E+00			0.0
1.000E+06	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	2.632E+00	7.716E+00	7.716E+00	7.716E+00			0.0

LOG S/S' = -2.5

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R25	R A B A T T E M E N T S					R E C U I T S									
1.000E-01	2.471E-02	2.473E-02	2.471E-02	2.473E-02	2.484E-02	2.493E-02	2.490E-02	2.490E-02	2.424E-02	4.625E-03	0.0				0.0
3.162E-01	2.134E-01	3.134E-01	3.135E-01	3.141E-01	3.158E-01	3.159E-01	3.159E-01	3.159E-01	2.426E-01	1.002E-02					0.0
1.000E+00	1.036E+00	1.036E+00	1.037E+00	1.040E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	4.655E-01	1.021E-02					0.0
3.162E+00	2.022E+00	2.022E+00	2.024E+00	2.033E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	5.031E-01	1.135E-02					0.0
1.000E+01	3.112E+00	3.112E+00	3.119E+00	3.132E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	2.016E-01	1.535E-02					0.0
3.162E+01	4.237E+00	4.240E+00	4.253E+00	4.266E+00	4.270E+00	4.270E+00	4.270E+00	4.270E+00	2.215E+00	3.022E-02					0.0
1.000E+02	5.375E+00	5.382E+00	5.395E+00	5.412E+00	5.432E+00	5.432E+00	5.432E+00	5.432E+00	2.222E+00	5.624E-02					0.0
3.162E+02	6.518E+00	6.531E+00	6.548E+00	6.561E+00	6.570E+00	6.570E+00	6.570E+00	6.570E+00	2.266E+00	3.720E-01					0.0
1.000E+03	7.664E+00	7.682E+00	7.699E+00	7.724E+00	7.746E+00	7.746E+00	7.746E+00	7.746E+00	2.322E+00	1.042E+00					0.0
3.162E+03	8.815E+00	8.833E+00	8.850E+00	8.866E+00	8.873E+00	8.873E+00	8.873E+00	8.873E+00	2.382E+00	2.042E+00					0.0
1.000E+04	9.968E+00	9.986E+00	9.999E+00	1.000E+01	1.000E+01	1.000E+01	1.000E+01	1.000E+01	2.432E+00	3.137E+00					0.0
3.162E+04	1.115E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	2.482E+00	4.270E+00					0.0
1.000E+05	1.222E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	2.532E+00	5.416E+00					0.0
3.162E+05	1.351E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	2.582E+00	6.566E+00					0.0
1.000E+06	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	2.632E+00	7.716E+00					0.0

LOG S/S' = -2.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0 2.0 3.0

TT/R25	R A B A T T E M E N T S					R E C U I T S									
1.000E-01	2.471E-02	2.473E-02	2.471E-02	2.473E-02	2.484E-02	2.493E-02	2.490E-02	2.490E-02	2.424E-02	4.625E-03	0.0				2.357E-07
3.162E-01	2.134E-01	3.134E-01	3.135E-01	3.141E-01	3.158E-01	3.159E-01	3.159E-01	3.159E-01	2.427E-01	1.070E-02	1.143E-07				4.761E-07
1.000E+00	1.036E+00	1.036E+00	1.037E+00	1.040E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	4.655E-01	1.021E-02	1.563E-05				0.0
3.162E+00	2.022E+00	2.022E+00	2.024E+00	2.033E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	5.031E-01	1.135E-02	8.065E-04	7.271E-05			0.0
1.000E+01	3.112E+00	3.112E+00	3.119E+00	3.132E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	2.016E-01	1.535E-02	3.155E-02	2.493E-02			0.0
3.162E+01	4.237E+00	4.240E+00	4.253E+00	4.266E+00	4.270E+00	4.270E+00	4.270E+00	4.270E+00	2.215E+00	3.022E-02	3.175E-01	3.125E-01			0.0
1.000E+02	5.375E+00	5.382E+00	5.395E+00	5.412E+00	5.432E+00	5.432E+00	5.432E+00	5.432E+00	2.222E+00	5.624E-02	1.050E+00	1.032E+00			0.0
3.162E+02	6.518E+00	6.531E+00	6.548E+00	6.561E+00	6.570E+00	6.570E+00	6.570E+00	6.570E+00	2.266E+00	3.720E-01	2.026E+00	2.026E+00			0.0
1.000E+03	7.664E+00	7.682E+00	7.699E+00	7.724E+00	7.746E+00	7.746E+00	7.746E+00	7.746E+00	2.322E+00	1.042E+00	3.127E+00	3.127E+00			0.0
3.162E+03	8.815E+00	8.833E+00	8.850E+00	8.866E+00	8.873E+00	8.873E+00	8.873E+00	8.873E+00	2.382E+00	2.042E+00	4.261E+00	4.261E+00			0.0
1.000E+04	9.968E+00	9.986E+00	9.999E+00	1.000E+01	1.000E+01	1.000E+01	1.000E+01	1.000E+01	2.432E+00	3.137E+00	5.407E+00	5.407E+00			0.0
3.162E+04	1.115E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	1.116E+01	2.482E+00	4.270E+00	6.556E+00	6.556E+00			0.0
1.000E+05	1.222E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	1.223E+01	2.532E+00	5.416E+00	7.707E+00	7.707E+00			0.0
3.162E+05	1.351E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	1.352E+01	2.582E+00	6.566E+00	8.555E+00	8.555E+00			0.0
1.000E+06	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	1.472E+01	2.632E+00	7.716E+00	1.001E+01	1.001E+01			0.0

LOG S/S' = -2.0

LOG K'R2/KB2 4.0

TT/R25 R A B A T T E M E N T S R E C U I T S

1.000E-01	2.132E-08														
3.162E-01	0.0														
1.000E+00	0.0														
3.162E+00	4.119E-05														
1.000E+01	2.418E-02														
3.162E+01	2.115E-01														
1.000E+02	1.037E+00														
3.162E+02	2.329E+00														
1.000E+03	3.127E+00														
3.162E+03	4.261E+00														
1.000E+04	5.467E+00														
3.162E+04	6.566E+00														
1.000E+05	7.707E+00														
3.162E+05	8.555E+00														
1.000E+06	1.001E+01														

LOG S/S' = -1.5

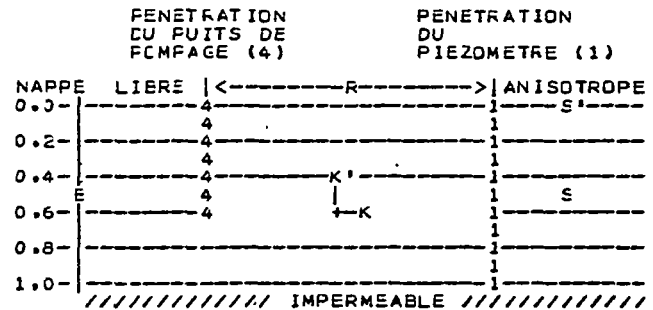
LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R25	R A B A T T E M E N T S					R E C U I T S									
1.000E-01	2.471E-02	2.473E-02	2.471E-02	2.473E-02	2.485E-02	2.491E-02	2.490E-02	2.490E-02	2.424E-02	4.927E-03					
3.162E-01	3.134E-01	3.134E-01	3.135E-01	3.141E-01	3.158E-01	3.159E-01	3.159E-01	3.159E-01	2.431E-01	1.208E-02					
1.000E+00	1.036E+00	1.036E+00	1.037E+00	1.040E+00	1.044E+00	1.045E+00	1.045E+00	1.045E+00	1.027E+00	6.672E-01	6.632E-01				
1.000E+01	3.112E+00	2.112E+00	2.119E+00	3.132E+00	3.136E+00	3.132E+00	2.208E+00	7.555E-01	3.600E-02						
1.000E+02	3.375E+00	5.382E+00	7.333E+00	4.658E+00	4.658E+00	4.658E+00	4.658E+00	4.658E+00	4.658E+00	4.658E+00	4.658E+00				
1.000E+03	7.605E+00	5.382E+00	7.605E+00	7.605E+00	7.730E+00	6.594E+00	6.594E+00	6.594E+00	6.594E+00	6.594E+00	6.594E+00				
1.000E+04	5.656E+00	5.656E+00	5.656E+00	5.656E+00	5.656E+00	5.656E+00	5.656E+00	5.656E+00	5.656E+00	5.656E+00	5.656E+00				

ICCE - CNRS - CENTRE INTER REGIONAL DE CALCUL ELECTRONIQUE - CIRCE CNRS - CENTRE INTER REGIONAL DE CALCUL ELECTRONIQUE - CIRCE UNIS - CENTRE INTER REGIONAL DE CALCUL

PUITS A PENETRATION DE 0.0 A 0.6 ET PIEZOMETRE COMPLET
ABAQUE POUR L'INTERPRETATION DE FOMPAGES EN NAPPE LIBRE ANISOTROPE.
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCOVA

TABLEAU 4 1



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.467E-02	2.447E-02	2.359E-02	2.077E-02	1.277E-02	2.078E-03
3.162E-01	3.133E-01	3.132E-01	3.132E-01	3.124E-01	3.076E-01	2.895E-01	2.327E-01	1.109E-01	4.247E-03
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.112E-01	6.413E-01	2.090E-01	4.282E-03
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.998E+00	1.915E+00	1.651E+00	1.002E+00	2.225E-01	4.794E-03
1.000E+01	3.110E+00	3.109E+00	3.099E+00	3.046E+00	2.856E+00	2.276E+00	1.160E+00	2.296E-01	6.352E-03
1.000E+02	5.370E+00	5.359E+00	5.299E+00	5.072E+00	4.356E+00	2.861E+00	1.217E+00	3.211E-01	6.168E-02
1.000E+03	7.640E+00	7.578E+00	7.342E+00	6.586E+00	4.954E+00	2.973E+00	1.618E+00	1.168E+00	1.074E+00
1.000E+04	9.863E+00	9.625E+00	8.860E+00	7.190E+00	5.114E+00	3.739E+00	3.603E+00	3.425E+00	3.230E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.467E-02	2.448E-02	2.360E-02	2.080E-02	1.278E-02	2.052E-03
3.162E-01	3.133E-01	3.132E-01	3.132E-01	3.124E-01	3.076E-01	2.896E-01	2.328E-01	1.111E-01	4.279E-03
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.113E-01	6.417E-01	2.102E-01	4.658E-03
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.998E+00	1.915E+00	1.651E+00	1.002E+00	2.287E-01	6.232E-03
1.000E+01	3.110E+00	3.109E+00	3.099E+00	3.046E+00	2.857E+00	2.277E+00	1.168E+00	2.504E-01	1.364E-02
1.000E+02	5.370E+00	5.359E+00	5.299E+00	5.072E+00	4.359E+00	2.882E+00	1.316E+00	5.433E-01	3.341E-01
1.000E+03	7.640E+00	7.578E+00	7.343E+00	6.590E+00	4.958E+00	3.181E+00	2.364E+00	2.236E+00	2.103E+00
1.000E+04	9.863E+00	9.626E+00	8.866E+00	7.236E+00	5.413E+00	4.808E+00	4.932E+00	4.615E+00	4.378E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.467E-02	2.448E-02	2.362E-02	2.088E-02	1.282E-02	1.969E-03
3.162E-01	3.133E-01	3.132E-01	3.132E-01	3.125E-01	3.076E-01	2.896E-01	2.331E-01	1.115E-01	4.389E-03
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.116E-01	6.421E-01	2.135E-01	5.864E-03
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.998E+00	1.915E+00	1.652E+00	1.002E+00	2.469E-01	1.212E-02
1.000E+01	3.110E+00	3.109E+00	3.099E+00	3.046E+00	2.857E+00	2.282E+00	1.195E+00	3.162E-01	5.554E-02
1.000E+02	5.370E+00	5.359E+00	5.299E+00	5.073E+00	4.368E+00	2.947E+00	1.610E+00	1.160E+00	1.067E+00
1.000E+03	7.640E+00	7.578E+00	7.344E+00	6.604E+00	5.091E+00	3.731E+00	3.594E+00	3.415E+00	3.221E+00
1.000E+04	9.863E+00	9.628E+00	8.883E+00	7.367E+00	6.080E+00	6.193E+00	6.180E+00	5.782E+00	5.525E+00

LOG S/S' = -1.5

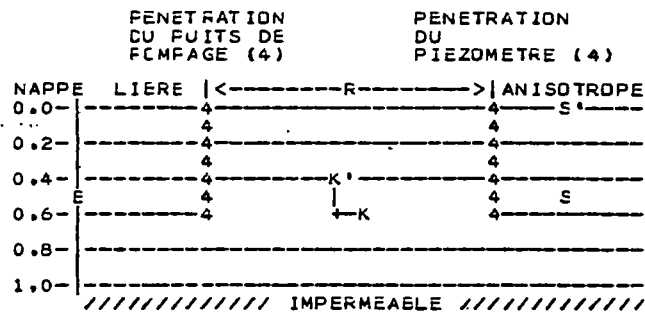
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.467E-02	2.449E-02	2.369E-02	2.113E-02	1.293E-02	1.711E-03
3.162E-01	3.133E-01	3.132E-01	3.132E-01	3.125E-01	3.076E-01	2.899E-01	2.340E-01	1.127E-01	4.829E-03
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.029E+00	1.002E+00	9.125E-01	6.474E-01	2.257E-01	1.145E-02
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.998E+00	1.916E+00	1.655E+00	1.029E+00	2.046E-01	5.590E-02
1.000E+01	3.110E+00	3.109E+00	3.099E+00	3.047E+00	2.859E+00	2.298E+00	1.279E+00	5.247E-01	3.200E-01
1.000E+02	5.370E+00	5.359E+00	5.299E+00	5.075E+00	4.396E+00	3.140E+00	2.337E+00	2.207E+00	2.075E+00
1.000E+03	7.640E+00	7.579E+00	7.345E+00	6.644E+00	5.372E+00	4.783E+00	4.903E+00	4.564E+00	4.345E+00
1.000E+04	9.864E+00	9.633E+00	8.932E+00	7.687E+00	7.197E+00	7.536E+00	7.363E+00	6.525E+00	6.655E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.470E-02	2.469E-02	2.469E-02	2.468E-02	2.453E-02	2.393E-02	2.193E-02	1.321E-02	9.217E-04
3.162E-01	3.133E-01	3.132E-01	3.132E-01	3.125E-01	3.077E-01	2.907E-01	2.368E-01	1.165E-01	6.578E-03
1.000E+00	1.035E+00	1.035E+00	1.035E+00	1.030E+00	1.003E+00	9.155E-01	6.607E-01	2.622E-01	4.441E-02
3.162E+00	2.021E+00	2.020E+00	2.018E+00	1.998E+00	1.918E+00	1.668E+00	1.092E+00	4.829E-01	2.683E-01
1.000E+01	3.110E+00	3.109E+00	3.102E+00	3.048E+00	2.866E+00	2.344E+00	1.522E+00	1.085E+00	9.552E-01
1.000E+02	5.370E+00	5.359E+00	5.301E+00	5.087E+00	4.480E+00	3.635E+00	3.505E+00	3.325E+00	3.125E+00
1.000E+03	7.640E+00	7.580E+00	7.364E+00	6.755E+00	5.984E+00	6.105E+00	6.088E+00	5.692E+00	5.445E+00
1.000E+04	9.866E+00	9.651E+00	8.957E+00	8.321E+00	8.540E+00	8.730E+00	8.479E+00	8.025E+00	7.761E+00

PUITS A PENETRATION DE 0.0 A 0.6 ET PIEZOMETRE OUVERT DE 0.0 A 0.6
ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCOVA

TABLEAU 4 4



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.058E-02	4.057E-02	4.058E-02	4.091E-02	4.036E-02	3.815E-02	3.108E-02	1.215E-02	1.437E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.178E-01	5.055E-01	4.603E-01	3.184E-01	8.376E-02	2.957E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.408E+00	7.510E-01	1.513E-01	3.146E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.429E+00	1.020E+00	1.613E-01	3.738E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.527E+00	3.100E+00	1.131E+00	1.674E-01	5.638E-03
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.164E+00	6.401E+00	3.532E+00	1.181E+00	2.491E-01	6.413E-02
1.000E+03	1.267E+01	1.251E+01	1.192E+01	1.006E+01	6.844E+00	3.633E+00	1.560E+00	1.025E+00	1.036E+00
1.000E+04	1.631E+01	1.571E+01	1.382E+01	1.051E+01	6.997E+00	4.378E+00	3.424E+00	3.148E+00	3.134E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.058E-02	4.057E-02	4.058E-02	4.091E-02	4.044E-02	3.815E-02	3.107E-02	1.215E-02	1.442E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.178E-01	5.056E-01	4.605E-01	3.184E-01	8.387E-02	3.066E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.403E+00	7.513E-01	1.524E-01	3.662E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.429E+00	1.022E+00	1.665E-01	5.744E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.527E+00	3.102E+00	1.139E+00	1.858E-01	1.459E-02
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.165E+00	6.404E+00	3.552E+00	1.275E+00	4.504E-01	2.273E-01
1.000E+03	1.267E+01	1.251E+01	1.193E+01	1.006E+01	6.877E+00	3.838E+00	2.262E+00	2.019E+00	2.030E+00
1.000E+04	1.631E+01	1.571E+01	1.383E+01	1.055E+01	7.290E+00	5.399E+00	4.655E+00	4.292E+00	4.267E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.058E-02	4.057E-02	4.058E-02	4.091E-02	4.044E-02	3.815E-02	3.107E-02	1.216E-02	1.459E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.178E-01	5.056E-01	4.605E-01	3.185E-01	8.422E-02	3.418E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.408E+00	7.522E-01	1.558E-01	5.444E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.430E+00	1.028E+00	1.828E-01	1.410E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.528E+00	3.106E+00	1.164E+00	2.449E-01	6.256E-02
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.165E+00	6.412E+00	3.615E+00	1.551E+00	1.018E+00	1.029E+00
1.000E+03	1.267E+01	1.251E+01	1.193E+01	1.007E+01	6.978E+00	4.369E+00	3.410E+00	2.139E+00	3.125E+00
1.000E+04	1.631E+01	1.571E+01	1.384E+01	1.068E+01	7.938E+00	6.697E+00	5.834E+00	5.435E+00	5.407E+00

LOG S/S' = -1.5

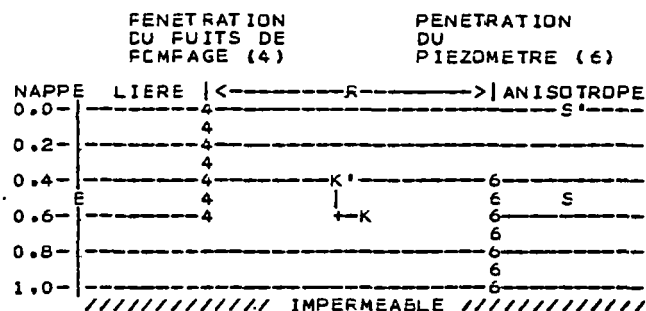
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.058E-02	4.057E-02	4.058E-02	4.091E-02	4.044E-02	3.815E-02	3.108E-02	1.218E-02	1.512E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.178E-01	5.056E-01	4.605E-01	3.187E-01	8.531E-02	4.594E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.408E+00	7.552E-01	1.665E-01	1.266E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.432E+00	1.046E+00	2.349E-01	5.852E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.529E+00	3.119E+00	1.242E+00	4.343E-01	3.144E-01
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.168E+00	6.438E+00	3.802E+00	2.236E+00	1.593E+00	2.005E+00
1.000E+03	1.267E+01	1.252E+01	1.193E+01	1.011E+01	7.253E+00	5.371E+00	4.627E+00	4.265E+00	4.240E+00
1.000E+04	1.631E+01	1.572E+01	1.389E+01	1.099E+01	9.008E+00	7.545E+00	6.987E+00	6.576E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.058E-02	4.057E-02	4.058E-02	4.091E-02	4.043E-02	3.815E-02	3.109E-02	1.225E-02	1.643E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.178E-01	5.056E-01	4.606E-01	3.194E-01	8.874E-02	8.804E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.409E+00	7.643E-01	2.003E-01	4.853E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.091E+00	2.440E+00	1.103E+00	3.580E-01	2.852E-01
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.003E+00	4.533E+00	3.159E+00	1.471E+00	9.521E-01	9.625E-01
1.000E+02	8.910E+00	8.884E+00	8.734E+00	8.176E+00	6.514E+00	4.278E+00	3.225E+00	2.056E+00	2.045E+00
1.000E+03	1.267E+01	1.252E+01	1.194E+01	1.022E+01	7.844E+00	6.610E+00	5.748E+00	5.255E+00	5.232E+00
1.000E+04	1.631E+01	1.573E+01	1.401E+01	1.161E+01	1.026E+01	9.072E+00	8.070E+00	7.664E+00	7.641E+00

PUITS A PENETRATION DE 0.0 A 0.6 ET PIEZOMETRE OUVERT DE 0.4 A 1.0
 ABAQUE POUR L'INTERPRETATION DE FCMAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCOVA

TABEAU 4 6



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.467E-02	2.842E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.440E-01	5.804E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.235E-01	2.759E-01	6.059E-03
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.051E+00	2.541E-01	7.001E-03
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.829E+00	1.303E+00	3.011E-01	1.010E-02
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.104E+00	2.588E+00	1.345E+00	3.915E-01	6.127E-02
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.293E+00	4.382E+00	2.635E+00	1.562E+00	1.111E+00	1.051E+00
1.000E+04	5.567E+00	5.573E+00	5.563E+00	5.152E+00	3.919E+00	2.887E+00	2.786E+00	3.108E+00	3.136E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.467E-02	2.849E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.441E-01	5.969E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.235E-01	2.770E-01	6.882E-03
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.051E+00	2.592E-01	9.561E-03
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.829E+00	1.307E+00	3.218E-01	2.208E-02
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.104E+00	2.593E+00	1.359E+00	5.550E-01	5.537E-01
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.293E+00	4.383E+00	2.698E+00	1.977E+00	2.021E+00	2.036E+00
1.000E+04	5.567E+00	5.573E+00	5.563E+00	5.157E+00	3.983E+00	3.348E+00	3.855E+00	4.238E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.466E-02	2.874E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.443E-01	6.498E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.237E-01	2.805E-01	9.526E-03
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.052E+00	2.178E-01	2.142E-02
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.829E+00	1.318E+00	3.661E-01	7.542E-02
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.104E+00	2.603E+00	1.553E+00	1.111E+00	1.044E+00
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.293E+00	4.382E+00	2.678E+00	2.777E+00	3.095E+00	3.127E+00
1.000E+04	5.567E+00	5.573E+00	5.563E+00	5.172E+00	4.166E+00	4.194E+00	4.986E+00	5.377E+00	5.407E+00

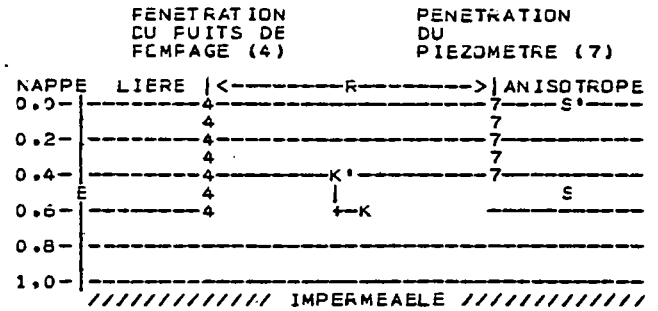
LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.466E-02	2.946E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.451E-01	8.225E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.241E-01	2.912E-01	1.945E-02
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.059E+00	2.733E-01	7.511E-02
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.830E+00	1.355E+00	5.760E-01	3.402E-01
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.105E+00	2.652E+00	1.950E+00	1.595E+00	2.010E+00
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.293E+00	4.386E+00	2.779E+00	3.827E+00	4.211E+00	4.241E+00
1.000E+04	5.567E+00	5.573E+00	5.564E+00	5.217E+00	4.618E+00	5.263E+00	6.125E+00	6.517E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.404E-02	1.470E-02	3.149E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.476E-01	1.410E-02
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.253E-01	3.238E-01	6.277E-02
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.116E+00	5.233E-01	3.098E-01
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.832E+00	1.455E+00	1.042E+00	5.778E-01
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.107E+00	2.779E+00	2.692E+00	3.016E+00	3.047E+00
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.293E+00	4.066E+00	4.107E+00	4.903E+00	5.297E+00	5.332E+00
1.000E+04	5.567E+00	5.573E+00	5.566E+00	5.346E+00	5.405E+00	6.341E+00	7.204E+00	7.604E+00	7.641E+00

ABaque POUR L'INTERPRETATION DE FOMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.098E-02	4.097E-02	4.098E-02	4.091E-02	4.036E-02	3.814E-02	3.075E-02	9.837E-03	1.016E-03
3.162E-01	5.199E-01	5.198E-01	5.197E-01	5.178E-01	5.055E-01	4.604E-01	3.015E-01	6.128E-02	2.094E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.402E+00	6.675E-01	1.083E-01	2.292E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.374E+00	8.637E-01	1.158E-01	2.945E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.520E+00	2.945E+00	9.412E-01	1.216E-01	5.200E-03
1.000E+02	9.910E+00	8.884E+00	6.733E+00	8.157E+00	6.233E+00	3.258E+00	9.878E-01	1.596E-01	6.367E-02
1.000E+03	1.267E+01	1.251E+01	1.192E+01	9.889E+00	6.556E+00	3.356E+00	1.359E+00	9.480E-01	1.016E+00
1.000E+04	1.621E+01	1.570E+01	1.365E+01	1.022E+01	6.705E+00	4.093E+00	3.176E+00	3.014E+00	3.027E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.098E-02	4.097E-02	4.098E-02	4.091E-02	4.043E-02	3.814E-02	3.073E-02	9.843E-03	1.036E-03
3.162E-01	5.199E-01	5.198E-01	5.197E-01	5.178E-01	5.056E-01	4.604E-01	3.015E-01	6.140E-02	2.234E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.402E+00	6.677E-01	1.094E-01	2.882E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.374E+00	8.655E-01	1.208E-01	5.120E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.520E+00	2.946E+00	9.452E-01	1.392E-01	1.433E-02
1.000E+02	9.910E+00	8.884E+00	6.733E+00	8.157E+00	6.236E+00	3.278E+00	1.080E+00	3.530E-01	3.221E-01
1.000E+03	1.267E+01	1.251E+01	1.192E+01	9.893E+00	6.589E+00	3.559E+00	2.048E+00	1.913E+00	1.995E+00
1.000E+04	1.621E+01	1.570E+01	1.366E+01	1.027E+01	6.996E+00	5.100E+00	4.376E+00	4.135E+00	4.213E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.098E-02	4.097E-02	4.098E-02	4.091E-02	4.043E-02	3.811E-02	3.068E-02	9.864E-03	1.059E-03
3.162E-01	5.199E-01	5.198E-01	5.197E-01	5.178E-01	5.056E-01	4.603E-01	3.014E-01	6.180E-02	2.682E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.402E+00	6.685E-01	1.129E-01	4.874E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.374E+00	8.711E-01	1.366E-01	1.350E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.520E+00	2.950E+00	9.743E-01	1.958E-01	6.240E-02
1.000E+02	9.910E+00	8.884E+00	6.733E+00	8.157E+00	6.243E+00	3.341E+00	1.352E+00	5.416E-01	1.000E+00
1.000E+03	1.267E+01	1.251E+01	1.192E+01	9.905E+00	6.689E+00	4.084E+00	3.168E+00	3.006E+00	3.072E+00
1.000E+04	1.621E+01	1.571E+01	1.367E+01	1.039E+01	7.639E+00	6.368E+00	5.527E+00	5.270E+00	5.349E+00

LOG S/S' = -1.5

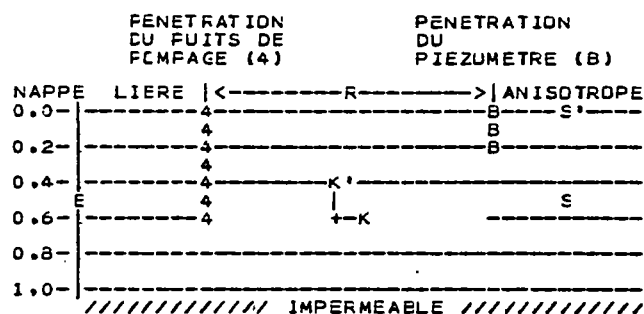
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.098E-02	4.097E-02	4.098E-02	4.091E-02	4.042E-02	3.804E-02	3.053E-02	9.932E-03	1.293E-03
3.162E-01	5.199E-01	5.198E-01	5.197E-01	5.178E-01	5.055E-01	4.601E-01	3.012E-01	6.307E-02	4.146E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.402E+00	6.708E-01	1.237E-01	1.261E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.375E+00	8.890E-01	1.870E-01	5.899E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.520E+00	2.962E+00	1.052E+00	3.784E-01	3.057E-01
1.000E+02	9.910E+00	8.884E+00	6.733E+00	8.159E+00	6.267E+00	3.526E+00	2.023E+00	1.889E+00	1.970E+00
1.000E+03	1.267E+01	1.251E+01	1.192E+01	9.941E+00	6.962E+00	5.072E+00	4.350E+00	4.113E+00	4.187E+00
1.000E+04	1.621E+01	1.571E+01	1.372E+01	1.070E+01	8.694E+00	7.579E+00	6.660E+00	6.405E+00	6.482E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.098E-02	4.097E-02	4.098E-02	4.091E-02	4.037E-02	3.782E-02	3.005E-02	1.019E-02	1.844E-03
3.162E-01	5.199E-01	5.198E-01	5.197E-01	5.178E-01	5.054E-01	4.595E-01	3.006E-01	6.712E-02	9.163E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.401E+00	6.782E-01	1.579E-01	4.525E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.295E+00	3.089E+00	2.383E+00	9.439E-01	3.458E-01	2.819E-01
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.522E+00	2.998E+00	1.277E+00	8.813E-01	9.454E-01
1.000E+02	9.910E+00	8.884E+00	6.733E+00	8.165E+00	6.339E+00	3.937E+00	3.067E+00	2.928E+00	3.001E+00
1.000E+03	1.267E+01	1.251E+01	1.193E+01	1.004E+01	7.548E+00	6.282E+00	5.444E+00	5.196E+00	5.277E+00
1.000E+04	1.621E+01	1.572E+01	1.383E+01	1.131E+01	9.919E+00	8.677E+00	7.735E+00	7.494E+00	7.522E+00

PUITS A PENETRATION DE 0.0 A 0.6 ET PIEZOMETRE OUVERT DE 0.0 A 0.2
 ABAQUE POUR L'INTERPRETATION DE FOMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 4 B



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0			1.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
TT/R2S	R			A			B			A			T			T			E			M			E			N			T			S			R			E			C			U			I			T			S																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
1.000E-01	4.046E-02			4.045E-02			4.045E-02			4.045E-02			4.033E-02			3.929E-02			3.488E-02			2.158E-02			5.597E-03			5.313E-04																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0		-6.0		-5.0		-4.0		-3.0		-2.0		-1.0		0.0		1.0			
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S	
1.000E-01	4.046E-02			4.045E-02				4.045E-02			4.032E-02		3.928E-02		3.486E-02		2.154E-02		5.615E-03	5.653E-04
3.162E-01	5.133E-01			5.132E-01				5.128E-01			5.092E-01		4.845E-01		3.946E-01		1.946E-01		3.279E-02	1.282E-03
1.000E+00	1.656E+00			1.656E+00				1.653E+00			1.667E+00		1.530E+00		1.093E+00		4.083E-01		5.611E-02	1.959E-03
3.162E+00	3.311E+00			3.309E+00				3.295E+00			3.195E+00		2.784E+00		1.728E+00		5.147E-01		6.648E-02	4.289E-03
1.000E+01	5.095E+00			5.089E+00				5.042E+00			4.777E+00		3.858E+00		2.062E+00		5.620E-01		6.411E-02	1.367E-02
1.000E+02	6.793E+00			6.741E+00				6.439E+00			7.334E+00		4.934E+00		2.250E+00		6.877E-01		3.288E-01	3.160E-01
1.000E+03	1.248E+01			1.217E+01				1.102E+01			8.424E+00		5.142E+00		2.525E+00		1.641E+00		1.607E+00	1.960E+00
1.000E+04	1.591E+01			1.475E+01				1.211E+01			8.649E+00		5.543E+00		4.051E+00		3.916E+00		3.989E+00	4.160E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	4.046E-02	4.045E-02	4.045E-02	4.045E-02	4.032E-02	3.927E-02	3.479E-02	2.165E-02	5.676E-03	6.722E-04									
3.162E-01	5.133E-01	5.132E-01	5.132E-01	5.128E-01	5.092E-01	4.845E-01	3.944E-01	1.944E-01	3.330E-02	1.810E-03									
1.000E+00	1.656E+00	1.656E+00	1.656E+00	1.653E+00	1.667E+00	1.530E+00	1.097E+00	4.095E-01	6.166E-02	4.053E-03									
3.162E+00	3.311E+00	3.309E+00	3.309E+00	3.295E+00	3.195E+00	2.783E+00	1.726E+00	5.204E-01	6.195E-02	1.329E-02									
1.000E+01	5.095E+00	5.089E+00	5.089E+00	5.042E+00	4.777E+00	3.858E+00	2.066E+00	5.871E-01	1.388E-01	6.145E-02									
1.000E+02	6.793E+00	6.741E+00	6.741E+00	6.439E+00	7.334E+00	4.941E+00	2.312E+00	9.560E-01	6.618E-01	9.857E-01									
1.000E+03	1.248E+01	1.217E+01	1.217E+01	1.102E+01	8.435E+00	5.241E+00	3.047E+00	2.739E+00	2.875E+00	3.033E+00									
1.000E+04	1.591E+01	1.476E+01	1.476E+01	1.213E+01	8.777E+00	6.182E+00	5.295E+00	5.040E+00	5.109E+00	5.292E+00									

LOG S/S' = -1.5

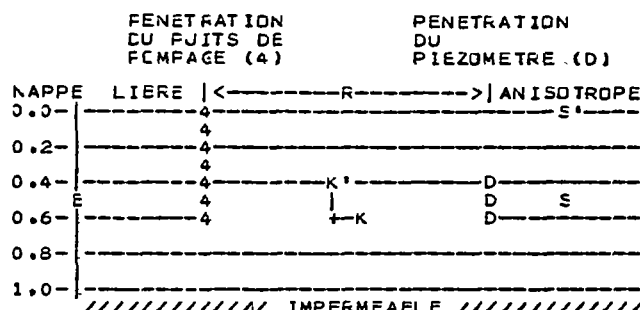
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	4.046E-02	4.045E-02	4.045E-02	4.045E-02	4.031E-02	3.922E-02	3.459E-02	2.154E-02	5.672E-03	1.001E-03									
3.162E-01	5.133E-01	5.132E-01	5.132E-01	5.128E-01	5.092E-01	4.844E-01	3.938E-01	1.939E-01	3.494E-02	3.518E-03									
1.000E+00	1.656E+00	1.656E+00	1.656E+00	1.653E+00	1.666E+00	1.529E+00	1.096E+00	4.115E-01	7.297E-02	1.218E-02									
3.162E+00	3.311E+00	3.309E+00	3.309E+00	3.295E+00	3.195E+00	2.783E+00	1.726E+00	5.384E-01	1.314E-01	5.629E-02									
1.000E+01	5.095E+00	5.089E+00	5.089E+00	5.042E+00	4.776E+00	3.857E+00	2.076E+00	6.645E-01	3.161E-01	3.042E-01									
1.000E+02	6.793E+00	6.741E+00	6.741E+00	6.439E+00	7.335E+00	4.964E+00	2.496E+00	1.618E+00	1.765E+00	1.936E+00									
1.000E+03	1.248E+01	1.217E+01	1.217E+01	1.102E+01	8.469E+00	5.513E+00	4.323E+00	3.891E+00	3.966E+00	4.135E+00									
1.000E+04	1.591E+01	1.476E+01	1.476E+01	1.217E+01	9.066E+00	7.225E+00	6.476E+00	6.146E+00	6.239E+00	6.425E+00									

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0				-6.0				-5.0				-4.0				-3.0				-2.0				-1.0				0.0		1.0		
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S	R	E	C	U	I	T	S	R	E	C	U	I	T	S
1.000E-01	4.046E-02			4.045E-02				4.044E-02			4.029E-02		3.907E-02			3.396E-02			2.058E-02			6.553E-03			1.937E-03								
3.162E-01	5.133E-01			5.132E-01				5.128E-01			5.091E-01		4.839E-01			3.920E-01			1.923E-01			4.021E-02			9.195E-03								
1.000E+00	1.656E+00			1.656E+00				1.653E+00			1.666E+00		1.528E+00			1.093E+00			4.182E-01			1.086E-01			4.924E-02								
3.162E+00	3.311E+00			3.309E+00				3.295E+00			3.194E+00		2.783E+00			1.726E+00			5.938E-01			2.679E-01			2.776E-01								
1.000E+01	5.095E+00			5.089E+00				5.042E+00			4.775E+00		3.855E+00			2.103E+00			8.903E-01			6.076E-01			9.264E-01								
1.000E+02	6.793E+00			6.741E+00				6.438E+00			7.336E+00		5.030E+00			2.964E+00			2.664E+00			2.804E+00			2.958E+00								
1.000E+03	1.248E+01			1.217E+01				1.103E+01			8.563E+00		6.094E+00			5.212E+00			4.964E+00			5.042E+00			5.223E+00								
1.000E+04	1.591E+01			1.477E+01				1.228E+01			9.690E+00		8.428E+00			7.549E+00			7.224E+00			7.328E+00			7.524E+00								

PUITS A PENETRATION DE 0.0 A 0.6 ET PIEZOMETRE OUVERT DE 0.4 A 0.6

TABLEAU 4 D

ABAQUE POUR L'INTERPRETATION DE FOMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.092E-02	4.036E-02	3.814E-02	3.170E-02	1.674E-02	2.344E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.606E-01	3.521E-01	1.287E-01	4.808E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	9.178E-01	2.371E-01	6.158E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.539E+00	1.333E+00	2.521E-01	6.242E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.410E+00	1.507E+00	2.564E-01	9.822E-03
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.180E+00	6.735E+00	4.071E+00	1.543E+00	3.392E-01	8.402E-02
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.039E+01	7.405E+00	4.112E+00	1.737E+00	5.945E-01	1.013E+00
1.000E+04	1.631E+01	1.573E+01	1.416E+01	1.106E+01	7.447E+00	4.338E+00	2.825E+00	2.647E+00	3.040E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.036E-02	3.814E-02	3.168E-02	1.672E-02	2.381E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.521E-01	1.287E-01	5.047E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	9.177E-01	2.380E-01	6.137E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.539E+00	1.333E+00	2.572E-01	9.758E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.410E+00	1.510E+00	2.768E-01	2.328E-02
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.180E+00	6.735E+00	4.075E+00	1.591E+00	5.218E-01	3.472E-01
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.039E+01	7.409E+00	4.168E+00	2.109E+00	1.824E+00	1.964E+00
1.000E+04	1.631E+01	1.573E+01	1.416E+01	1.107E+01	7.504E+00	4.752E+00	3.812E+00	3.535E+00	4.157E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.036E-02	3.813E-02	3.162E-02	1.667E-02	2.454E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.519E-01	1.289E-01	5.803E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	9.174E-01	2.410E-01	9.373E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.539E+00	1.334E+00	2.732E-01	2.268E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.410E+00	1.520E+00	3.343E-01	8.231E-02
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.180E+00	6.735E+00	4.083E+00	1.729E+00	5.883E-01	1.007E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.039E+01	7.422E+00	4.329E+00	2.827E+00	2.635E+00	3.031E+00
1.000E+04	1.631E+01	1.573E+01	1.416E+01	1.108E+01	7.668E+00	5.511E+00	4.874E+00	5.049E+00	5.282E+00

LOG S/S' = -1.5

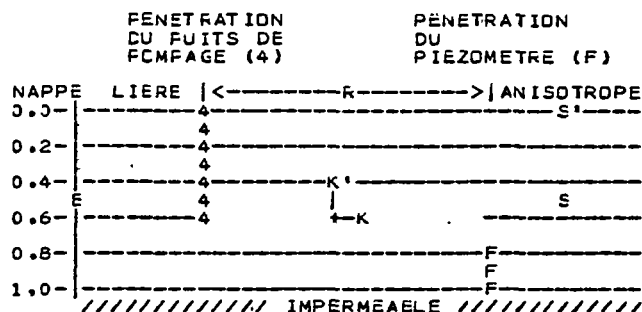
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.035E-02	3.811E-02	3.143E-02	1.650E-02	2.848E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.604E-01	3.513E-01	1.292E-01	8.222E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.418E+00	9.164E-01	2.503E-01	2.090E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.538E+00	1.337E+00	3.226E-01	7.835E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.542E+00	3.409E+00	1.551E+00	5.046E-01	3.348E-01
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.180E+00	6.734E+00	4.126E+00	2.082E+00	1.801E+00	1.940E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.039E+01	7.461E+00	4.724E+00	3.784E+00	3.910E+00	4.132E+00
1.000E+04	1.631E+01	1.573E+01	1.416E+01	1.112E+01	8.070E+00	6.485E+00	5.959E+00	6.176E+00	6.425E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.034E-02	3.802E-02	3.085E-02	1.602E-02	3.890E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.602E-01	3.495E-01	1.306E-01	1.604E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.418E+00	9.134E-01	2.789E-01	6.700E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.536E+00	1.348E+00	4.658E-01	3.068E-01
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.541E+00	3.405E+00	1.639E+00	5.261E-01	9.452E-01
1.000E+02	8.910E+00	8.884E+00	8.733E+00	8.179E+00	6.730E+00	4.233E+00	2.744E+00	2.764E+00	2.958E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.039E+01	7.569E+00	5.424E+00	4.791E+00	4.977E+00	5.220E+00
1.000E+04	1.631E+01	1.573E+01	1.415E+01	1.123E+01	8.770E+00	7.495E+00	7.026E+00	7.262E+00	7.521E+00

PUITS A PENETRATION DE 0.0 A 0.6 ET PIEZOMETRE OUVERT DE 0.8 A 1.0
 ABaque POUR L'INTERPRETATION DE FOMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 4 F



LOG S/S' = -3.0

TT/R2S	R A B A T T E M E N T S				R E C U I T S			
1.000E-01	1.424E-06	1.341E-06	1.413E-06	1.358E-06	7.583E-07	0.0	6.454E-04	1.234E-02
3.162E-01	1.737E-05	1.745E-05	1.753E-05	1.649E-05	3.758E-06	9.536E-05	4.480E-02	1.549E-01
1.000E+00	5.738E-05	5.738E-05	5.735E-05	4.629E-05	4.545E-06	1.139E-02	3.525E-01	3.055E-01
3.162E+00	1.123E-04	1.121E-04	1.097E-04	5.948E-05	2.306E-04	1.392E-01	8.587E-01	3.261E-01
1.000E+01	1.726E-04	1.724E-04	1.554E-04	6.075E-05	1.570E-02	5.916E-01	1.101E+00	3.323E-01
1.000E+02	2.981E-04	2.802E-04	1.722E-04	1.627E-02	6.292E-01	1.424E+00	1.138E+00	4.111E-01
1.000E+03	4.071E-04	2.581E-04	1.644E-02	6.332E-01	1.471E+00	1.463E+00	1.279E+00	1.025E+00
1.000E+04	4.245E-04	1.661E-02	6.346E-01	1.477E+00	1.510E+00	1.615E+00	2.171E+00	2.810E+00

LOG S/S' = -2.5

TT/R2S	R A B A T T E M E N T S				R E C U I T S			
1.000E-01	1.430E-06	1.340E-06	1.443E-06	1.353E-06	5.695E-07	0.0	6.348E-04	1.231E-02
3.162E-01	1.732E-05	1.748E-05	1.759E-05	1.651E-05	3.083E-06	9.173E-05	4.477E-02	1.546E-01
1.000E+00	5.735E-05	5.742E-05	5.739E-05	4.633E-05	2.747E-06	1.138E-02	3.534E-01	3.066E-01
3.162E+00	1.122E-04	1.121E-04	1.099E-04	5.912E-05	2.263E-04	1.391E-01	8.587E-01	3.309E-01
1.000E+01	1.725E-04	1.724E-04	1.558E-04	5.929E-05	1.568E-02	5.914E-01	1.102E+00	3.502E-01
1.000E+02	2.982E-04	2.802E-04	1.710E-04	1.622E-02	6.290E-01	1.426E+00	1.171E+00	5.846E-01
1.000E+03	4.078E-04	2.674E-04	1.642E-02	6.331E-01	1.473E+00	1.499E+00	1.562E+00	1.810E+00
1.000E+04	4.245E-04	1.661E-02	6.345E-01	1.479E+00	1.546E+00	1.916E+00	3.076E+00	3.891E+00

LOG S/S' = -2.0

TT/R2S	R A B A T T E M E N T S				R E C U I T S			
1.000E-01	1.406E-06	1.355E-06	1.427E-06	1.392E-06	0.0	0.0	6.011E-04	1.222E-02
3.162E-01	1.735E-05	1.747E-05	1.763E-05	1.653E-05	1.636E-06	7.888E-05	4.466E-02	1.548E-01
1.000E+00	5.736E-05	5.741E-05	5.750E-05	4.607E-05	0.0	1.134E-02	3.531E-01	3.090E-01
3.162E+00	1.122E-04	1.122E-04	1.100E-04	5.765E-05	2.130E-04	1.393E-01	8.586E-01	3.460E-01
1.000E+01	1.726E-04	1.725E-04	1.558E-04	5.929E-05	1.564E-02	5.911E-01	1.100E+00	4.054E-01
1.000E+02	2.977E-04	2.806E-04	1.661E-04	1.622E-02	6.287E-01	1.432E+00	1.270E+00	1.012E+00
1.000E+03	4.075E-04	2.954E-04	1.638E-02	6.327E-01	1.479E+00	1.606E+00	2.163E+00	2.802E+00
1.000E+04	4.241E-04	1.659E-02	6.341E-01	1.485E+00	1.654E+00	2.539E+00	4.114E+00	5.002E+00

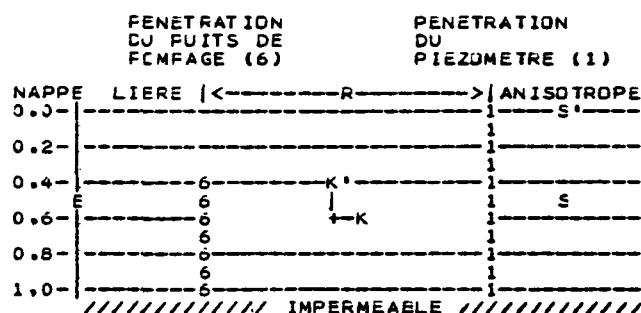
LOG S/S' = -1.5

TT/R2S	R A B A T T E M E N T S				R E C U I T S			
1.000E-01	1.421E-06	1.376E-06	1.463E-06	1.001E-06	0.0	0.0	4.942E-04	1.194E-02
3.162E-01	1.733E-05	1.751E-05	1.762E-05	1.567E-05	0.0	3.901E-05	4.433E-02	1.545E-01
1.000E+00	5.739E-05	5.752E-05	5.763E-05	4.403E-05	0.0	1.122E-02	3.521E-01	3.165E-01
3.162E+00	1.123E-04	1.124E-04	1.098E-04	5.298E-05	1.730E-04	1.336E-01	8.583E-01	3.521E-01
1.000E+01	1.728E-04	1.730E-04	1.542E-04	4.143E-05	1.551E-02	5.899E-01	1.125E+00	5.656E-01
1.000E+02	2.990E-04	2.804E-04	1.527E-04	1.609E-02	6.275E-01	1.451E+00	1.536E+00	1.786E+00
1.000E+03	4.082E-04	2.911E-04	1.624E-02	6.316E-01	1.496E+00	1.883E+00	3.048E+00	3.866E+00
1.000E+04	4.247E-04	1.655E-02	6.328E-01	1.503E+00	1.938E+00	3.437E+00	5.190E+00	6.128E+00

LOG S/S' = -1.0

TT/R2S	R A B A T T E M E N T S				R E C U I T S			
1.000E-01	1.376E-06	1.372E-06	1.440E-06	7.054E-07	0.0	0.0	1.562E-04	1.112E-02
3.162E-01	1.732E-05	1.752E-05	1.755E-05	1.444E-05	0.0	0.0	4.326E-02	1.538E-01
1.000E+00	5.734E-05	5.755E-05	5.704E-05	4.015E-05	0.0	1.082E-02	3.490E-01	3.392E-01
3.162E+00	1.124E-04	1.126E-04	1.082E-04	4.342E-05	4.410E-05	1.373E-01	8.574E-01	5.227E-01
1.000E+01	1.729E-04	1.730E-04	1.495E-04	1.175E-06	1.511E-02	5.864E-01	1.173E+00	5.525E-01
1.000E+02	2.992E-04	2.790E-04	1.088E-04	1.568E-02	6.239E-01	1.504E+00	2.079E+00	2.725E+00
1.000E+03	4.081E-04	2.769E-04	1.580E-02	6.279E-01	1.552E+00	2.452E+00	4.029E+00	4.529E+00
1.000E+04	4.235E-04	1.640E-02	6.288E-01	1.558E+00	2.504E+00	4.422E+00	6.254E+00	7.212E+00

ABaque POUR L'INTERPRETATION DE FCMFAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.491E-02	2.217E-02	4.099E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.136E-01	2.113E-01	8.359E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.863E-01	4.033E-01	8.617E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.032E+00	1.671E+00	4.289E-01	9.383E-03	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.052E+00	1.980E+00	4.366E-01	1.205E-02	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.417E+00	5.329E+00	4.163E+00	2.032E+00	5.354E-01	8.202E-02	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.628E+00	6.452E+00	4.223E+00	2.264E+00	1.323E+00	1.094E+00	
1.000E+04	1.002E+01	1.002E+01	9.933E+00	8.753E+00	6.510E+00	4.487E+00	3.580E+00	3.439E+00	3.236E+00	

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.490E-02	2.462E-02	2.220E-02	4.076E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.136E-01	2.115E-01	8.454E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.864E-01	4.045E-01	8.238E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.032E+00	1.672E+00	4.352E-01	1.192E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.052E+00	1.984E+00	4.592E-01	2.310E-02	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.417E+00	5.329E+00	4.163E+00	2.089E+00	7.568E-01	3.650E-01	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.628E+00	6.457E+00	4.287E+00	2.709E+00	2.291E+00	2.112E+00	
1.000E+04	1.002E+01	1.002E+01	9.933E+00	8.759E+00	6.578E+00	4.981E+00	4.729E+00	4.610E+00	4.382E+00	

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0				-6.0				-5.0				-4.0				-3.0				-2.0				-1.0				0.0				1.0					
TT/R2S	R		A		B		A		T		T		E		M		E		N		T		S		R		E		C		U		I		T		S	
1.000E-01	2.491E-02				2.490E-02					2.491E-02					2.490E-02					2.490E-02					2.491E-02					2.496E-02					2.225E-02		4.000E-03	
3.162E-01	3.159E-01				3.159E-01					3.159E-01					3.159E-01					3.159E-01					3.160E-01					3.137E-01					2.115E-01		8.762E-03	
1.000E+00	1.044E+00				1.044E+00					1.044E+00					1.044E+00					1.044E+00					1.044E+00					9.869E-01					4.084E-01		1.139E-02	
3.162E+00	2.038E+00				2.038E+00					2.038E+00					2.038E+00					2.038E+00					2.032E+00					1.675E+00					4.549E-01		2.234E-02	
1.000E+01	3.136E+00				3.136E+00					3.136E+00					3.136E+00					3.137E+00					3.053E+00					1.975E+00					5.294E-01		7.994E-02	
1.000E+02	5.417E+00				5.416E+00					5.417E+00					5.417E+00					5.329E+00					4.184E+00					2.255E+00					1.315E+00		1.067E+00	
1.000E+03	7.717E+00				7.717E+00					7.717E+00					7.629E+00					6.474E+00					4.473E+00					3.571E+00					1.425E+00		1.226E+00	
1.000E+04	1.002E+01				1.002E+01					9.934E+00					8.775E+00					6.773E+00					5.890E+00					5.924E+00					5.774E+00		5.529E+00	

LOG S/S' = -1.5

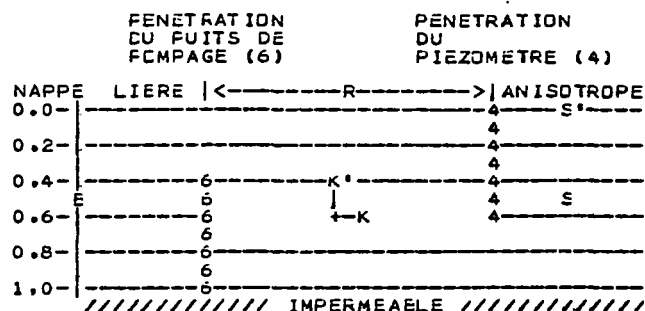
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.491E-02	2.492E-02	2.509E-02	2.257E-02	3.772E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.141E-01	2.134E-01	8.823E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.885E-01	4.204E-01	2.005E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.032E+00	1.683E+00	5.155E-01	7.513E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.055E+00	2.037E+00	7.362E-01	1.502E-01	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.417E+00	5.332E+00	4.233E+00	2.682E+00	2.263E+00	2.084E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.631E+00	6.524E+00	4.953E+00	4.703E+00	4.580E+00	4.353E+00	
1.000E+04	1.002E+01	1.002E+01	9.936E+00	8.825E+00	7.253E+00	7.041E+00	7.093E+00	6.916E+00	6.662E+00	

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.491E-02	2.493E-02	2.553E-02	2.337E-02	3.052E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.162E-01	3.154E-01	2.177E-01	1.362E-02	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.045E+00	9.932E-01	4.566E-01	6.137E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.034E+00	1.706E+00	6.895E-01	3.169E-01	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.137E+00	3.061E+00	2.153E+00	1.240E+00	1.014E+00	
1.000E+02	5.417E+00	5.416E+00	5.417E+00	5.417E+00	5.338E+00	4.372E+00	3.485E+00	3.338E+00	3.140E+00	
1.000E+03	7.717E+00	7.717E+00	7.718E+00	7.638E+00	6.665E+00	5.803E+00	5.836E+00	5.686E+00	5.448E+00	
1.000E+04	1.002E+01	1.002E+01	9.943E+00	8.967E+00	8.108E+00	8.184E+00	8.208E+00	8.017E+00	7.764E+00	

PUITS A PENETRATION DE 0.4 A 1.0 ET PIEZOMETRE OUVERT DE 0.0 A 0.6
 ABAQUE POUR L'INTERPRETATION DE FCMPS EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 6 4



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.467E-02	2.842E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.440E-01	5.804E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.235E-01	2.759E-01	6.099E-03
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.091E+00	2.941E-01	7.001E-03
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.829E+00	1.303E+00	3.011E-01	1.010E-02
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.104E+00	2.568E+00	1.345E+00	3.915E-01	8.127E-02
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.382E+00	3.872E+00	2.636E+00	1.562E+00	1.116E+00	1.051E+00
1.000E+04	5.567E+00	5.573E+00	5.563E+00	5.152E+00	3.919E+00	2.887E+00	2.786E+00	3.108E+00	3.136E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.467E-02	2.849E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.441E-01	5.969E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.235E-01	2.770E-01	6.882E-03
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.091E+00	2.598E-01	9.961E-03
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.829E+00	1.307E+00	3.218E-01	2.208E-02
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.104E+00	2.593E+00	1.358E+00	3.950E-01	3.537E-01
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.383E+00	3.877E+00	2.692E+00	1.977E+00	2.021E+00	2.036E+00
1.000E+04	5.567E+00	5.573E+00	5.563E+00	5.157E+00	3.983E+00	3.348E+00	3.855E+00	4.238E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.468E-02	2.874E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.443E-01	6.498E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.237E-01	2.805E-01	9.526E-03
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.093E+00	3.178E-01	2.143E-02
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.829E+00	1.318E+00	3.661E-01	7.542E-02
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.104E+00	2.608E+00	1.553E+00	1.111E+00	1.044E+00
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.383E+00	3.892E+00	2.878E+00	2.777E+00	3.095E+00	3.127E+00
1.000E+04	5.567E+00	5.573E+00	5.563E+00	5.172E+00	4.166E+00	4.194E+00	4.986E+00	5.377E+00	5.407E+00

LOG S/S' = -1.5

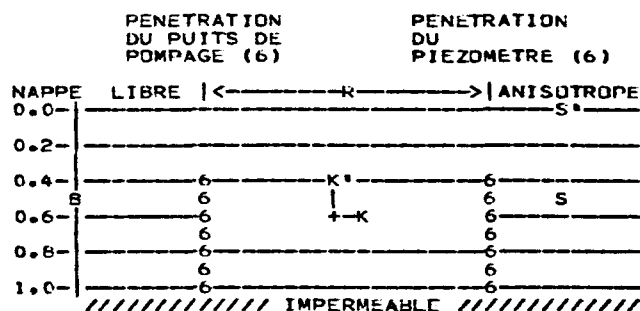
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.405E-02	1.468E-02	2.948E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.451E-01	6.225E-03
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.241E-01	2.912E-01	1.945E-02
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.099E+00	3.733E-01	7.511E-02
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.830E+00	1.355E+00	5.760E-01	3.402E-01
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.105E+00	2.652E+00	1.950E+00	1.995E+00	2.010E+00
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.384E+00	3.938E+00	3.320E+00	3.827E+00	4.211E+00	4.241E+00
1.000E+04	5.567E+00	5.573E+00	5.564E+00	5.217E+00	4.618E+00	5.263E+00	6.125E+00	6.517E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.384E-02	1.384E-02	1.384E-02	1.383E-02	1.383E-02	1.384E-02	1.404E-02	1.470E-02	3.149E-03
3.162E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.755E-01	1.867E-01	1.476E-01	1.410E-02
1.000E+00	5.802E-01	5.801E-01	5.802E-01	5.801E-01	5.801E-01	5.839E-01	6.253E-01	3.238E-01	6.277E-02
3.162E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.132E+00	1.169E+00	1.116E+00	5.331E-01	3.098E-01
1.000E+01	1.742E+00	1.743E+00	1.742E+00	1.742E+00	1.748E+00	1.832E+00	1.455E+00	1.042E+00	9.778E-01
1.000E+02	3.009E+00	3.009E+00	3.009E+00	3.015E+00	3.107E+00	2.779E+00	2.692E+00	3.016E+00	3.047E+00
1.000E+03	4.287E+00	4.287E+00	4.287E+00	4.386E+00	4.366E+00	4.107E+00	4.900E+00	5.297E+00	5.332E+00
1.000E+04	5.567E+00	5.573E+00	5.566E+00	5.346E+00	5.405E+00	6.341E+00	7.204E+00	7.604E+00	7.641E+00

PUITS A PENETRATION DE 0.4 A 1.0 ET PIEZOMETRE OUVERT DE 0.4 A 1.0
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 6 6



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	4.133E-02	4.132E-02	4.133E-02	4.131E-02	4.115E-02	4.033E-02	3.796E-02	3.028E-02	5.540E-03
3.162E-01	5.243E-01	5.243E-01	5.243E-01	5.236E-01	5.196E-01	5.045E-01	4.569E-01	2.858E-01	1.131E-02
1.000E+00	1.733E+00	1.733E+00	1.733E+00	1.728E+00	1.705E+00	1.630E+00	1.386E+00	5.443E-01	1.174E-02
3.162E+00	3.382E+00	3.382E+00	3.380E+00	3.363E+00	3.294E+00	3.073E+00	2.312E+00	5.776E-01	1.301E-02
1.000E+01	5.205E+00	5.204E+00	5.197E+00	5.152E+00	4.994E+00	4.484E+00	2.726E+00	5.842E-01	1.727E-02
1.000E+02	8.989E+00	8.980E+00	8.930E+00	8.740E+00	8.117E+00	5.983E+00	2.779E+00	6.676E-01	1.010E-01
1.000E+03	1.280E+01	1.275E+01	1.255E+01	1.189E+01	9.632E+00	6.037E+00	2.921E+00	1.314E+00	1.067E+00
1.000E+04	1.657E+01	1.637E+01	1.571E+01	1.341E+01	9.687E+00	6.189E+00	3.839E+00	3.188E+00	3.138E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	4.133E-02	4.132E-02	4.133E-02	4.131E-02	4.115E-02	4.033E-02	3.796E-02	3.028E-02	5.548E-03
3.162E-01	5.243E-01	5.243E-01	5.243E-01	5.236E-01	5.196E-01	5.045E-01	4.569E-01	2.858E-01	1.154E-02
1.000E+00	1.733E+00	1.733E+00	1.733E+00	1.728E+00	1.705E+00	1.630E+00	1.386E+00	5.450E-01	1.283E-02
3.162E+00	3.382E+00	3.382E+00	3.380E+00	3.363E+00	3.294E+00	3.073E+00	2.312E+00	5.827E-01	1.707E-02
1.000E+01	5.205E+00	5.204E+00	5.197E+00	5.152E+00	4.994E+00	4.484E+00	2.726E+00	6.031E-01	3.275E-02
1.000E+02	8.989E+00	8.980E+00	8.929E+00	8.740E+00	8.117E+00	5.985E+00	2.812E+00	8.506E-01	3.800E-01
1.000E+03	1.280E+01	1.275E+01	1.255E+01	1.189E+01	9.634E+00	6.073E+00	3.209E+00	2.140E+00	2.042E+00
1.000E+04	1.657E+01	1.637E+01	1.571E+01	1.341E+01	9.723E+00	6.494E+00	4.788E+00	4.305E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	4.133E-02	4.133E-02	4.133E-02	4.131E-02	4.115E-02	4.033E-02	3.796E-02	3.028E-02	5.676E-03
3.162E-01	5.243E-01	5.243E-01	5.243E-01	5.236E-01	5.196E-01	5.045E-01	4.569E-01	2.859E-01	1.226E-02
1.000E+00	1.733E+00	1.733E+00	1.733E+00	1.728E+00	1.705E+00	1.630E+00	1.386E+00	5.475E-01	1.645E-02
3.162E+00	3.382E+00	3.382E+00	3.380E+00	3.363E+00	3.294E+00	3.073E+00	2.313E+00	5.985E-01	3.189E-02
1.000E+01	5.205E+00	5.204E+00	5.197E+00	5.152E+00	4.994E+00	4.484E+00	2.734E+00	6.614E-01	9.887E-02
1.000E+02	8.989E+00	8.980E+00	8.929E+00	8.740E+00	8.117E+00	5.991E+00	2.912E+00	1.307E+00	1.060E+00
1.000E+03	1.280E+01	1.275E+01	1.255E+01	1.189E+01	9.642E+00	6.180E+00	3.830E+00	3.179E+00	3.129E+00
1.000E+04	1.657E+01	1.637E+01	1.571E+01	1.342E+01	9.835E+00	7.136E+00	5.875E+00	5.439E+00	5.407E+00

LOG S/S' = -1.5

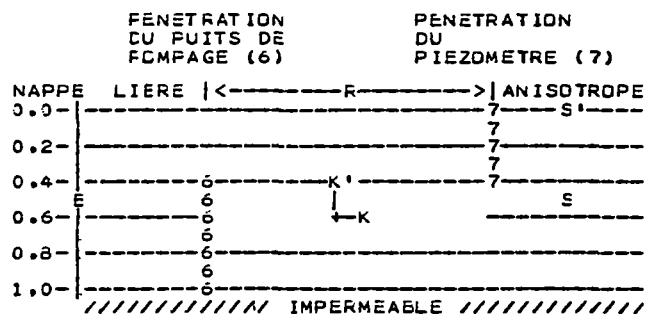
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	4.133E-02	4.132E-02	4.133E-02	4.131E-02	4.115E-02	4.033E-02	3.796E-02	3.028E-02	5.662E-03
3.162E-01	5.243E-01	5.243E-01	5.243E-01	5.236E-01	5.196E-01	5.045E-01	4.569E-01	2.862E-01	1.457E-02
1.000E+00	1.733E+00	1.733E+00	1.733E+00	1.728E+00	1.705E+00	1.630E+00	1.386E+00	5.553E-01	2.929E-02
3.162E+00	3.382E+00	3.382E+00	3.380E+00	3.363E+00	3.294E+00	3.073E+00	2.314E+00	6.466E-01	9.387E-02
1.000E+01	5.205E+00	5.204E+00	5.197E+00	5.152E+00	4.994E+00	4.484E+00	2.751E+00	8.297E-01	3.660E-01
1.000E+02	8.989E+00	8.980E+00	8.929E+00	8.740E+00	8.117E+00	6.010E+00	3.182E+00	2.114E+00	2.016E+00
1.000E+03	1.280E+01	1.275E+01	1.255E+01	1.189E+01	9.662E+00	6.466E+00	4.750E+00	4.277E+00	4.241E+00
1.000E+04	1.657E+01	1.637E+01	1.571E+01	1.344E+01	1.012E+01	8.080E+00	7.000E+00	6.578E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	4.133E-02	4.133E-02	4.133E-02	4.131E-02	4.114E-02	4.034E-02	3.796E-02	3.028E-02	5.901E-03
3.162E-01	5.243E-01	5.243E-01	5.243E-01	5.236E-01	5.196E-01	5.045E-01	4.569E-01	2.872E-01	2.214E-02
1.000E+00	1.733E+00	1.733E+00	1.733E+00	1.728E+00	1.705E+00	1.630E+00	1.386E+00	5.785E-01	7.953E-02
3.162E+00	3.382E+00	3.382E+00	3.380E+00	3.363E+00	3.294E+00	3.073E+00	2.318E+00	7.825E-01	3.343E-01
1.000E+01	5.205E+00	5.204E+00	5.197E+00	5.152E+00	4.994E+00	4.484E+00	2.801E+00	1.235E+00	9.931E-01
1.000E+02	8.989E+00	8.980E+00	8.929E+00	8.740E+00	8.117E+00	6.065E+00	3.745E+00	3.096E+00	3.049E+00
1.000E+03	1.280E+01	1.275E+01	1.255E+01	1.189E+01	9.716E+00	7.049E+00	5.789E+00	5.359E+00	5.333E+00
1.000E+04	1.657E+01	1.637E+01	1.571E+01	1.349E+01	1.070E+01	9.114E+00	8.075E+00	7.665E+00	7.641E+00

PUITS A PENETRATION DE 0.4 A 1.0 ET PIEZOMETRE OUVERT DE 0.0 A 0.4
 ABAQUE POUR L'INTERPRETATION DE FMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABEAU 67



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.625E-04	2.628E-04	2.658E-04	2.947E-04	5.365E-04	1.642E-03	5.183E-03	9.525E-03	1.582E-03
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.345E-03	1.048E-02	3.301E-02	9.841E-02	9.533E-02	4.070E-02
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.265E-02	1.663E-01	3.866E-01	1.914E-01	4.370E-01
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.042E-02	1.533E-01	4.693E-01	7.099E-01	2.046E-01	5.303E-01
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.127E-01	3.500E-01	9.029E-01	8.577E-01	2.113E-01	6.488E-01
1.000E+02	5.871E-02	7.169E-02	1.473E-01	4.315E-01	1.146E+00	1.430E+00	8.939E-01	2.586E-01	7.932E-01
1.000E+03	9.616E-02	1.734E-01	4.684E-01	1.234E+00	1.679E+00	1.473E+00	1.135E+00	1.002E+00	1.030E+00
1.000E+04	1.981E-01	4.951E-01	1.272E+00	1.767E+00	1.720E+00	1.716E+00	2.297E+00	2.939E+00	3.067E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.625E-04	2.628E-04	2.658E-04	2.947E-04	5.362E-04	1.641E-03	5.174E-03	9.514E-03	2.006E-03
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.345E-03	1.048E-02	3.300E-02	9.838E-02	9.958E-02	4.264E-02
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.265E-02	1.662E-01	3.865E-01	1.925E-01	5.202E-01
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.041E-02	1.533E-01	4.693E-01	7.103E-01	2.102E-01	8.367E-01
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.127E-01	3.500E-01	9.029E-01	8.614E-01	2.313E-01	2.064E-01
1.000E+02	5.871E-02	7.169E-02	1.473E-01	4.314E-01	1.146E+00	1.434E+00	9.455E-01	4.953E-01	3.464E-01
1.000E+03	9.616E-02	1.734E-01	4.683E-01	1.234E+00	1.684E+00	1.531E+00	1.510E+00	1.875E+00	1.999E+00
1.000E+04	1.981E-01	4.951E-01	1.272E+00	1.772E+00	1.782E+00	2.167E+00	3.335E+00	4.050E+00	4.212E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.625E-04	2.628E-04	2.658E-04	2.946E-04	5.360E-04	1.637E-03	5.146E-03	9.502E-03	2.076E-03
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.345E-03	1.047E-02	3.299E-02	9.830E-02	9.978E-02	4.279E-02
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.264E-02	1.662E-01	3.865E-01	1.925E-01	7.591E-01
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.041E-02	1.533E-01	4.692E-01	7.118E-01	2.276E-01	2.005E-01
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.127E-01	3.499E-01	9.029E-01	8.728E-01	2.533E-01	7.755E-01
1.000E+02	5.871E-02	7.169E-02	1.473E-01	4.314E-01	1.146E+00	1.443E+00	1.057E+00	9.952E-01	1.023E+00
1.000E+03	9.616E-02	1.734E-01	4.683E-01	1.234E+00	1.698E+00	1.737E+00	2.268E+00	2.631E+00	3.079E+00
1.000E+04	1.981E-01	4.950E-01	1.272E+00	1.787E+00	1.961E+00	2.989E+00	4.438E+00	5.177E+00	5.348E+00

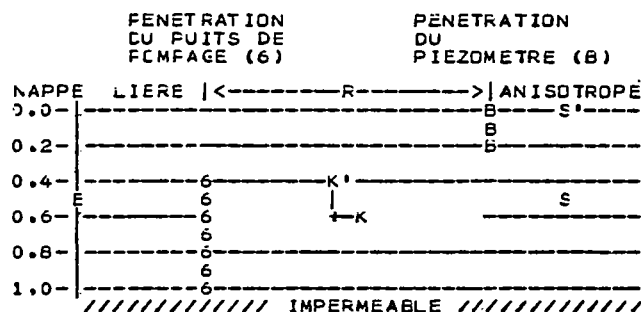
LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.625E-04	2.628E-04	2.657E-04	2.943E-04	5.348E-04	1.625E-03	5.059E-03	9.782E-03	2.297E-03
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.344E-03	1.047E-02	3.295E-02	9.803E-02	1.004E-01	6.874E-02
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.263E-02	1.661E-01	3.862E-01	2.064E-01	1.829E-01
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.041E-02	1.532E-01	4.688E-01	7.165E-01	2.815E-01	7.357E-01
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.126E-01	3.498E-01	9.027E-01	9.079E-01	4.774E-01	3.335E-01
1.000E+02	5.871E-02	7.169E-02	1.473E-01	4.313E-01	1.146E+00	1.491E+00	1.484E+00	1.855E+00	1.974E+00
1.000E+03	9.616E-02	1.734E-01	4.682E-01	1.234E+00	1.742E+00	2.139E+00	3.337E+00	4.024E+00	4.186E+00
1.000E+04	1.981E-01	4.950E-01	1.272E+00	1.831E+00	2.398E+00	4.027E+00	5.557E+00	6.311E+00	6.466E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.625E-04	2.628E-04	2.657E-04	2.941E-04	5.306E-04	1.586E-03	4.783E-03	9.497E-03	2.938E-03
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.343E-03	1.046E-02	3.283E-02	9.720E-02	1.023E-01	1.251E-01
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.847E-02	5.259E-02	1.657E-01	3.853E-01	2.385E-01	6.266E-01
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.040E-02	1.531E-01	4.677E-01	7.336E-01	4.371E-01	3.045E-01
1.000E+01	3.321E-02	3.453E-02	4.628E-02	1.126E-01	3.494E-01	9.021E-01	1.009E+00	9.299E-01	9.592E-01
1.000E+02	5.871E-02	7.169E-02	1.472E-01	4.309E-01	1.145E+00	1.613E+00	2.205E+00	2.651E+00	3.002E+00
1.000E+03	9.616E-02	1.734E-01	4.678E-01	1.233E+00	1.866E+00	2.903E+00	4.353E+00	5.101E+00	5.276E+00
1.000E+04	1.981E-01	4.947E-01	1.271E+00	1.955E+00	3.166E+00	5.077E+00	6.625E+00	7.395E+00	7.580E+00

TABLEAU 6 B

[illegible][illegible]

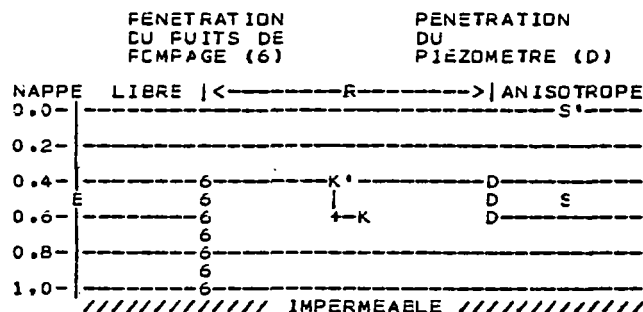
LOG K ¹ R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A S A T T E M E N T S					R E C U I T S				
1.000E-01	1.032E-06	1.001E-06	5.682E-07	8.282E-07	0.0	0.0	5.411E-04	4.680E-03	1.184E-03	
3.162E-01	1.267E-05	1.264E-05	1.258E-05	1.158E-05	0.0	5.406E-05	3.361E-02	5.101E-02	3.655E-03	
1.000E+00	4.179E-05	4.174E-05	4.153E-05	3.201E-05	0.0	1.106E-02	1.736E-01	1.026E-01	6.157E-03	
3.162E+00	8.147E-05	8.143E-05	7.943E-05	3.808E-05	1.847E-04	1.105E-01	3.409E-01	1.284E-01	1.827E-02	
1.000E+01	1.254E-04	1.251E-04	1.114E-04	2.886E-05	1.529E-02	3.202E-01	4.306E-01	1.923E-01	7.505E-02	
1.000E+02	2.163E-04	2.022E-04	1.056E-04	1.585E-02	3.457E-01	6.092E-01	6.446E-01	6.744E-01	1.002E+00	
1.000E+03	2.953E-04	2.040E-04	1.557E-02	3.484E-01	6.386E-01	8.577E-01	1.809E+00	2.763E+00	3.022E+00	
1.000E+04	3.063E-04	1.615E-02	3.491E-01	6.415E-01	8.919E-01	2.112E+00	3.907E+00	4.580E+00	5.257E+00	

[illegible]

L O G K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S	R E C U I T S							
1.000E-01	1.053E-05	9.928E-C7	7.951E-C7	0.0	0.0	0.0	0.0	4.216E-03	2.627E-C3
3.162E-01	1.270E-05	1.264E-C5	1.210E-05	7.475E-06	0.0	0.0	3.105E-02	5.336E-02	1.260E-C2
1.000E+00	4.182E-05	4.175E-C5	4.CC0E-05	1.906E-05	0.0	9.527E-03	1.651E-01	1.456E-01	6.071E-C2
3.162E+00	8.155E-05	8.134E-C5	7.478E-05	0.0	0.0	1.063E-01	3.556E-01	3.345E-01	2.985E-C1
1.000E+01	1.255E-04	1.243E-C4	5.742E-05	0.0	1.400E-02	3.149E-01	5.630E-01	6.136E-01	9.406E-C1
1.000E+02	2.166E-04	1.923E-C4	0.0	1.455E-02	3.403E-01	7.690E-01	1.727E+00	2.666E+00	2.958E+C0
1.000E+03	2.946E-04	1.046E-C4	1.463E-02	3.431E-01	8.014E-01	2.025E+00	3.823E+00	4.538E+00	5.221E+C0
1.000E+04	3.033E-04	1.516E-C2	3.433E-01	8.050E-01	2.069E+00	4.147E+00	6.065E+00	7.193E+00	7.522E+C0

PUITS A PENETRATION DE 0.4 A 1.0 ET PIEZOMETRE OUVERT DE 0.4 A 6.0
 ABAQUE POUR L'INTERPRETATION DE FCMPS EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCOVA

TABLEAU 6 D



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.092E-02	4.035E-02	3.814E-02	3.172E-02	2.412E-02	4.589E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.606E-01	3.631E-01	2.328E-01	9.359E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.037E+00	4.448E-01	9.825E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.568E+00	1.852E+00	4.724E-01	1.123E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.681E+00	2.152E+00	4.783E-01	1.558E-02
1.000E+02	8.911E+00	8.684E+00	8.733E+00	8.180E+00	7.018E+00	4.905E+00	2.236E+00	5.533E-01	1.009E-01
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.256E+00	4.953E+00	2.363E+00	1.139E+00	1.025E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.192E+01	8.302E+00	5.087E+00	3.189E+00	2.687E+00	3.039E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.035E-02	3.814E-02	3.171E-02	2.410E-02	4.624E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.630E-01	2.327E-01	9.649E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.097E+00	4.455E-01	1.107E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.567E+00	1.852E+00	4.768E-01	1.571E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.681E+00	2.152E+00	4.952E-01	3.232E-02
1.000E+02	8.911E+00	8.684E+00	8.733E+00	8.180E+00	7.018E+00	4.906E+00	2.266E+00	7.183E-01	3.693E-01
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.257E+00	4.982E+00	2.622E+00	1.503E+00	1.967E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.192E+01	8.334E+00	5.359E+00	4.059E+00	3.562E+00	4.155E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.036E-02	3.814E-02	3.168E-02	2.401E-02	4.735E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.629E-01	2.326E-01	1.057E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.097E+00	4.474E-01	1.515E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.567E+00	1.852E+00	4.508E-01	3.155E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.681E+00	2.152E+00	5.474E-01	9.851E-02
1.000E+02	8.911E+00	8.684E+00	8.733E+00	8.180E+00	7.017E+00	4.911E+00	2.355E+00	1.132E+00	1.019E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.264E+00	5.078E+00	3.180E+00	2.879E+00	3.030E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.192E+01	8.433E+00	5.937E+00	5.081E+00	5.072E+00	5.286E+00

LOG S/S' = -1.5

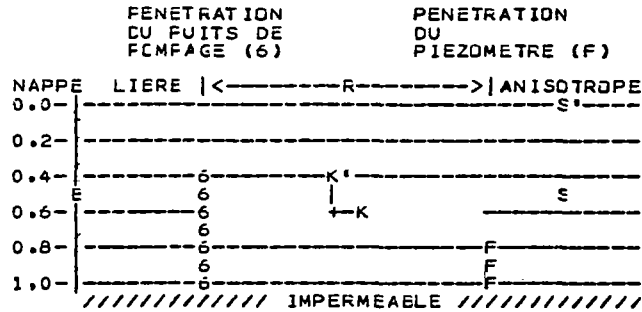
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.035E-02	3.813E-02	3.159E-02	2.374E-02	5.082E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.626E-01	2.322E-01	1.349E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.097E+00	4.533E-01	2.920E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.567E+00	1.851E+00	5.334E-01	9.435E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.680E+00	2.211E+00	6.986E-01	3.555E-01
1.000E+02	8.911E+00	8.684E+00	8.733E+00	8.180E+00	7.017E+00	4.926E+00	2.535E+00	1.875E+00	1.943E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.277E+00	5.331E+00	4.021E+00	3.937E+00	4.130E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.194E+01	8.685E+00	6.800E+00	6.153E+00	6.197E+00	6.422E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.035E-02	3.813E-02	3.153E-02	2.293E-02	6.117E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.604E-01	3.617E-01	2.311E-01	2.275E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.096E+00	4.723E-01	6.125E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.566E+00	1.849E+00	6.541E-01	3.275E-01
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.542E+00	3.677E+00	2.250E+00	1.065E+00	9.566E-01
1.000E+02	8.911E+00	8.684E+00	8.733E+00	8.180E+00	7.014E+00	4.963E+00	2.096E+00	2.601E+00	2.957E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.067E+01	8.320E+00	5.851E+00	4.997E+00	4.599E+00	5.217E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.198E+01	9.206E+00	7.769E+00	7.215E+00	7.280E+00	7.512E+00

PUIITS A PENETRATION DE 0.4 A 1.0 ET PIEZOMETRE OUVERT DE 0.8 A 1.0
 ABAQUE POUR L'INTERPRETATION DE FCMPAGE EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELETSOVA

TABLEAU E F



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.151E-02	4.150E-02	4.151E-02	4.150E-02	4.150E-02	4.151E-02	4.141E-02	3.529E-02	6.358E-03
3.162E-01	5.266E-01	5.265E-01	5.266E-01	5.265E-01	5.266E-01	5.266E-01	5.205E-01	3.289E-01	1.299E-02
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.607E+00	6.245E-01	1.353E-02
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.381E+00	2.672E+00	6.625E-01	1.514E-02
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.031E+00	3.146E+00	6.680E-01	2.042E-02
1.000E+02	9.028E+00	9.027E+00	9.028E+00	9.027E+00	8.823E+00	6.753E+00	3.200E+00	7.377E-01	1.116E-01
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.266E+01	1.056E+01	6.808E+00	3.303E+00	1.281E+00	1.032E+00
1.000E+04	1.670E+01	1.670E+01	1.650E+01	1.440E+01	1.062E+01	6.916E+00	4.016E+00	2.571E+00	3.038E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.151E-02	4.150E-02	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.140E-02	3.527E-02	6.391E-03
3.162E-01	5.266E-01	5.265E-01	5.266E-01	5.265E-01	5.266E-01	5.266E-01	5.205E-01	3.288E-01	1.331E-02
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.607E+00	6.253E-01	1.454E-02
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.381E+00	2.672E+00	6.665E-01	2.020E-02
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.031E+00	3.147E+00	6.636E-01	3.669E-02
1.000E+02	9.028E+00	9.027E+00	9.028E+00	9.027E+00	8.823E+00	6.754E+00	3.224E+00	6.901E-01	3.825E-01
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.266E+01	1.057E+01	6.933E+00	3.518E+00	2.004E+00	1.968E+00
1.000E+04	1.670E+01	1.670E+01	1.650E+01	1.440E+01	1.064E+01	7.139E+00	4.832E+00	4.035E+00	4.153E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.151E-02	4.150E-02	4.151E-02	4.150E-02	4.151E-02	4.150E-02	4.138E-02	3.518E-02	6.495E-03
3.162E-01	5.266E-01	5.265E-01	5.266E-01	5.265E-01	5.266E-01	5.266E-01	5.204E-01	3.286E-01	1.432E-02
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.606E+00	6.267E-01	1.954E-02
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.381E+00	2.672E+00	6.788E-01	3.779E-02
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.031E+00	3.150E+00	7.313E-01	1.095E-01
1.000E+02	9.028E+00	9.027E+00	9.028E+00	9.027E+00	8.823E+00	6.756E+00	3.295E+00	1.273E+00	1.025E+00
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.266E+01	1.057E+01	6.907E+00	4.007E+00	2.962E+00	3.030E+00
1.000E+04	1.670E+01	1.670E+01	1.650E+01	1.440E+01	1.072E+01	7.641E+00	5.832E+00	5.146E+00	5.264E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.151E-02	4.150E-02	4.151E-02	4.150E-02	4.151E-02	4.150E-02	4.132E-02	3.491E-02	6.630E-03
3.162E-01	5.266E-01	5.265E-01	5.266E-01	5.265E-01	5.266E-01	5.265E-01	5.202E-01	3.279E-01	1.752E-02
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.606E+00	6.308E-01	3.508E-02
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.381E+00	2.670E+00	7.162E-01	1.046E-01
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.030E+00	3.157E+00	6.693E-01	3.694E-01
1.000E+02	9.028E+00	9.027E+00	9.028E+00	9.027E+00	8.822E+00	6.764E+00	3.491E+00	1.579E+00	1.945E+00
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.265E+01	1.058E+01	7.111E+00	4.604E+00	4.013E+00	4.129E+00
1.000E+04	1.670E+01	1.670E+01	1.650E+01	1.441E+01	1.093E+01	8.448E+00	6.895E+00	6.265E+00	6.421E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.151E-02	4.150E-02	4.151E-02	4.150E-02	4.150E-02	4.148E-02	4.112E-02	3.406E-02	7.632E-03
3.162E-01	5.266E-01	5.265E-01	5.266E-01	5.265E-01	5.265E-01	5.265E-01	5.195E-01	3.260E-01	2.758E-02
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.604E+00	6.433E-01	5.641E-02
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.380E+00	2.667E+00	6.220E-01	3.398E-01
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.028E+00	3.179E+00	1.204E+00	9.639E-01
1.000E+02	9.028E+00	9.027E+00	9.028E+00	9.027E+00	8.820E+00	6.787E+00	3.923E+00	2.883E+00	2.956E+00
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.265E+01	1.060E+01	7.555E+00	5.747E+00	5.070E+00	5.216E+00
1.000E+04	1.670E+01	1.670E+01	1.649E+01	1.443E+01	1.137E+01	9.395E+00	7.955E+00	7.352E+00	7.516E+00

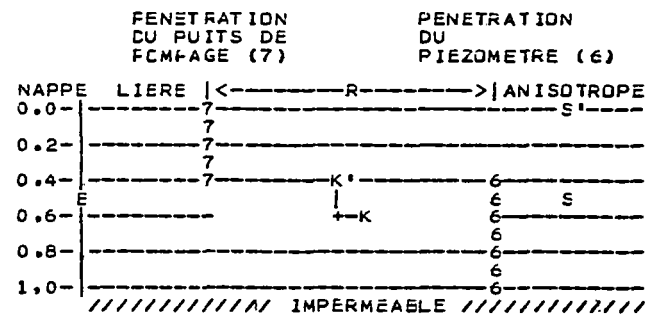
PENETRATION DU FUIT DE FCMPAGE (7)		PENETRATION DU PIEZOMETRE (1)	
NAPPE LIBRE	<-----R----->		ANISOTROPE
0.0-	7-----	1	S'
0.2-	7-----	1	
0.4-	7-----	1	
0.6-	E----- K' +K	1	S
0.8-	-----	1	
1.0-	-----	1	
////////////////// IMPERMEABLE ////////////////////			

[illegible][illegible][illegible][illegible]

	-7.0		-6.0		-5.0		-4.0		-3.0		-2.0		-1.0		0.0		1.0										
TT/R2S	R	A B A T T E M E N T S	R	E C U I T S																							
1.000E-01	2.459E-02	2.459E-02	2.459E-02	2.457E-02	2.443E-02	2.384E-02	2.050E-02	9.081E-03	0.0																		
3.162E-01	3.119E-01	3.119E-01	3.118E-01	3.108E-01	3.039E-01	2.793E-01	2.021E-01	6.203E-02	2.258E-03																		
1.000E+00	1.031E+00	1.031E+00	1.030E+00	1.022E+00	9.830E-01	9.551E-01	5.334E-01	1.960E-01	3.203E-02																		
3.162E+00	2.012E+00	2.012E+00	2.008E+00	1.978E+00	1.860E+00	1.504E+00	8.933E-01	4.141E-01	2.715E-01																		
1.000E+01	3.057E+00	3.055E+00	3.048E+00	3.004E+00	2.739E+00	2.075E+00	1.383E+00	1.065E+00	9.954E-01																		
1.000E+02	5.346E+00	5.331E+00	5.244E+00	4.935E+00	4.184E+00	3.713E+00	3.951E+00	3.472E+00	3.177E+00																		
1.000E+03	7.602E+00	7.515E+00	7.205E+00	6.484E+00	6.281E+00	7.174E+00	6.775E+00	5.865E+00	5.459E+00																		
1.000E+04	9.790E+00	9.487E+00	6.802E+00	6.722E+00	9.927E+00	1.006E+01	9.217E+00	8.231E+00	7.615E+00																		

PUITS A PENETRATION DE 0.0 A 0.4 ET PIEZOMETRE OUVERT DE 0.4 A 1.0
ABAQUE POUR L'INTERPRETATION DE CMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCOVA

TABLEAU 7 6



LOG S/S' = -3.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.627E-04	2.629E-04	2.658E-04	2.947E-04	5.366E-04	1.643E-03	5.191E-03	9.535E-03	1.968E-03	
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.345E-03	1.048E-02	3.301E-02	9.844E-02	9.556E-02	4.023E-02	
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.265E-02	1.663E-01	3.867E-01	1.915E-01	4.221E-01	
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.042E-02	1.533E-01	4.694E-01	7.101E-01	2.049E-01	4.835E-01	
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.127E-01	3.500E-01	9.031E-01	8.566E-01	2.124E-01	7.034E-01	
1.000E+02	5.871E-02	7.159E-02	1.473E-01	4.315E-01	1.146E+00	1.431E+00	9.027E-01	3.098E-01	6.554E-01	
1.000E+03	9.616E-02	1.734E-01	4.684E-01	1.234E+00	1.680E+00	1.483E+00	1.185E+00	1.115E+00	1.062E+00	
1.000E+04	1.981E-01	4.951E-01	1.272E+00	1.769E+00	1.733E+00	1.825E+00	2.686E+00	3.243E+00	3.183E+00	

LOG S/S' = -2.5

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.626E-04	2.629E-04	2.658E-04	2.948E-04	5.367E-04	1.645E-03	5.202E-03	9.547E-03	1.959E-03	
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.345E-03	1.048E-02	3.301E-02	9.847E-02	9.566E-02	4.115E-02	
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.265E-02	1.663E-01	3.868E-01	1.922E-01	4.734E-01	
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.042E-02	1.533E-01	4.694E-01	7.112E-01	2.112E-01	6.514E-01	
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.127E-01	3.500E-01	9.033E-01	8.642E-01	2.347E-01	1.636E-01	
1.000E+02	5.871E-02	7.159E-02	1.473E-01	4.315E-01	1.147E+00	1.438E+00	9.728E-01	5.331E-01	3.424E-01	
1.000E+03	9.616E-02	1.734E-01	4.684E-01	1.234E+00	1.688E+00	1.569E+00	1.714E+00	2.101E+00	2.069E+00	
1.000E+04	1.981E-01	4.951E-01	1.273E+00	1.776E+00	1.822E+00	2.429E+00	3.876E+00	4.401E+00	4.323E+00	

LOG S/S' = -2.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.626E-04	2.629E-04	2.658E-04	2.948E-04	5.372E-04	1.650E-03	5.235E-03	9.584E-03	1.928E-03	
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.345E-03	1.048E-02	3.303E-02	9.858E-02	1.001E-01	4.413E-02	
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.266E-02	1.663E-01	3.873E-01	1.969E-01	6.541E-01	
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.042E-02	1.533E-01	4.696E-01	7.146E-01	2.310E-01	1.576E-01	
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.127E-01	3.501E-01	9.041E-01	8.817E-01	3.045E-01	6.775E-01	
1.000E+02	5.871E-02	7.159E-02	1.473E-01	4.315E-01	1.147E+00	1.461E+00	1.177E+00	1.108E+00	1.055E+00	
1.000E+03	9.616E-02	1.734E-01	4.684E-01	1.235E+00	1.711E+00	1.816E+00	2.677E+00	3.233E+00	3.174E+00	
1.000E+04	1.981E-01	4.951E-01	1.274E+00	1.800E+00	2.073E+00	3.458E+00	5.067E+00	5.555E+00	5.466E+00	

LOG S/S' = -1.5

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.627E-04	2.629E-04	2.658E-04	2.948E-04	5.389E-04	1.665E-03	5.340E-03	1.010E-02	1.835E-03	
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.345E-03	1.048E-02	3.303E-02	9.893E-02	1.014E-01	5.433E-02	
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.848E-02	5.267E-02	1.665E-01	3.850E-01	2.096E-01	1.402E-01	
3.162E+00	2.152E-02	2.189E-02	2.532E-02	5.042E-02	1.534E-01	4.701E-01	7.253E-01	2.922E-01	6.362E-01	
1.000E+01	3.321E-02	3.453E-02	4.629E-02	1.127E-01	3.502E-01	9.067E-01	9.351E-01	5.142E-01	3.286E-01	
1.000E+02	5.871E-02	7.159E-02	1.473E-01	4.317E-01	1.150E+00	1.529E+00	1.687E+00	2.074E+00	2.042E+00	
1.000E+03	9.616E-02	1.734E-01	4.686E-01	1.238E+00	1.782E+00	2.401E+00	3.648E+00	4.372E+00	4.255E+00	
1.000E+04	1.981E-01	4.953E-01	1.276E+00	1.871E+00	2.667E+00	4.554E+00	6.234E+00	6.691E+00	6.592E+00	

LOG S/S' = -1.0

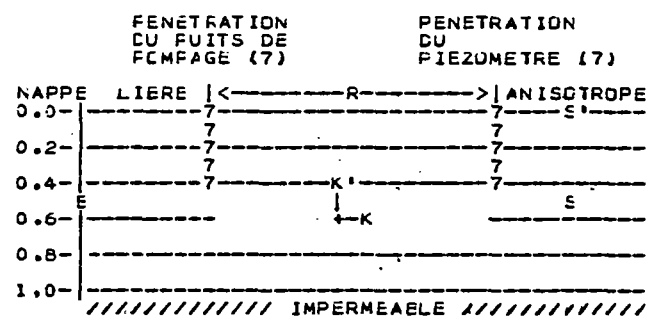
LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.627E-04	2.629E-04	2.658E-04	2.954E-04	5.437E-04	1.712E-03	5.668E-03	1.042E-02	1.529E-03	
3.162E-01	3.331E-03	3.341E-03	3.437E-03	4.347E-03	1.050E-02	3.323E-02	9.999E-02	1.053E-01	9.290E-02	
1.000E+00	1.102E-02	1.109E-02	1.186E-02	1.849E-02	5.272E-02	1.670E-01	3.940E-01	2.484E-01	5.184E-01	
3.162E+00	2.152E-02	2.189E-02	2.533E-02	5.044E-02	1.535E-01	4.717E-01	7.576E-01	4.716E-01	2.576E-01	
1.000E+01	3.321E-02	3.453E-02	4.630E-02	1.127E-01	3.507E-01	9.145E-01	1.082E+00	1.036E+00	9.857E-01	
1.000E+02	5.871E-02	7.170E-02	1.474E-01	4.322E-01	1.158E+00	1.721E+00	2.591E+00	3.145E+00	3.091E+00	
1.000E+03	9.616E-02	1.735E-01	4.691E-01	1.246E+00	1.978E+00	3.371E+00	4.979E+00	5.469E+00	5.386E+00	
1.000E+04	1.981E-01	4.956E-01	1.285E+00	2.068E+00	3.645E+00	5.792E+00	7.327E+00	7.790E+00	7.701E+00	

CNRS - CENTRE INTER REGIONAL DE CALCUL ELECTRONIQUE - CIRCE

PUITS PENETRANT DE 0.0 A 0.4 ET PIEZOMETRE DE 0.0 A 0.4
ABAQUE POUR L'INTERPRETATION DE FMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 7 7



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.108E-02	6.107E-02	6.107E-02	6.093E-02	5.973E-02	5.476E-02	3.886E-02	6.371E-03	6.516E-04
3.162E-01	7.749E-01	7.748E-01	7.744E-01	7.703E-01	7.426E-01	6.412E-01	3.380E-01	4.581E-02	1.435E-03
1.000E+00	2.561E+00	2.561E+00	2.557E+00	2.527E+00	2.374E+00	1.862E+00	6.705E-01	7.663E-02	1.560E-03
3.162E+00	4.998E+00	4.996E+00	4.981E+00	4.868E+00	4.405E+00	2.960E+00	8.164E-01	6.414E-02	1.960E-03
1.000E+01	7.692E+00	7.686E+00	7.633E+00	7.334E+00	6.266E+00	3.484E+00	8.723E-01	6.925E-02	3.432E-03
1.000E+02	1.328E+01	1.322E+01	1.268E+01	1.160E+01	9.079E+00	3.723E+00	9.305E-01	1.608E-01	5.320E-02
1.000E+03	1.886E+01	1.851E+01	1.718E+01	1.344E+01	8.333E+00	3.886E+00	1.435E+00	5.567E-01	1.025E+00
1.000E+04	2.416E+01	2.283E+01	1.902E+01	1.370E+01	8.609E+00	5.130E+00	3.812E+00	3.172E+00	2.133E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.108E-02	6.107E-02	6.107E-02	6.093E-02	5.985E-02	5.476E-02	3.886E-02	6.374E-03	6.957E-04
3.162E-01	7.749E-01	7.748E-01	7.744E-01	7.703E-01	7.427E-01	6.412E-01	3.380E-01	4.592E-02	1.509E-03
1.000E+00	2.561E+00	2.561E+00	2.557E+00	2.527E+00	2.374E+00	1.862E+00	6.710E-01	7.960E-02	1.910E-03
3.162E+00	4.998E+00	4.996E+00	4.981E+00	4.868E+00	4.405E+00	2.961E+00	8.192E-01	6.856E-02	3.367E-03
1.000E+01	7.692E+00	7.686E+00	7.633E+00	7.334E+00	6.266E+00	3.487E+00	8.836E-01	1.050E-01	1.011E-02
1.000E+02	1.328E+01	1.322E+01	1.268E+01	1.160E+01	8.065E+00	3.759E+00	1.055E+00	3.534E-01	3.096E-01
1.000E+03	1.886E+01	1.851E+01	1.719E+01	1.344E+01	8.398E+00	4.235E+00	2.373E+00	2.014E+00	2.026E+00
1.000E+04	2.416E+01	2.283E+01	1.904E+01	1.380E+01	9.155E+00	6.679E+00	5.165E+00	4.326E+00	4.267E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.108E-02	6.107E-02	6.107E-02	6.093E-02	5.985E-02	5.476E-02	3.886E-02	6.366E-03	7.081E-04
3.162E-01	7.749E-01	7.748E-01	7.744E-01	7.703E-01	7.427E-01	6.412E-01	3.381E-01	4.628E-02	1.751E-03
1.000E+00	2.561E+00	2.561E+00	2.557E+00	2.527E+00	2.374E+00	1.863E+00	6.726E-01	6.266E-02	3.165E-03
3.162E+00	4.998E+00	4.996E+00	4.981E+00	4.868E+00	4.405E+00	2.962E+00	8.283E-01	1.028E-01	9.735E-03
1.000E+01	7.692E+00	7.686E+00	7.633E+00	7.334E+00	6.267E+00	3.496E+00	9.192E-01	1.574E-01	5.182E-02
1.000E+02	1.328E+01	1.322E+01	1.268E+01	1.160E+01	8.103E+00	3.872E+00	1.428E+00	9.501E-01	1.016E+00
1.000E+03	1.886E+01	1.851E+01	1.719E+01	1.347E+01	8.595E+00	5.119E+00	3.756E+00	3.164E+00	3.124E+00
1.000E+04	2.416E+01	2.283E+01	1.907E+01	1.406E+01	1.030E+01	6.356E+00	6.378E+00	5.472E+00	5.407E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.108E-02	6.107E-02	6.107E-02	6.093E-02	5.985E-02	5.476E-02	3.886E-02	6.416E-03	7.473E-04
3.162E-01	7.749E-01	7.748E-01	7.744E-01	7.703E-01	7.427E-01	6.413E-01	3.386E-01	4.743E-02	2.577E-03
1.000E+00	2.561E+00	2.561E+00	2.557E+00	2.527E+00	2.374E+00	1.863E+00	6.779E-01	9.257E-02	6.630E-03
3.162E+00	4.998E+00	4.996E+00	4.981E+00	4.868E+00	4.406E+00	2.968E+00	8.567E-01	1.495E-01	4.862E-02
1.000E+01	7.692E+00	7.686E+00	7.633E+00	7.335E+00	6.270E+00	3.522E+00	1.030E+00	3.353E-01	2.972E-01
1.000E+02	1.328E+01	1.322E+01	1.268E+01	1.163E+01	8.158E+00	4.204E+00	2.348E+00	1.988E+00	2.001E+00
1.000E+03	1.886E+01	1.851E+01	1.720E+01	1.355E+01	9.123E+00	6.651E+00	5.137E+00	4.298E+00	4.240E+00
1.000E+04	2.416E+01	2.284E+01	1.917E+01	1.467E+01	1.197E+01	9.736E+00	7.540E+00	6.613E+00	6.537E+00

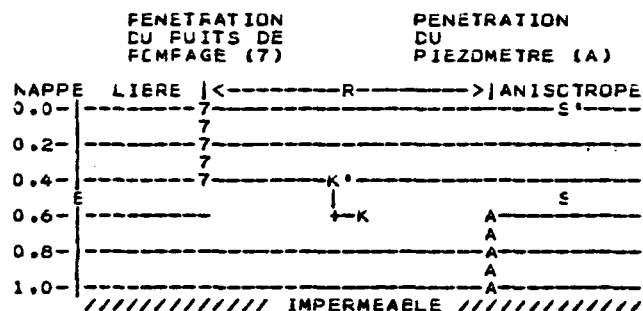
LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.108E-02	6.107E-02	6.107E-02	6.093E-02	5.984E-02	5.476E-02	3.886E-02	6.516E-03	6.325E-04
3.162E-01	7.749E-01	7.748E-01	7.744E-01	7.703E-01	7.427E-01	6.414E-01	3.400E-01	5.106E-02	5.706E-03
1.000E+00	2.561E+00	2.561E+00	2.557E+00	2.527E+00	2.374E+00	1.866E+00	6.944E-01	1.245E-01	3.951E-02
3.162E+00	4.998E+00	4.996E+00	4.981E+00	4.868E+00	4.407E+00	2.984E+00	9.445E-01	3.079E-01	2.689E-01
1.000E+01	7.692E+00	7.686E+00	7.633E+00	7.336E+00	6.280E+00	3.605E+00	1.357E+00	8.869E-01	5.522E-01
1.000E+02	1.328E+01	1.322E+01	1.288E+01	1.163E+01	8.321E+00	5.033E+00	3.715E+00	3.080E+00	3.044E+00
1.000E+03	1.886E+01	1.852E+01	1.722E+01	1.378E+01	1.021E+01	6.269E+00	6.291E+00	5.391E+00	5.332E+00
1.000E+04	2.417E+01	2.288E+01	1.943E+01	1.580E+01	1.361E+01	1.090E+01	8.627E+00	7.702E+00	7.640E+00

PUITS PENETRANT DE 0.0 A 0.4 ET PIEZOMETRE DE 0.6 A 1.0

TABEAU 7 A

ABAUQUE POUR L'INTERPRETATION DE FCMAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELETSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.051E-06	1.138E-06	1.029E-06	9.587E-07	6.574E-07	0.0	4.678E-04	6.481E-03	2.153E-03
3.162E-01	1.324E-05	1.325E-05	1.314E-05	1.238E-05	3.192E-06	7.323E-05	3.329E-02	1.032E-01	4.409E-03
1.000E+00	4.349E-05	4.360E-05	4.333E-05	3.484E-05	4.636E-06	8.551E-03	2.450E-01	2.033E-01	4.678E-03
3.162E+00	8.477E-05	8.451E-05	8.290E-05	4.565E-05	1.761E-04	1.036E-01	5.855E-01	2.176E-01	5.509E-03
1.000E+01	1.305E-04	1.305E-04	1.175E-04	4.771E-05	1.178E-02	4.207E-01	7.465E-01	2.249E-01	6.351E-03
1.000E+02	2.253E-04	2.120E-04	1.322E-04	1.221E-02	4.480E-01	9.755E-01	7.842E-01	3.184E-01	7.754E-02
1.000E+03	3.080E-04	2.271E-04	1.234E-02	4.510E-01	1.009E+00	1.017E+00	1.000E+00	1.061E+00	1.049E+00
1.000E+04	3.233E-04	1.247E-02	4.520E-01	1.013E+00	1.051E+00	1.260E+00	2.235E+00	3.068E+00	3.135E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.127E-06	1.139E-06	1.092E-06	8.839E-07	7.709E-07	3.234E-09	4.878E-04	6.481E-03	2.161E-03
3.162E-01	1.325E-05	1.326E-05	1.309E-05	1.222E-05	3.253E-06	7.333E-05	3.329E-02	1.033E-01	4.564E-03
1.000E+00	4.349E-05	4.364E-05	4.323E-05	3.469E-05	4.642E-06	8.551E-03	2.451E-01	2.044E-01	5.402E-03
3.162E+00	8.478E-05	8.452E-05	8.273E-05	4.553E-05	1.761E-04	1.036E-01	5.860E-01	2.236E-01	6.263E-03
1.000E+01	1.305E-04	1.305E-04	1.173E-04	4.768E-05	1.178E-02	4.207E-01	7.502E-01	2.464E-01	1.575E-02
1.000E+02	2.252E-04	2.119E-04	1.321E-04	1.221E-02	4.481E-01	9.799E-01	8.368E-01	3.277E-01	3.452E-02
1.000E+03	3.074E-04	2.281E-04	1.234E-02	4.510E-01	1.013E+00	1.077E+00	1.416E+00	1.575E+00	2.035E+00
1.000E+04	3.215E-04	1.247E-02	4.520E-01	1.017E+00	1.112E+00	1.717E+00	3.317E+00	4.200E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.130E-06	1.120E-06	9.293E-07	9.381E-07	5.141E-07	4.142E-08	4.880E-04	6.484E-03	2.185E-03
3.162E-01	1.325E-05	1.321E-05	1.295E-05	1.237E-05	2.986E-06	7.331E-05	3.329E-02	1.035E-01	5.058E-03
1.000E+00	4.347E-05	4.356E-05	4.305E-05	3.492E-05	4.399E-06	8.551E-03	2.451E-01	2.061E-01	7.666E-03
3.162E+00	8.474E-05	8.481E-05	8.247E-05	4.574E-05	1.757E-04	1.036E-01	5.877E-01	2.425E-01	1.513E-02
1.000E+01	1.304E-04	1.302E-04	1.172E-04	4.783E-05	1.178E-02	4.208E-01	7.615E-01	3.130E-01	7.573E-02
1.000E+02	2.249E-04	2.116E-04	1.320E-04	1.221E-02	4.482E-01	9.937E-01	9.917E-01	1.054E+00	1.042E+00
1.000E+03	3.072E-04	2.266E-04	1.234E-02	4.512E-01	1.028E+00	1.251E+00	2.226E+00	3.059E+00	3.127E+00
1.000E+04	3.213E-04	1.247E-02	4.521E-01	1.031E+00	1.288E+00	2.569E+00	4.455E+00	5.339E+00	5.407E+00

LOG S/S' = -1.5

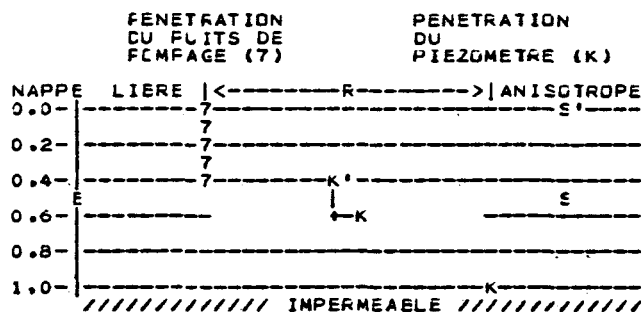
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.120E-06	1.100E-06	9.395E-07	1.024E-06	7.636E-07	0.0	4.880E-04	6.490E-03	2.260E-03
3.162E-01	1.323E-05	1.319E-05	1.294E-05	1.246E-05	3.239E-06	7.315E-05	3.329E-02	1.044E-01	6.682E-03
1.000E+00	4.347E-05	4.350E-05	4.299E-05	3.492E-05	4.675E-06	8.550E-03	2.454E-01	2.197E-01	1.728E-02
3.162E+00	8.479E-05	8.474E-05	8.246E-05	4.578E-05	1.760E-04	1.036E-01	5.926E-01	3.004E-01	7.154E-02
1.000E+01	1.305E-04	1.302E-04	1.171E-04	4.796E-05	1.178E-02	4.212E-01	7.978E-01	3.089E-01	3.259E-02
1.000E+02	2.251E-04	2.115E-04	1.317E-04	1.221E-02	4.486E-01	1.036E+00	1.350E+00	1.545E+00	2.009E+00
1.000E+03	3.080E-04	2.264E-04	1.234E-02	4.516E-01	1.071E+00	1.689E+00	3.250E+00	4.172E+00	4.241E+00
1.000E+04	3.222E-04	1.247E-02	4.525E-01	1.074E+00	1.734E+00	3.652E+00	5.596E+00	6.479E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.116E-06	1.137E-06	9.612E-07	7.690E-07	6.549E-07	0.0	4.859E-04	6.506E-03	2.460E-03
3.162E-01	1.327E-05	1.319E-05	1.303E-05	1.215E-05	3.071E-06	7.266E-05	3.329E-02	1.071E-01	1.228E-02
1.000E+00	4.347E-05	4.336E-05	4.314E-05	3.464E-05	4.278E-06	8.548E-03	2.501E-01	2.547E-01	5.555E-02
3.162E+00	8.470E-05	8.450E-05	8.271E-05	4.554E-05	1.751E-04	1.036E-01	6.084E-01	4.664E-01	3.056E-02
1.000E+01	1.302E-04	1.299E-04	1.173E-04	4.757E-05	1.178E-02	4.224E-01	9.013E-01	3.850E-01	3.753E-02
1.000E+02	2.248E-04	2.113E-04	1.322E-04	1.221E-02	4.498E-01	1.156E+00	2.141E+00	2.575E+00	3.047E+00
1.000E+03	3.075E-04	2.260E-04	1.234E-02	4.528E-01	1.193E+00	2.482E+00	4.369E+00	5.255E+00	5.332E+00
1.000E+04	3.229E-04	1.246E-02	4.538E-01	1.197E+00	2.528E+00	4.737E+00	6.676E+00	7.567E+00	7.641E+00

PUITS PENETRANT DE 0.0 A 0.4 ET PIEZOMETRE FONCTUEL A LA BASE DE LA NAPPE
 ABAQUE POUR L'INTERPRETATION DE FMPAGES EN NAPPE LIBRE ANISTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCVA

TABLEAU 7 K



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.170E-04	1.168E-04	1.152E-04	1.027E-04	3.430E-05	8.890E-06	1.115E-07	6.550E-03	2.301E-03
3.162E-01	1.483E-03	1.478E-03	1.436E-03	1.080E-03	1.039E-04	7.326E-07	3.589E-03	1.043E-01	4.712E-03
1.000E+00	4.858E-03	4.664E-03	4.536E-03	2.418E-03	1.077E-04	6.025E-06	1.413E-01	2.112E-01	4.954E-03
3.162E+00	9.548E-03	9.389E-03	8.003E-03	2.758E-03	1.097E-04	9.605E-03	4.822E-01	2.264E-01	5.866E-03
1.000E+01	1.466E-02	1.408E-02	1.010E-02	2.765E-03	1.167E-04	2.033E-01	6.539E-01	2.337E-01	6.665E-03
1.000E+02	2.472E-02	2.026E-02	1.051E-02	2.774E-03	2.118E-01	7.740E-01	6.904E-01	3.276E-01	7.979E-02
1.000E+03	3.096E-02	2.067E-02	1.051E-02	2.153E-01	7.882E-01	8.131E-01	8.871E-01	1.061E+00	1.051E+00
1.000E+04	3.138E-02	2.068E-02	1.052E-02	7.925E-01	8.276E-01	1.029E+00	2.051E+00	3.049E+00	3.136E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.170E-04	1.167E-04	1.151E-04	1.026E-04	3.386E-05	3.819E-07	1.226E-07	6.550E-03	2.305E-03
3.162E-01	1.483E-03	1.478E-03	1.436E-03	1.079E-03	1.037E-04	8.230E-07	3.589E-03	1.043E-01	4.674E-03
1.000E+00	4.858E-03	4.664E-03	4.536E-03	2.417E-03	1.075E-04	6.009E-06	1.413E-01	2.123E-01	5.755E-03
3.162E+00	9.548E-03	9.389E-03	8.002E-03	2.756E-03	1.098E-04	9.605E-03	4.826E-01	2.324E-01	6.751E-03
1.000E+01	1.466E-02	1.408E-02	1.010E-02	2.763E-03	1.168E-04	2.038E-01	6.571E-01	2.553E-01	2.068E-02
1.000E+02	2.472E-02	2.026E-02	1.051E-02	2.772E-03	2.118E-01	7.777E-01	7.380E-01	3.357E-01	3.526E-01
1.000E+03	3.097E-02	2.067E-02	1.052E-02	2.153E-01	7.919E-01	8.657E-01	1.272E+00	1.962E+00	2.036E+00
1.000E+04	3.139E-02	2.068E-02	1.052E-02	7.952E-01	8.808E-01	1.445E+00	3.113E+00	4.180E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.170E-04	1.168E-04	1.150E-04	1.025E-04	3.460E-05	3.562E-07	4.867E-07	6.551E-03	2.335E-03
3.162E-01	1.483E-03	1.479E-03	1.436E-03	1.079E-03	1.048E-04	7.321E-07	3.590E-03	1.046E-01	5.393E-03
1.000E+00	4.858E-03	4.664E-03	4.536E-03	2.416E-03	1.081E-04	5.762E-06	1.413E-01	2.160E-01	6.335E-03
3.162E+00	9.548E-03	9.389E-03	8.002E-03	2.755E-03	1.110E-04	9.605E-03	4.837E-01	2.513E-01	2.005E-02
1.000E+01	1.466E-02	1.408E-02	1.010E-02	2.762E-03	1.178E-04	2.039E-01	6.671E-01	3.221E-01	7.755E-02
1.000E+02	2.472E-02	2.026E-02	1.051E-02	2.772E-03	2.119E-01	7.890E-01	8.786E-01	1.053E+00	1.044E+00
1.000E+03	3.096E-02	2.067E-02	1.052E-02	2.153E-01	8.034E-01	1.020E+00	2.042E+00	3.040E+00	3.127E+00
1.000E+04	3.137E-02	2.068E-02	1.052E-02	8.077E-01	1.037E+00	2.251E+00	4.244E+00	5.319E+00	5.407E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.170E-04	1.167E-04	1.149E-04	1.024E-04	3.407E-05	1.276E-08	1.270E-07	6.554E-03	2.413E-03
3.162E-01	1.483E-03	1.478E-03	1.435E-03	1.079E-03	1.041E-04	2.992E-07	3.589E-03	1.054E-01	7.053E-03
1.000E+00	4.858E-03	4.664E-03	4.535E-03	2.416E-03	1.081E-04	5.219E-06	1.414E-01	2.273E-01	1.612E-02
3.162E+00	9.548E-03	9.389E-03	8.001E-03	2.756E-03	1.100E-04	9.604E-03	4.874E-01	3.090E-01	7.367E-02
1.000E+01	1.466E-02	1.408E-02	1.010E-02	2.763E-03	1.164E-04	2.040E-01	6.578E-01	5.165E-01	3.393E-01
1.000E+02	2.472E-02	2.025E-02	1.051E-02	2.772E-03	2.120E-01	8.243E-01	1.245E+00	1.953E+00	2.010E+00
1.000E+03	3.096E-02	2.067E-02	1.052E-02	2.155E-01	8.395E-01	1.417E+00	3.085E+00	4.152E+00	4.241E+00
1.000E+04	3.138E-02	2.067E-02	1.052E-02	8.431E-01	1.440E+00	3.311E+00	5.382E+00	6.456E+00	6.537E+00

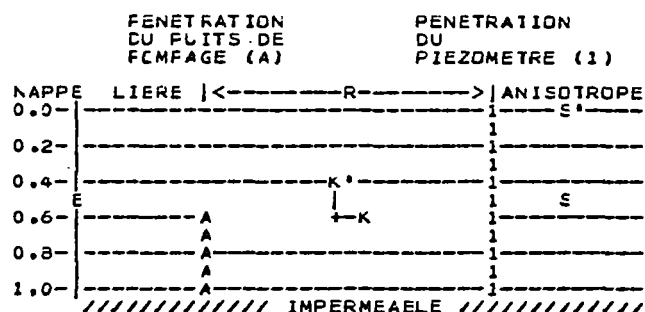
LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.170E-04	1.168E-04	1.148E-04	1.033E-04	3.455E-05	3.631E-07	0.0	6.555E-03	2.624E-03
3.162E-01	1.483E-03	1.478E-03	1.435E-03	1.080E-03	1.045E-04	3.229E-07	3.583E-03	1.077E-01	1.252E-02
1.000E+00	4.858E-03	4.663E-03	4.534E-03	2.416E-03	1.082E-04	3.635E-06	1.416E-01	2.615E-01	6.141E-02
3.162E+00	9.548E-03	9.389E-03	7.958E-03	2.757E-03	1.095E-04	9.597E-03	4.986E-01	4.731E-01	3.089E-01
1.000E+01	1.466E-02	1.408E-02	1.010E-02	2.764E-03	1.147E-04	2.043E-01	7.870E-01	5.641E-01	5.773E-01
1.000E+02	2.472E-02	2.025E-02	1.050E-02	2.771E-03	2.123E-01	9.242E-01	1.958E+00	2.557E+00	3.047E+00
1.000E+03	3.096E-02	2.067E-02	1.050E-02	2.158E-01	9.403E-01	2.164E+00	4.157E+00	5.238E+00	5.332E+00
1.000E+04	3.137E-02	2.066E-02	1.051E-02	9.448E-01	2.187E+00	4.389E+00	6.462E+00	7.546E+00	7.641E+00

PUITS PENETRANT DE 0.6 A 1.0 ET PIEZOMETRE COMPLET

TABLEAU A 1

ABaque pour l'interpretation de fcmpages en nappe libre anisotrope,
dans l'hypothese de Neuman, selon formules de Boulton - Streletsova



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0		-6.0		-5.0		-4.0		-3.0		-2.0		-1.0		0.0		1.0	
TT/R2S	R A B A T T E M E N T S										R E C U I T S							
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.491E-02	2.491E-02	2.491E-02	2.491E-02	2.491E-02	2.491E-02	2.345E-02	4.458E-03		
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.157E-01	2.287E-01	9.082E-03			
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.018E+00	4.375E-01	5.303E-03			
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.037E+00	1.761E+00	4.656E-01	9.943E-03					
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.100E+00	2.095E+00	4.740E-01	1.227E-02					
1.000E+02	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.417E+00	4.304E+00	2.151E+00	5.757E-01	5.001E-02					
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.717E+00	7.717E+00	7.679E+00	6.597E+00	4.364E+00	2.388E+00	1.411E+00	1.114E+00							
1.000E+04	1.002E+01	1.002E+01	5.583E+00	8.899E+00	6.657E+00	4.630E+00	3.755E+00	3.604E+00	3.267E+00									

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.491E-02	2.493E-02	2.350E-02	4.416E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.157E-01	2.289E-01	9.129E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.018E+00	4.392E-01	5.789E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.037E+00	1.761E+00	4.726E-01	1.209E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.100E+00	2.100E+00	4.583E-01	2.230E-02	
1.000E+02	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.379E+00	4.309E+00	2.209E+00	5.151E-01	3.679E-02	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.679E+00	6.602E+00	4.430E+00	2.846E+00	2.421E+00	2.151E+00	
1.000E+04	1.002E+01	1.002E+01	5.583E+00	8.904E+00	6.724E+00	5.131E+00	4.952E+00	4.796E+00	4.440E+00	

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.491E-02	2.491E-02	2.459E-02	4.266E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.159E-01	2.295E-01	9.280E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.019E+00	4.436E-01	1.154E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	1.761E+00	4.935E-01	2.151E-02	
1.000E+01	2.136E+00	2.136E+00	2.136E+00	2.136E+00	3.137E+00	3.101E+00	2.113E+00	5.736E-01	7.784E-03	
1.000E+02	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.380E+00	4.325E+00	2.279E+00	1.403E+00	1.107E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.680E+00	6.618E+00	4.621E+00	3.744E+00	3.594E+00	3.277E+00	
1.000E+04	1.002E+01	1.002E+01	5.584E+00	8.920E+00	6.917E+00	6.075E+00	6.185E+00	5.574E+00	5.591E+00	

LOG S/S' = -1.5

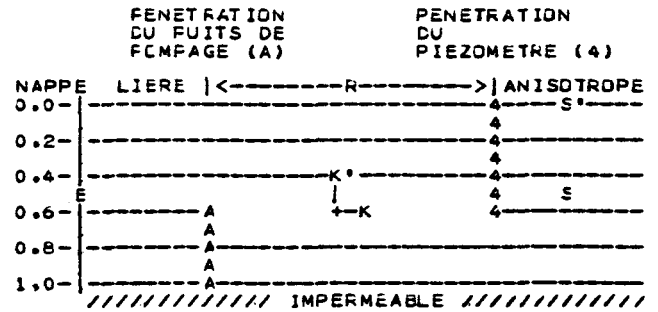
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.491E-02	2.518E-02	2.405E-02	3.675E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.165E-01	2.314E-01	9.683E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.045E+00	1.021E+00	4.565E-01	1.911E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.039E+00	1.772E+00	5.592E-01	7.262E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.103E+00	2.154E+00	7.938E-01	3.524E-01	
1.000E+02	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.382E+00	4.373E+00	2.819E+00	2.392E+00	2.122E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.683E+00	6.667E+00	5.102E+00	4.923E+00	4.766E+00	4.410E+00	
1.000E+04	1.002E+01	1.002E+01	5.587E+00	8.969E+00	7.404E+00	7.276E+00	7.377E+00	7.123E+00	6.726E+00	

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.491E-02	2.501E-02	2.577E-02	2.541E-02	2.611E-02	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.163E-01	3.184E-01	2.371E-01	1.258E-02	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.045E+00	1.027E+00	4.571E-01	5.649E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.045E+00	1.758E+00	7.453E-01	3.177E-01	
1.000E+01	2.136E+00	2.136E+00	2.136E+00	2.137E+00	3.137E+00	3.111E+00	2.274E+00	1.325E+00	1.031E+00	
1.000E+02	5.417E+00	5.417E+00	5.417E+00	5.418E+00	5.390E+00	4.512E+00	3.657E+00	2.495E+00	3.187E+00	
1.000E+03	7.717E+00	7.717E+00	7.718E+00	7.690E+00	6.807E+00	5.587E+00	6.097E+00	5.882E+00	5.507E+00	
1.000E+04	1.002E+01	1.002E+01	5.595E+00	9.110E+00	8.293E+00	8.457E+00	8.505E+00	8.226E+00	7.827E+00	

PUITS A PENETRATION DE 0.6 A 1.0 ET PIEZOMETRE OUVERT DE 0.0 A 0.6
 ABAQUE POUR L'INTERPRETATION DE FOMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABEAU A 4



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.629E-04	2.629E-04	2.659E-04	2.949E-04	5.367E-04	1.643E-03	5.198E-03	1.362E-02	3.088E-03
3.162E-01	3.334E-03	3.343E-03	3.439E-03	4.347E-03	1.048E-02	3.301E-02	1.039E-01	1.516E-01	6.298E-03
1.000E+00	1.102E-02	1.110E-02	1.186E-02	1.848E-02	5.265E-02	1.664E-01	4.764E-01	2.966E-01	6.559E-03
3.162E+00	2.154E-02	2.190E-02	2.534E-02	5.042E-02	1.533E-01	4.835E-01	9.698E-01	3.151E-01	7.353E-03
1.000E+01	3.323E-02	3.456E-02	4.631E-02	1.127E-01	3.501E-01	1.038E+00	1.201E+00	3.227E-01	1.013E-02
1.000E+02	5.876E-02	7.173E-02	1.473E-01	4.316E-01	1.288E+00	1.847E+00	1.246E+00	4.195E-01	7.951E-02
1.000E+03	9.622E-02	1.735E-01	4.685E-01	1.376E+00	2.105E+00	1.995E+00	1.467E+00	1.187E+00	1.071E+00
1.000E+04	1.981E-01	4.953E-01	1.415E+00	2.195E+00	2.154E+00	2.144E+00	2.743E+00	3.248E+00	3.185E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.629E-04	2.629E-04	2.659E-04	2.949E-04	5.368E-04	1.644E-03	5.205E-03	1.364E-02	3.079E-03
3.162E-01	3.334E-03	3.343E-03	3.439E-03	4.347E-03	1.048E-02	3.301E-02	1.039E-01	1.517E-01	6.421E-03
1.000E+00	1.102E-02	1.110E-02	1.186E-02	1.848E-02	5.265E-02	1.664E-01	4.764E-01	2.966E-01	7.227E-03
3.162E+00	2.154E-02	2.190E-02	2.534E-02	5.042E-02	1.533E-01	4.835E-01	9.703E-01	3.213E-01	9.962E-03
1.000E+01	3.323E-02	3.456E-02	4.631E-02	1.127E-01	3.502E-01	1.039E+00	1.205E+00	3.449E-01	2.127E-02
1.000E+02	5.876E-02	7.173E-02	1.473E-01	4.316E-01	1.288E+00	1.851E+00	1.299E+00	6.360E-01	3.567E-01
1.000E+03	9.622E-02	1.735E-01	4.685E-01	1.376E+00	2.110E+00	1.957E+00	1.894E+00	2.128E+00	2.073E+00
1.000E+04	1.981E-01	4.953E-01	1.415E+00	2.200E+00	2.216E+00	2.612E+00	3.851E+00	4.400E+00	4.324E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.629E-04	2.629E-04	2.658E-04	2.950E-04	5.369E-04	1.647E-03	5.228E-03	1.368E-02	3.053E-03
3.162E-01	3.334E-03	3.343E-03	3.439E-03	4.347E-03	1.048E-02	3.302E-02	1.040E-01	1.521E-01	6.818E-03
1.000E+00	1.102E-02	1.110E-02	1.186E-02	1.848E-02	5.265E-02	1.664E-01	4.767E-01	3.004E-01	9.523E-03
3.162E+00	2.154E-02	2.190E-02	2.534E-02	5.043E-02	1.533E-01	4.836E-01	9.723E-01	3.408E-01	2.058E-02
1.000E+01	3.323E-02	3.456E-02	4.631E-02	1.127E-01	3.502E-01	1.039E+00	1.217E+00	4.138E-01	7.757E-02
1.000E+02	5.876E-02	7.173E-02	1.473E-01	4.317E-01	1.288E+00	1.866E+00	1.458E+00	1.179E+00	1.064E+00
1.000E+03	9.622E-02	1.735E-01	4.685E-01	1.377E+00	2.125E+00	2.135E+00	2.726E+00	3.235E+00	3.176E+00
1.000E+04	1.981E-01	4.953E-01	1.415E+00	2.214E+00	2.397E+00	3.488E+00	5.017E+00	5.551E+00	5.467E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.629E-04	2.629E-04	2.658E-04	2.950E-04	5.383E-04	1.656E-03	5.302E-03	1.382E-02	2.971E-03
3.162E-01	3.334E-03	3.343E-03	3.439E-03	4.347E-03	1.048E-02	3.305E-02	1.042E-01	1.532E-01	8.146E-03
1.000E+00	1.102E-02	1.110E-02	1.186E-02	1.849E-02	5.266E-02	1.665E-01	4.776E-01	3.123E-01	1.852E-02
3.162E+00	2.154E-02	2.190E-02	2.534E-02	5.043E-02	1.533E-01	4.839E-01	9.786E-01	4.004E-01	7.307E-02
1.000E+01	3.323E-02	3.456E-02	4.631E-02	1.127E-01	3.503E-01	1.040E+00	1.254E+00	6.161E-01	3.426E-01
1.000E+02	5.876E-02	7.173E-02	1.473E-01	4.318E-01	1.289E+00	1.910E+00	1.866E+00	2.101E+00	2.046E+00
1.000E+03	9.622E-02	1.735E-01	4.687E-01	1.378E+00	2.169E+00	2.584E+00	3.823E+00	4.371E+00	4.296E+00
1.000E+04	1.981E-01	4.953E-01	1.417E+00	2.259E+00	2.850E+00	4.605E+00	6.178E+00	6.687E+00	6.599E+00

LOG S/S' = -1.0

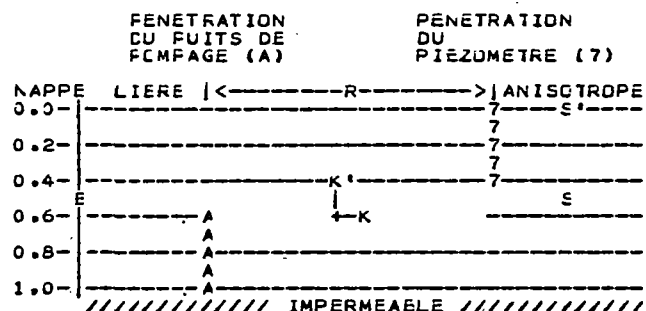
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.629E-04	2.629E-04	2.659E-04	2.951E-04	5.409E-04	1.685E-03	5.531E-03	1.423E-02	2.698E-03
3.162E-01	3.334E-03	3.343E-03	3.439E-03	4.348E-03	1.049E-02	3.314E-02	1.049E-01	1.567E-01	1.291E-02
1.000E+00	1.102E-02	1.110E-02	1.186E-02	1.849E-02	5.269E-02	1.668E-01	4.804E-01	3.481E-01	6.021E-02
3.162E+00	2.154E-02	2.190E-02	2.534E-02	5.044E-02	1.534E-01	4.848E-01	9.976E-01	5.712E-01	3.109E-01
1.000E+01	3.323E-02	3.456E-02	4.631E-02	1.127E-01	3.506E-01	1.044E+00	1.362E+00	1.107E+00	3.943E-01
1.000E+02	5.876E-02	7.173E-02	1.473E-01	4.321E-01	1.293E+00	2.035E+00	2.641E+00	3.151E+00	3.063E+00
1.000E+03	9.622E-02	1.735E-01	4.690E-01	1.382E+00	2.296E+00	3.402E+00	4.930E+00	5.467E+00	5.389E+00
1.000E+04	1.981E-01	4.953E-01	1.421E+00	2.386E+00	3.672E+00	5.719E+00	7.269E+00	7.786E+00	7.702E+00

UNKS - CENTRE INTER REGIONAL DE CALCUL ELE
CENTRE INTER REGIONAL DE CALCUL ELE
CENTRE INTER REGIONAL DE CALCUL ELE

PUITS PENETRANT DE 0.6 A 1.0 ET PIEZOMETRE DE 0.0 A 0.4

TABLEAU A 7

ABaque pour l'interpretation de fcmpages en nappe libre anisotrope,
dans l'hypothese de Nelman, selon formules de Boulton - Streletsky



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.200E-06	1.128E-06	6.754E-07	9.128E-07	6.423E-07	0.0	4.878E-04	6.481E-03	2.153E-C3
3.162E-01	1.335E-05	1.322E-05	1.258E-05	1.229E-05	3.046E-06	7.323E-05	3.329E-02	1.032E-01	4.405E-C3
1.000E+00	4.366E-05	4.370E-05	4.326E-05	3.470E-05	4.219E-06	8.550E-03	2.490E-01	2.032E-01	4.678E-C3
3.162E+00	8.502E-05	6.507E-05	6.088E-05	4.536E-05	1.753E-04	1.036E-01	5.855E-01	2.176E-01	5.509E-C3
1.000E+01	1.308E-04	1.307E-04	1.174E-04	4.711E-05	1.178E-02	4.207E-01	7.465E-01	2.249E-01	6.391E-C3
1.000E+02	2.257E-04	2.120E-04	1.315E-04	1.221E-02	4.480E-01	9.755E-01	7.842E-01	3.184E-01	7.754E-C2
1.000E+03	3.065E-04	2.264E-04	1.234E-02	4.510E-01	1.009E+00	1.017E+00	1.000E+00	1.061E+00	1.049E+C0
1.000E+04	3.235E-04	1.246E-02	4.520E-01	1.013E+00	1.051E+00	1.260E+00	2.235E+00	3.068E+00	3.135E+C0

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.212E-06	1.079E-06	6.626E-07	7.981E-07	8.254E-07	9.154E-08	4.878E-04	6.481E-03	2.161E-C3
3.162E-01	1.336E-05	1.321E-05	1.255E-05	1.203E-05	3.194E-06	7.331E-05	3.329E-02	1.033E-01	4.564E-C3
1.000E+00	4.366E-05	4.363E-05	4.311E-05	3.430E-05	4.298E-06	8.550E-03	2.491E-01	2.044E-01	5.402E-C3
3.162E+00	8.501E-05	6.456E-05	6.257E-05	4.481E-05	1.754E-04	1.036E-01	5.860E-01	2.236E-01	6.263E-C3
1.000E+01	1.308E-04	1.306E-04	1.169E-04	4.657E-05	1.178E-02	4.207E-01	7.502E-01	2.464E-01	1.575E-C2
1.000E+02	2.255E-04	2.117E-04	1.311E-04	1.221E-02	4.481E-01	9.799E-01	8.368E-01	3.277E-01	4.593E-C2
1.000E+03	3.075E-04	2.270E-04	1.233E-02	4.510E-01	1.013E+00	1.077E+00	1.416E+00	1.975E+00	2.025E+C0
1.000E+04	3.210E-04	1.247E-02	4.520E-01	1.017E+00	1.112E+00	1.717E+00	3.317E+00	4.200E+00	4.268E+C0

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.211E-06	1.052E-06	6.626E-07	8.721E-07	5.403E-07	1.381E-07	4.881E-04	6.483E-03	2.185E-C3
3.162E-01	1.337E-05	1.319E-05	1.263E-05	1.217E-05	2.937E-06	7.337E-05	3.329E-02	1.035E-01	5.058E-C3
1.000E+00	4.367E-05	4.362E-05	4.288E-05	3.441E-05	4.074E-06	8.550E-03	2.491E-01	2.041E-01	7.666E-C3
3.162E+00	8.501E-05	6.450E-05	6.211E-05	4.497E-05	1.751E-04	1.036E-01	5.677E-01	2.425E-01	1.913E-C2
1.000E+01	1.308E-04	1.302E-04	1.154E-04	4.666E-05	1.178E-02	4.208E-01	7.619E-01	3.130E-01	7.573E-C2
1.000E+02	2.253E-04	2.111E-04	1.304E-04	1.221E-02	4.482E-01	9.937E-01	9.917E-01	1.054E+00	1.042E+C0
1.000E+03	3.070E-04	2.252E-04	1.233E-02	4.512E-01	1.028E+00	1.251E+00	2.226E+00	3.059E+00	3.127E+C0
1.000E+04	3.209E-04	1.246E-02	4.521E-01	1.031E+00	1.288E+00	2.569E+00	4.455E+00	5.339E+00	5.407E+C0

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.214E-06	1.074E-06	7.624E-07	1.030E-06	8.460E-07	0.0	4.880E-04	6.489E-03	2.260E-C3
3.162E-01	1.337E-05	1.315E-05	1.267E-05	1.229E-05	3.237E-06	7.316E-05	3.329E-02	1.044E-01	6.682E-C3
1.000E+00	4.367E-05	4.347E-05	4.261E-05	3.450E-05	4.392E-06	8.550E-03	2.494E-01	2.197E-01	1.728E-C2
3.162E+00	8.504E-05	6.462E-05	6.172E-05	4.509E-05	1.753E-04	1.036E-01	5.928E-01	3.004E-01	7.154E-C2
1.000E+01	1.308E-04	1.258E-04	1.160E-04	4.684E-05	1.178E-02	4.212E-01	7.978E-01	5.089E-01	3.359E-C1
1.000E+02	2.250E-04	2.105E-04	1.299E-04	1.221E-02	4.486E-01	1.036E+00	1.350E+00	1.545E+00	2.009E+C0
1.000E+03	3.071E-04	2.249E-04	1.233E-02	4.516E-01	1.071E+00	1.689E+00	3.290E+00	4.172E+00	4.241E+C0
1.000E+04	3.205E-04	1.246E-02	4.525E-01	1.074E+00	1.734E+00	3.652E+00	5.596E+00	6.479E+00	6.537E+C0

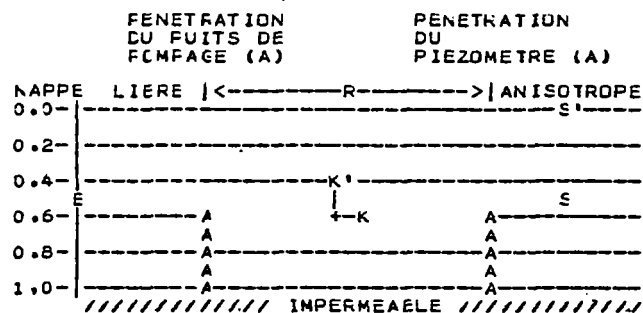
LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.180E-06	1.023E-06	7.603E-07	7.347E-07	7.793E-07	0.0	4.859E-04	6.506E-03	2.460E-C3
3.162E-01	1.336E-05	1.305E-05	1.267E-05	1.200E-05	3.094E-06	7.259E-05	3.329E-02	1.071E-01	1.222E-C2
1.000E+00	4.364E-05	4.320E-05	4.254E-05	3.420E-05	4.029E-06	8.548E-03	2.501E-01	2.547E-01	5.555E-C2
3.162E+00	8.490E-05	6.412E-05	6.175E-05	4.470E-05	1.745E-04	1.036E-01	6.084E-01	4.664E-01	3.056E-C1
1.000E+01	1.303E-04	1.291E-04	1.159E-04	4.626E-05	1.177E-02	4.224E-01	9.013E-01	5.850E-01	9.753E-C1
1.000E+02	2.243E-04	2.057E-04	1.300E-04	1.221E-02	4.493E-01	1.156E+00	2.141E+00	2.575E+00	3.047E+C0
1.000E+03	3.062E-04	2.235E-04	1.233E-02	4.528E-01	1.193E+00	2.482E+00	4.369E+00	5.255E+00	5.332E+C0
1.000E+04	3.211E-04	1.246E-02	4.537E-01	1.197E+00	2.528E+00	4.737E+00	6.676E+00	7.567E+00	7.641E+C0

PUITS PENETRANT DE 0.6 A 1.0 ET PIEZOMETRE DE 0.6 A 1.0

TABEAL A A

ABAQUE POUR L'INTERPRETATION DE FCMPAGE EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.187E-02	6.186E-02	6.186E-02	6.181E-02	6.145E-02	5.968E-02	5.435E-02	3.810E-02	6.578E-03
3.162E-01	7.848E-01	7.848E-01	7.847E-01	7.833E-01	7.741E-01	7.402E-01	6.332E-01	3.442E-01	1.342E-02
1.000E+00	2.594E+00	2.594E+00	2.593E+00	2.583E+00	2.532E+00	2.361E+00	1.830E+00	6.511E-01	1.350E-02
3.162E+00	5.062E+00	5.062E+00	5.057E+00	5.019E+00	4.865E+00	4.368E+00	2.944E+00	6.503E-01	1.525E-02
1.000E+01	7.751E+00	7.789E+00	7.772E+00	7.672E+00	7.316E+00	6.192E+00	3.436E+00	6.566E-01	1.555E-02
1.000E+02	1.345E+01	1.343E+01	1.332E+01	1.289E+01	1.152E+01	7.953E+00	3.493E+00	7.767E-01	1.079E-01
1.000E+03	1.915E+01	1.903E+01	1.859E+01	1.713E+01	1.333E+01	8.047E+00	3.618E+00	1.395E+00	1.072E+00
1.000E+04	2.475E+01	2.431E+01	2.284E+01	1.895E+01	1.339E+01	8.178E+00	4.454E+00	3.232E+00	3.139E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.187E-02	6.186E-02	6.186E-02	6.181E-02	6.145E-02	5.968E-02	5.435E-02	3.810E-02	6.587E-03
3.162E-01	7.848E-01	7.848E-01	7.847E-01	7.833E-01	7.741E-01	7.402E-01	6.332E-01	3.442E-01	1.367E-02
1.000E+00	2.594E+00	2.594E+00	2.593E+00	2.583E+00	2.532E+00	2.361E+00	1.830E+00	6.511E-01	1.510E-02
3.162E+00	5.062E+00	5.062E+00	5.057E+00	5.019E+00	4.865E+00	4.368E+00	2.944E+00	6.550E-01	1.973E-02
1.000E+01	7.751E+00	7.789E+00	7.772E+00	7.672E+00	7.316E+00	6.192E+00	3.437E+00	7.147E-01	3.663E-02
1.000E+02	1.345E+01	1.343E+01	1.332E+01	1.289E+01	1.152E+01	7.990E+00	3.522E+00	5.517E-01	3.668E-01
1.000E+03	1.915E+01	1.903E+01	1.859E+01	1.713E+01	1.333E+01	8.078E+00	3.674E+00	2.197E+00	2.044E+00
1.000E+04	2.475E+01	2.431E+01	2.284E+01	1.895E+01	1.342E+01	8.445E+00	5.367E+00	4.345E+00	4.265E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.187E-02	6.186E-02	6.186E-02	6.181E-02	6.146E-02	5.968E-02	5.435E-02	3.810E-02	6.615E-03
3.162E-01	7.848E-01	7.848E-01	7.847E-01	7.833E-01	7.741E-01	7.402E-01	6.332E-01	3.442E-01	1.446E-02
1.000E+00	2.594E+00	2.594E+00	2.593E+00	2.583E+00	2.532E+00	2.361E+00	1.830E+00	6.539E-01	1.905E-02
3.162E+00	5.062E+00	5.062E+00	5.057E+00	5.019E+00	4.865E+00	4.368E+00	2.944E+00	7.059E-01	3.569E-02
1.000E+01	7.751E+00	7.789E+00	7.772E+00	7.672E+00	7.316E+00	6.192E+00	3.441E+00	7.703E-01	1.056E-01
1.000E+02	1.345E+01	1.343E+01	1.332E+01	1.289E+01	1.152E+01	7.990E+00	3.609E+00	1.388E+00	1.065E+00
1.000E+03	1.915E+01	1.903E+01	1.859E+01	1.713E+01	1.333E+01	8.169E+00	4.445E+00	3.223E+00	3.130E+00
1.000E+04	2.475E+01	2.431E+01	2.284E+01	1.896E+01	1.352E+01	9.033E+00	6.440E+00	5.478E+00	5.407E+00

LOG S/S' = -1.5

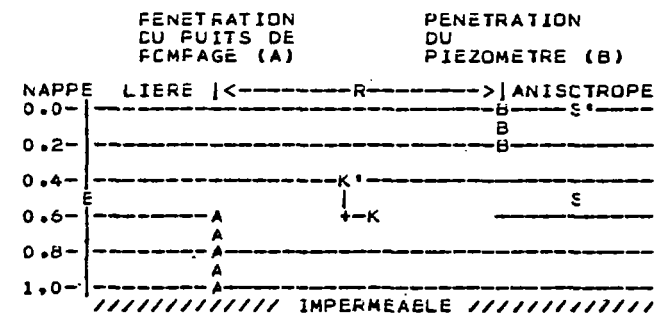
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.187E-02	6.186E-02	6.186E-02	6.181E-02	6.146E-02	5.968E-02	5.435E-02	3.810E-02	6.703E-03
3.162E-01	7.848E-01	7.848E-01	7.847E-01	7.833E-01	7.741E-01	7.402E-01	6.332E-01	3.442E-01	1.697E-02
1.000E+00	2.594E+00	2.594E+00	2.593E+00	2.583E+00	2.532E+00	2.361E+00	1.830E+00	6.605E-01	3.287E-02
3.162E+00	5.062E+00	5.062E+00	5.057E+00	5.019E+00	4.865E+00	4.368E+00	2.945E+00	7.549E-01	1.004E-01
1.000E+01	7.751E+00	7.789E+00	7.772E+00	7.672E+00	7.316E+00	6.192E+00	3.454E+00	5.303E-01	3.746E-01
1.000E+02	1.345E+01	1.343E+01	1.332E+01	1.289E+01	1.152E+01	8.008E+00	3.847E+00	2.171E+00	2.018E+00
1.000E+03	1.915E+01	1.903E+01	1.859E+01	1.713E+01	1.335E+01	8.417E+00	5.339E+00	4.317E+00	4.242E+00
1.000E+04	2.475E+01	2.431E+01	2.284E+01	1.897E+01	1.377E+01	9.939E+00	7.560E+00	6.615E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	6.187E-02	6.186E-02	6.186E-02	6.181E-02	6.145E-02	5.968E-02	5.435E-02	3.805E-02	6.949E-03
3.162E-01	7.848E-01	7.848E-01	7.847E-01	7.833E-01	7.741E-01	7.402E-01	6.332E-01	3.450E-01	2.509E-02
1.000E+00	2.594E+00	2.594E+00	2.593E+00	2.583E+00	2.532E+00	2.361E+00	1.830E+00	6.602E-01	6.536E-02
3.162E+00	5.062E+00	5.062E+00	5.057E+00	5.019E+00	4.865E+00	4.368E+00	2.947E+00	6.818E-01	3.425E-01
1.000E+01	7.751E+00	7.789E+00	7.772E+00	7.672E+00	7.316E+00	6.192E+00	3.451E+00	1.316E+00	5.561E-01
1.000E+02	1.345E+01	1.343E+01	1.332E+01	1.289E+01	1.152E+01	8.043E+00	4.360E+00	3.140E+00	3.050E+00
1.000E+03	1.915E+01	1.903E+01	1.859E+01	1.713E+01	1.339E+01	8.947E+00	6.354E+00	5.397E+00	5.333E+00
1.000E+04	2.475E+01	2.431E+01	2.284E+01	1.901E+01	1.429E+01	1.096E+01	8.634E+00	7.703E+00	7.641E+00

PUITS PENETRANT DE 0.6 A 1.0 ET PIEZOMETRE DE 0.3 A 3.2
ABaque pour l'interpretation de fcmpages en nappe libre anisotrope,
dans l'hypothese de Neuman, selon formules de Boulton - Streletsova

TABLEAU A B



LOG S/S' = -3.0																		
LOG K'R2/KB2	-7.0		-6.0		-5.0		-4.0		-3.0		-2.0		-1.0		0.0		1.0	
TT/R2S	R A B A T T E M E N T S									R E C U I T S								
1.000E-01	3.634E-07	2.140E-07	2.136E-07	1.487E-07	1.348E-07	0.0	7.255E-06	3.571E-03	1.115E-03									
3.162E-01	3.182E-06	3.156E-06	3.050E-06	2.699E-06	8.426E-07	0.0	7.521E-03	5.207E-02	2.309E-02									
1.000E+00	1.007E-05	1.044E-05	1.005E-05	8.055E-06	1.401E-05	1.463E-04	1.022E-01	1.036E-01	2.577E-02									
3.162E+00	1.985E-05	1.983E-05	1.931E-05	1.090E-05	1.455E-06	1.965E-02	2.723E-01	1.120E-01	3.427E-02									
1.000E+01	3.051E-05	3.062E-05	2.766E-05	1.171E-05	1.959E-04	1.570E-01	3.556E-01	1.190E-01	6.354E-02									
1.000E+02	5.233E-05	4.654E-05	3.303E-05	2.115E-04	1.644E-01	4.394E-01	3.858E-01	2.095E-01	7.475E-02									
1.000E+03	6.616E-05	5.231E-05	5.801E-05	1.652E-01	4.499E-01	4.731E-01	5.976E-01	9.315E-01	1.027E+00									
1.000E+04	6.661E-05	5.165E-05	6.711E-05	4.512E-01	4.840E-01	7.124E-01	1.804E+00	2.685E+00	3.067E+00									

LOG S/S' = -2.5										
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	3.608E-07	2.555E-07	2.064E-07	1.167E-07	1.987E-07	0.0	0.0	3.560E-03	1.138E-03	
3.162E-01	3.183E-06	3.208E-06	3.027E-06	2.637E-06	7.175E-07	0.0	7.491E-03	5.214E-02	2.451E-02	
1.000E+00	1.008E-05	1.048E-05	9.558E-06	8.047E-06	5.266E-07	1.346E-04	1.022E-01	1.048E-01	3.342E-02	
3.162E+00	1.989E-05	1.989E-05	1.903E-05	1.100E-05	3.0	1.961E-02	2.727E-01	1.179E-01	6.248E-02	
1.000E+01	3.054E-05	3.070E-05	2.722E-05	1.129E-05	1.836E-04	1.569E-01	3.552E-01	1.395E-01	1.777E-02	
1.000E+02	5.230E-05	5.099E-05	3.086E-05	1.998E-04	1.643E-01	4.437E-01	4.374E-01	4.132E-01	3.411E-01	
1.000E+03	6.557E-05	5.730E-05	5.341E-05	1.651E-01	4.543E-01	5.320E-01	1.005E+00	1.621E+00	1.558E+00	
1.000E+04	6.642E-05	5.665E-05	6.252E-05	4.555E-01	5.438E-01	1.160E+00	2.859E+00	4.003E+00	4.212E+00	

LDG S/S' = -2.0										
LDG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0										
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	3.681E-07	1.893E-07	1.825E-07	1.937E-07	0.0	0.0	0.0	0.0	3.925E-03	1.213E-03
3.162E-01	3.208E-06	3.124E-06	2.929E-06	2.824E-06	0.0	0.0	0.0	7.397E-03	5.236E-02	3.072E-02
1.000E+00	1.014E-05	1.033E-05	1.049E-05	8.219E-06	0.0	0.0	9.511E-05	1.020E-01	1.065E-01	5.922E-02
3.162E+00	1.997E-05	1.979E-05	1.885E-05	1.041E-05	0.0	0.0	1.949E-02	2.740E-01	1.363E-01	1.723E-02
1.000E+01	3.058E-05	3.053E-05	2.721E-05	8.010E-06	1.428E-04	1.567E-01	3.705E-01	2.048E-01	7.312E-02	
1.000E+02	5.173E-05	5.159E-05	3.176E-05	1.598E-04	1.641E-01	4.570E-01	5.852E-01	5.252E-01	1.020E+00	
1.000E+03	6.405E-05	5.673E-05	5.574E-05	1.649E-01	4.679E-01	7.335E-01	1.756E+00	2.681E+00	3.079E+00	
1.000E+04	6.450E-05	5.814E-05	6.485E-05	4.691E-01	7.175E-01	1.993E+00	3.970E+00	5.131E+00	5.348E+00	

LOG S/S' = -1.5										
LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0										
TT/R2S	R A B A T T E M E N T S					R E C U I T S				
1.000E-01	3.839E-07	1.888E-07	1.747E-07	2.112E-07	0.0	0.0	0.0	3.816E-03	1.444E-03	
3.162E-01	3.180E-06	3.119E-06	3.011E-06	2.573E-06	0.0	0.0	7.101E-03	5.305E-02	4.959E-02	
1.000E+00	1.011E-05	1.033E-05	1.025E-05	7.093E-06	0.0	0.0	1.014E-01	1.200E-01	1.562E-02	
3.162E+00	1.987E-05	1.964E-05	2.018E-05	6.613E-06	0.0	1.911E-02	2.760E-01	1.531E-01	6.926E-02	
1.000E+01	3.064E-05	3.034E-05	2.939E-05	0.0	1.501E-05	1.561E-01	4.054E-01	3.956E-01	3.264E-01	
1.000E+02	5.310E-05	4.993E-05	3.627E-05	3.166E-05	1.635E-01	4.979E-01	9.788E-01	1.757E+00	1.673E+00	
1.000E+03	6.828E-05	5.576E-05	6.204E-05	1.643E-01	5.094E-01	1.132E+00	2.831E+00	3.977E+00	4.186E+00	

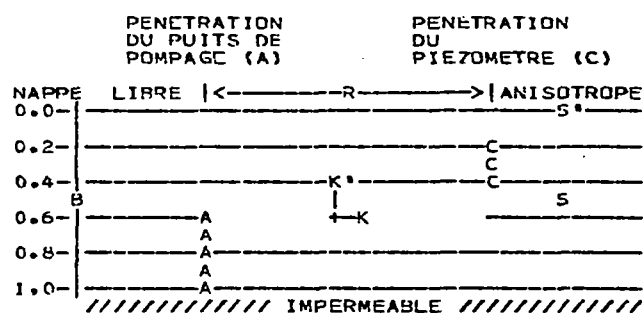
LOG S/S' = -1.0											
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0		
TT/R2S	R A B A T T E M E N T S					R E C U I T S					
1.000E-01	3.590E-07	1.742E-07	2.467E-07	0.0	0.0	0.0	0.0	3.510E-03	2.111E-03		
3.162E-01	3.126E-06	3.064E-06	3.160E-06	8.751E-07	0.0	0.0	6.168E-03	5.528E-02	1.130E-02		
1.000E+00	1.005E-05	1.014E-05	1.036E-05	2.677E-06	0.0	0.0	9.569E-02	1.551E-01	5.819E-02		
3.162E+00	1.983E-05	1.946E-05	1.994E-05	0.0	0.0	1.783E-02	2.902E-01	1.561E-01	2.956E-01		
1.000E+01	3.056E-05	3.015E-05	2.642E-05	0.0	0.0	1.541E-01	5.055E-01	3.604E-01	9.563E-01		
1.000E+02	5.398E-05	4.911E-05	3.281E-05	0.0	1.615E-01	6.142E-01	1.712E+00	2.802E+00	3.002E+00		
1.000E+03	7.013E-05	5.340E-05	6.618E-05	1.623E-01	6.276E-01	1.906E+00	3.885E+00	5.055E+00	5.276E+00		

PUITS A PENETRATION DE 0.6 A 1.0 ET PIEZOMETRE OUVERT DE 0.2 A 0.4

TABLEAU A C

ABaque POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.955E-06	1.831E-06	1.638E-06	1.582E-06	1.194E-06	0.0	9.611E-04	1.298E-02	3.209E-03	
3.162E-01	2.294E-05	2.277E-05	2.252E-05	2.140E-05	5.010E-06	1.448E-04	5.903E-02	1.542E-01	6.558E-03	
1.000E+00	7.534E-05	7.522E-05	7.471E-05	6.009E-05	5.964E-06	1.694E-02	3.958E-01	3.028E-01	6.927E-03	
3.162E+00	1.468E-04	1.468E-04	1.433E-04	7.730E-05	3.459E-04	1.875E-01	8.985E-01	3.228E-01	8.056E-03	
1.000E+01	2.259E-04	2.255E-04	2.029E-04	7.891E-05	2.335E-02	6.843E-01	1.137E+00	3.294E-01	1.186E-02	
1.000E+02	3.897E-04	3.661E-04	2.249E-04	2.420E-02	7.316E-01	1.511E+00	1.175E+00	4.142E-01	8.960E-02	
1.000E+03	5.322E-04	3.889E-04	2.442E-02	7.367E-01	1.567E+00	1.551E+00	1.337E+00	1.075E+00	1.038E+00	
1.000E+04	5.561E-04	2.466E-02	7.383E-01	1.573E+00	1.608E+00	1.727E+00	2.333E+00	2.946E+00	3.087E+00	

LOG S/S' = -2.5

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.943E-06	1.819E-06	1.650E-06	1.564E-06	1.164E-06	0.0	9.549E-04	1.297E-02	3.232E-03	
3.162E-01	2.292E-05	2.281E-05	2.251E-05	2.131E-05	4.704E-06	1.429E-04	5.901E-02	1.543E-01	6.785E-03	
1.000E+00	7.527E-05	7.525E-05	7.462E-05	5.998E-05	4.886E-06	1.694E-02	3.957E-01	3.037E-01	7.926E-03	
3.162E+00	1.467E-04	1.468E-04	1.432E-04	7.691E-05	3.431E-04	1.875E-01	8.986E-01	3.281E-01	1.171E-02	
1.000E+01	2.257E-04	2.255E-04	2.027E-04	7.786E-05	2.334E-02	6.842E-01	1.139E+00	3.488E-01	2.590E-02	
1.000E+02	3.896E-04	3.662E-04	2.238E-04	2.419E-02	7.315E-01	1.513E+00	1.214E+00	6.013E-01	3.604E-01	
1.000E+03	5.319E-04	3.892E-04	2.441E-02	7.366E-01	1.570E+00	1.594E+00	1.659E+00	1.908E+00	2.001E+00	
1.000E+04	5.541E-04	2.465E-02	7.382E-01	1.576E+00	1.651E+00	2.071E+00	3.300E+00	4.049E+00	4.212E+00	

LOG S/S' = -2.0

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.908E-06	1.788E-06	1.618E-06	1.599E-06	6.989E-07	0.0	9.354E-04	1.292E-02	3.306E-03	
3.162E-01	2.287E-05	2.274E-05	2.248E-05	2.123E-05	3.695E-06	1.353E-04	5.895E-02	1.543E-01	7.507E-03	
1.000E+00	7.527E-05	7.517E-05	7.458E-05	5.976E-05	2.299E-06	1.691E-02	3.956E-01	3.066E-01	1.124E-02	
3.162E+00	1.467E-04	1.466E-04	1.430E-04	7.587E-05	3.353E-04	1.874E-01	8.991E-01	3.446E-01	2.521E-02	
1.000E+01	2.257E-04	2.253E-04	2.027E-04	7.511E-05	2.332E-02	6.840E-01	1.146E+00	4.085E-01	8.771E-02	
1.000E+02	3.894E-04	3.656E-04	2.204E-04	2.417E-02	7.313E-01	1.521E+00	1.329E+00	1.068E+00	1.031E+00	
1.000E+03	5.314E-04	3.856E-04	2.439E-02	7.364E-01	1.578E+00	1.719E+00	2.324E+00	2.937E+00	3.079E+00	
1.000E+04	5.527E-04	2.464E-02	7.380E-01	1.584E+00	1.777E+00	2.764E+00	4.378E+00	5.174E+00	5.347E+00	

LOG S/S' = -1.5

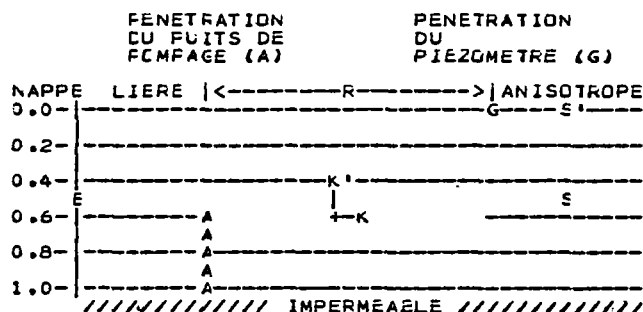
LOG K*R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.946E-06	1.807E-06	1.537E-06	1.399E-06	2.297E-07	0.0	8.734E-04	1.278E-02	3.536E-03	
3.162E-01	2.294E-05	2.274E-05	2.237E-05	2.087E-05	1.548E-06	1.114E-04	5.875E-02	1.545E-01	9.827E-03	
1.000E+00	7.532E-05	7.518E-05	7.441E-05	5.851E-05	0.0	1.684E-02	3.950E-01	3.155E-01	2.311E-02	
3.162E+00	1.465E-04	1.467E-04	1.426E-04	7.313E-05	3.114E-04	1.872E-01	9.004E-01	3.952E-01	8.333E-02	
1.000E+01	2.259E-04	2.253E-04	2.011E-04	6.706E-05	2.324E-02	6.834E-01	1.168E+00	5.821E-01	3.473E-01	
1.000E+02	3.897E-04	3.651E-04	2.120E-04	2.409E-02	7.307E-01	1.546E+00	1.632E+00	1.883E+00	1.977E+00	
1.000E+03	5.313E-04	3.825E-04	2.431E-02	7.358E-01	1.603E+00	2.043E+00	3.272E+00	4.023E+00	4.186E+00	
1.000E+04	5.529E-04	2.461E-02	7.374E-01	1.609E+00	2.104E+00	3.727E+00	5.489E+00	6.306E+00	6.485E+00	

LOG S/S' = -1.0

LOG K ¹ R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.971E-06	1.857E-06	1.483E-06	1.050E-06	0.0	0.0	6.766E-04	1.237E-02	4.206E-03	
3.162E-01	2.292E-05	2.278E-05	2.229E-05	1.997E-05	0.0	3.701E-05	5.813E-02	1.553E-01	1.741E-02	
1.000E+00	7.531E-05	7.507E-05	7.398E-05	5.610E-05	0.0	1.660E-02	3.934E-01	3.425E-01	7.075E-02	
3.162E+00	1.467E-04	1.465E-04	1.416E-04	6.545E-05	2.348E-04	1.865E-01	9.046E-01	5.387E-01	3.176E-01	
1.000E+01	2.255E-04	2.251E-04	1.981E-04	4.279E-05	2.300E-02	6.815E-01	1.232E+00	1.001E+00	9.670E-01	
1.000E+02	3.896E-04	3.638E-04	1.858E-04	2.385E-02	7.288E-01	1.617E+00	2.240E+00	2.858E+00	3.002E+00	
1.000E+03	5.309E-04	3.724E-04	2.405E-02	7.339E-01	1.675E+00	2.677E+00	4.293E+00	5.097E+00	5.275E+00	
1.000E+04	5.550E-04	2.451E-02	7.353E-01	1.682E+00	2.740E+00	4.752E+00	6.555E+00	7.392E+00	7.580E+00	

PUITS PENETRANT DE 0.6 A 1.0 ET PIEZOMETRE FNCTUEL AU SCHMET DE LA NAPPE
 ABAQUE POUR L'INTERPRETATION DE FMPAGES EN NAPPE LIBRE ANISTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCVA

TABLEAU A G



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	0.0			0.0				0.0			1.040E-09	1.104E-07	0.0	0.0	0.0	7.660E-07	2.548E-06		
3.162E-01	0.0			0.0				0.0			0.0	2.274E-07	1.573E-07	3.854E-07	6.125E-05	4.642E-05			
1.000E+00	0.0			0.0				0.0			0.0	5.301E-07	4.277E-07	3.301E-05	6.565E-04	2.029E-04			
3.162E+00	0.0			0.0				0.0			0.0	1.105E-06	1.630E-06	4.621E-04	3.010E-03	7.226E-04			
1.000E+01	0.0			0.0				0.0			0.0	1.641E-06	5.484E-05	2.674E-03	1.052E-02	2.616E-03			
1.000E+02	0.0			0.0				0.0			5.981E-07	5.960E-05	3.348E-03	3.425E-02	1.028E-01	6.076E-02			
1.000E+03	0.0			0.0				1.710E-06	5.905E-05	3.434E-03	4.166E-02	3.241E-01	5.203E-01	1.035E+00					
1.000E+04	0.0			0.0				1.731E-06	3.442E-03	4.256E-02	3.656E-01	1.855E+00	3.025E+00	3.134E+00					

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	0.0			0.0				0.0				3.750E-08	1.842E-08	4.163E-08	4.827E-08	2.261E-06	5.454E-06		
3.162E-01	0.0			0.0				0.0				0.0	4.515E-08	1.947E-07	1.154E-06	1.530E-04	1.478E-04		
1.000E+00	0.0			0.0				0.0				0.0	2.677E-07	5.161E-07	1.027E-04	2.073E-03	6.621E-04		
3.162E+00	0.0			0.0				0.0				0.0	7.504E-07	3.654E-06	1.456E-03	9.506E-03	2.537E-03		
1.000E+01	0.0			0.0				0.0				0.0	3.551E-07	1.225E-06	1.705E-04	8.431E-03	3.319E-02	1.056E-02	
1.000E+02	0.0			0.0				0.0				0.0	1.345E-06	1.805E-04	1.055E-02	1.063E-01	3.344E-01	3.265E-01	
1.000E+03	0.0			0.0				0.0				0.0	1.813E-04	1.081E-02	1.285E-01	8.655E-01	1.902E+00	2.030E+00	
1.000E+04	0.0			0.0				0.0				0.0	1.084E-02	1.312E-01	9.589E-01	3.047E+00	4.172E+00	4.267E+00	

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	0.0			0.0				3.308E-10	9.621E-08	0.0	1.785E-07	1.422E-07	7.145E-06	2.581E-05					
3.162E-01	0.0			0.0				0.0	7.670E-08	3.674E-08	3.786E-07	3.212E-06	6.090E-04	4.762E-04					
1.000E+00	0.0			0.0				0.0	7.986E-09	3.213E-07	7.597E-07	3.227E-04	6.538E-03	2.254E-03					
3.162E+00	0.0			0.0				0.0	9.212E-08	9.174E-07	9.526E-06	4.587E-03	2.954E-02	1.052E-02					
1.000E+01	0.0			0.0				0.0	4.433E-07	1.457E-06	5.343E-04	2.645E-02	1.041E-01	5.920E-02					
1.000E+02	0.0			0.0				0.0	1.440E-06	5.641E-04	3.305E-02	3.155E-01	5.130E-01	1.028E+00					
1.000E+03	0.0			0.0				0.0	5.667E-04	3.386E-02	3.767E-01	1.846E+00	3.021E+00	3.125E+00					
1.000E+04	0.0			0.0				0.0	3.395E-02	3.840E-01	2.047E+00	4.223E+00	5.317E+00	5.407E+00					

LOG S/S' = -1.5

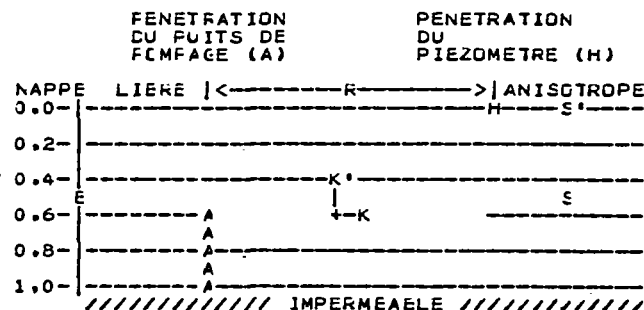
LOG K*R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	0.0			0.0				1.434E-08	1.396E-08	3.346E-08	3.709E-08	0.0	2.217E-05	9.302E-05	9.302E-05				
3.162E-01	0.0			0.0				0.0	0.0	6.378E-08	1.555E-07	8.826E-06	1.517E-03	1.569E-03	1.569E-03				
1.000E+00	0.0			0.0				0.0	0.0	2.629E-07	4.270E-07	1.013E-03	2.050E-02	9.197E-03	9.197E-03				
3.162E+00	0.0			0.0				0.0	0.0	1.211E-07	7.464E-07	2.643E-05	1.436E-02	5.561E-02	5.561E-02				
1.000E+01	0.0			0.0				0.0	0.0	5.455E-07	1.180E-06	1.676E-03	3.172E-02	3.135E-01	3.135E-01				
1.000E+02	0.0			1.376E-06				1.396E-06	1.768E-03	1.015E-01	8.386E-01	1.877E+00	2.004E+00						
1.000E+03	0.0			4.116E-06				1.188E-06	1.778E-03	1.039E-01	9.710E-01	3.019E+00	4.146E+00	4.240E+00					
1.000E+04	0.0			4.132E-06				1.477E-06	1.042E-01	9.864E-01	3.245E+00	5.276E+00	6.447E+00	6.537E+00					

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	C	U	I	T	S
1.000E-01	0.0			2.333E-08	1.470E-07	0.0		4.359E-08	0.0	0.0	0.0	0.0	6.613E-05	2.557E-04	2.557E-04				
3.162E-01	0.0			0.0	2.033E-07	0.0		2.439E-08	0.0	2.103E-05	5.578E-03	5.715E-03							
1.000E+00	0.0			0.0	2.654E-07	0.0		2.792E-08	0.0	3.145E-03	6.308E-02	4.535E-02							
3.162E+00	0.0			0.0	5.005E-07	9.612E-08	0.0	0.0	7.219E-05	4.405E-02	2.789E-01	2.643E-01							
1.000E+01	0.0			0.0	1.514E-07	2.315E-07	0.0	0.0	5.195E-03	2.354E-01	8.465E-01	9.621E-01							
1.000E+02	1.237E-06	0.0		0.0	0.0	0.0	0.0	5.478E-03	2.937E-01	1.762E+00	2.537E+00	3.045E+00							
1.000E+03	6.401E-06	0.0		0.0	0.0	0.0	0.0	5.507E-03	3.003E-01	1.963E+00	4.137E+00	5.236E+00	5.332E+00						
1.000E+04	6.429E-06	0.0		0.0	0.0	0.0	0.0	3.010E-01	1.983E+00	4.368E+00	6.459E+00	7.546E+00	7.640E+00						

PUITS PENETRANT DE 0.6 A 1.0 ET PIEZOMETRE FONCTIONNEL A LA PROFONDEUR 0.05
 ABAQUE POUR L'INTERPRETATION DE COMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABEAU A H



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	3.517E-05	3.511E-05	3.465E-05	3.100E-05	1.039E-05	0.0	7.579E-07	1.544E-03	5.575E-04
3.162E-01	4.460E-04	4.448E-04	4.319E-04	3.249E-04	3.159E-05	2.637E-07	2.718E-03	2.613E-02	1.173E-03
1.000E+00	1.474E-03	1.463E-03	1.365E-03	7.268E-04	3.336E-05	1.132E-05	4.754E-02	5.240E-02	1.360E-03
3.162E+00	2.873E-03	2.825E-03	2.407E-03	8.284E-04	3.502E-05	6.786E-03	1.335E-01	5.787E-02	1.965E-03
1.000E+01	4.410E-03	4.238E-03	3.038E-03	8.309E-04	4.972E-05	7.205E-02	1.767E-01	6.534E-02	4.131E-03
1.000E+02	7.439E-03	6.053E-03	3.161E-03	8.477E-04	7.525E-02	2.156E-01	2.094E-01	1.626E-01	6.538E-02
1.000E+03	9.317E-03	6.217E-03	3.178E-03	7.637E-02	2.204E-01	2.537E-01	4.754E-01	5.555E-01	1.039E+00
1.000E+04	9.444E-03	6.233E-03	7.827E-02	2.218E-01	2.591E-01	5.633E-01	1.919E+00	3.035E+00	3.134E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	3.523E-05	3.514E-05	3.466E-05	3.106E-05	1.056E-05	0.0	8.808E-07	1.545E-03	5.647E-04
3.162E-01	4.461E-04	4.448E-04	4.320E-04	3.251E-04	3.179E-05	2.109E-08	2.718E-03	2.625E-02	1.289E-03
1.000E+00	1.474E-03	1.463E-03	1.365E-03	7.274E-04	3.346E-05	1.117E-05	4.759E-02	5.376E-02	1.692E-03
3.162E+00	2.873E-03	2.825E-03	2.408E-03	8.296E-04	3.484E-05	6.787E-03	1.343E-01	6.426E-02	4.038E-03
1.000E+01	4.410E-03	4.238E-03	3.039E-03	8.324E-04	4.933E-05	7.213E-02	1.817E-01	6.782E-02	1.331E-02
1.000E+02	7.439E-03	6.054E-03	3.161E-03	8.488E-04	7.533E-02	2.219E-01	2.749E-01	3.644E-01	3.329E-01
1.000E+03	9.316E-03	6.220E-03	3.163E-03	7.646E-02	2.268E-01	3.313E-01	9.760E-01	1.916E+00	2.031E+00
1.000E+04	9.443E-03	6.227E-03	3.168E-03	2.282E-01	3.381E-01	1.125E+00	3.073E+00	4.176E+00	4.267E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	3.524E-05	3.511E-05	3.469E-05	3.126E-05	1.035E-05	1.560E-07	1.287E-06	1.545E-03	5.663E-04
3.162E-01	4.461E-04	4.448E-04	4.320E-04	3.256E-04	3.168E-05	6.368E-07	2.719E-03	2.663E-02	1.663E-03
1.000E+00	1.474E-03	1.463E-03	1.365E-03	7.284E-04	3.369E-05	1.186E-05	4.814E-02	5.804E-02	3.754E-03
3.162E+00	2.873E-03	2.826E-03	2.408E-03	8.312E-04	3.537E-05	6.791E-03	1.369E-01	6.437E-02	1.282E-02
1.000E+01	4.410E-03	4.238E-03	3.040E-03	8.344E-04	4.957E-05	7.239E-02	1.976E-01	1.575E-01	6.376E-02
1.000E+02	7.439E-03	6.055E-03	3.165E-03	8.510E-04	7.560E-02	2.413E-01	4.667E-01	5.484E-01	1.032E+00
1.000E+03	9.320E-03	6.221E-03	3.182E-03	7.673E-02	2.467E-01	5.544E-01	1.904E+00	3.024E+00	3.125E+00
1.000E+04	9.449E-03	6.240E-03	7.923E-02	2.481E-01	5.649E-01	2.111E+00	4.238E+00	5.316E+00	5.407E+00

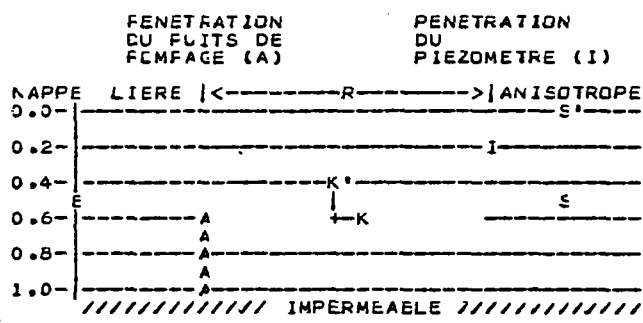
LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	3.516E-05	3.511E-05	3.472E-05	3.120E-05	1.049E-05	0.0	8.986E-07	1.561E-03	6.532E-04
3.162E-01	4.460E-04	4.448E-04	4.322E-04	3.257E-04	3.197E-05	3.539E-07	2.722E-03	2.781E-02	2.919E-03
1.000E+00	1.474E-03	1.464E-03	1.366E-03	7.293E-04	3.410E-05	1.148E-05	4.864E-02	7.142E-02	1.136E-02
3.162E+00	2.873E-03	2.826E-03	2.409E-03	8.319E-04	3.573E-05	6.799E-03	1.451E-01	1.465E-01	5.959E-02
1.000E+01	4.410E-03	4.238E-03	3.042E-03	8.352E-04	5.028E-05	7.319E-02	2.465E-01	3.666E-01	3.198E-01
1.000E+02	7.440E-03	6.057E-03	3.167E-03	8.520E-04	7.644E-02	3.007E-01	9.495E-01	1.892E+00	2.006E+00
1.000E+03	9.322E-03	6.223E-03	3.185E-03	7.758E-02	3.073E-01	1.057E+00	3.045E+00	4.145E+00	4.240E+00
1.000E+04	9.451E-03	6.239E-03	6.008E-02	3.088E-01	1.114E+00	3.275E+00	5.387E+00	6.455E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	3.524E-05	3.515E-05	3.493E-05	3.134E-05	1.072E-05	0.0	0.0	1.595E-03	6.271E-04
3.162E-01	4.461E-04	4.449E-04	4.327E-04	3.260E-04	3.210E-05	0.0	2.724E-03	3.148E-02	7.457E-03
1.000E+00	1.474E-03	1.464E-03	1.366E-03	7.293E-04	3.397E-05	8.574E-06	5.018E-02	1.121E-01	4.925E-02
3.162E+00	2.873E-03	2.826E-03	2.411E-03	8.324E-04	3.497E-05	6.810E-03	1.698E-01	3.272E-01	2.903E-01
1.000E+01	4.410E-03	4.239E-03	3.043E-03	8.356E-04	4.747E-05	7.565E-02	3.866E-01	6.811E-01	9.658E-01
1.000E+02	7.441E-03	6.057E-03	3.168E-03	8.499E-04	7.903E-02	4.683E-01	1.819E+00	2.943E+00	3.045E+00
1.000E+03	9.320E-03	6.223E-03	3.184E-03	8.018E-02	4.761E-01	2.324E+00	4.151E+00	5.233E+00	5.332E+00
1.000E+04	9.448E-03	6.241E-03	6.270E-02	4.800E-01	2.048E+00	4.358E+00	6.470E+00	7.547E+00	7.640E+00

PUITS PENETRANT DE 0.6 A 1.0 ET PIEZOMETRE FONCTUEL A LA PROFONDEUR 0.2
ABAUQUE POUR L'INTERPRETATION DE FCMAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.609E-04	1.606E-04	1.582E-04	1.414E-04	4.707E-05	1.302E-07	6.204E-05	6.152E-03	2.166E-C3
3.162E-01	2.038E-03	2.032E-03	1.573E-03	1.483E-03	1.411E-04	3.558E-07	2.019E-02	1.036E-01	4.461E-C3
1.000E+00	6.731E-03	6.684E-03	6.233E-03	3.316E-03	1.439E-04	8.328E-04	2.192E-01	2.066E-01	4.753E-C3
3.162E+00	1.312E-02	1.250E-02	1.099E-02	3.774E-03	1.445E-04	5.476E-02	5.562E-01	2.201E-01	6.555E-C3
1.000E+01	2.014E-02	1.935E-02	1.367E-02	3.779E-03	1.233E-03	3.449E-01	7.218E-01	2.274E-01	6.509E-C3
1.000E+02	3.358E-02	2.782E-02	1.442E-02	4.898E-03	3.626E-01	9.051E-01	7.551E-01	1.211E-01	7.809E-C2
1.000E+03	4.255E-02	2.838E-02	1.554E-02	3.680E-01	9.290E-01	9.457E-01	9.656E-01	1.062E+00	1.049E+00
1.000E+04	4.213E-02	2.951E-02	3.754E-01	9.352E-01	9.659E-01	1.181E+00	2.185E+00	3.064E+00	3.126E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.609E-04	1.606E-04	1.582E-04	1.412E-04	4.756E-05	8.238E-08	6.179E-05	6.152E-03	2.166E-C3
3.162E-01	2.038E-03	2.032E-03	1.573E-03	1.483E-03	1.418E-04	2.787E-07	2.019E-02	1.036E-01	4.461E-C3
1.000E+00	6.731E-03	6.684E-03	6.233E-03	3.318E-03	1.446E-04	8.327E-04	2.193E-01	2.067E-01	5.466E-C3
3.162E+00	1.312E-02	1.250E-02	1.099E-02	3.775E-03	1.449E-04	5.476E-02	5.567E-01	2.262E-01	6.360E-C3
1.000E+01	2.014E-02	1.935E-02	1.367E-02	3.780E-03	1.233E-03	3.450E-01	7.255E-01	2.490E-01	1.509E-C2
1.000E+02	3.358E-02	2.782E-02	1.442E-02	4.899E-03	3.626E-01	9.093E-01	8.103E-01	1.303E-01	1.502E-C1
1.000E+03	4.255E-02	2.838E-02	1.554E-02	3.681E-01	9.332E-01	1.003E+00	1.377E+00	1.972E+00	2.035E+00
1.000E+04	4.213E-02	2.951E-02	3.755E-01	9.395E-01	1.028E+00	1.625E+00	3.262E+00	4.195E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.609E-04	1.606E-04	1.582E-04	1.416E-04	4.648E-05	7.285E-08	6.211E-05	6.154E-03	2.220E-C3
3.162E-01	2.038E-03	2.032E-03	1.573E-03	1.484E-03	1.405E-04	1.631E-07	2.019E-02	1.042E-01	5.138E-C3
1.000E+00	6.731E-03	6.684E-03	6.233E-03	3.318E-03	1.431E-04	8.323E-04	2.193E-01	2.067E-01	7.576E-C3
3.162E+00	1.312E-02	1.250E-02	1.099E-02	3.777E-03	1.435E-04	5.476E-02	5.602E-01	2.450E-01	1.535E-C2
1.000E+01	2.014E-02	1.935E-02	1.367E-02	3.782E-03	1.232E-03	3.450E-01	7.366E-01	3.157E-01	7.626E-C2
1.000E+02	3.358E-02	2.782E-02	1.442E-02	4.900E-03	3.627E-01	9.223E-01	9.612E-01	1.054E+00	1.042E+00
1.000E+03	4.255E-02	2.838E-02	1.554E-02	3.682E-01	9.464E-01	1.172E+00	2.176E+00	3.055E+00	3.127E+00
1.000E+04	4.213E-02	2.951E-02	3.756E-01	9.528E-01	1.199E+00	2.465E+00	4.398E+00	5.235E+00	5.407E+00

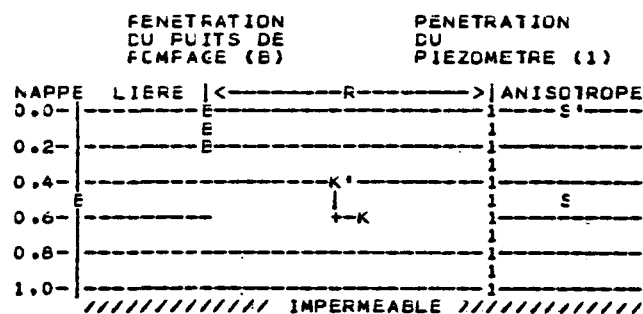
LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.609E-04	1.606E-04	1.582E-04	1.417E-04	4.712E-05	2.799E-07	6.222E-05	6.155E-03	2.266E-C3
3.162E-01	2.038E-03	2.032E-03	1.573E-03	1.484E-03	1.411E-04	3.733E-07	2.019E-02	1.050E-01	6.780E-C3
1.000E+00	6.731E-03	6.684E-03	6.233E-03	3.317E-03	1.439E-04	8.325E-04	2.193E-01	2.220E-01	1.748E-C2
3.162E+00	1.312E-02	1.250E-02	1.100E-02	3.777E-03	1.442E-04	5.476E-02	5.649E-01	3.030E-01	7.266E-C2
1.000E+01	2.014E-02	1.936E-02	1.367E-02	3.782E-03	1.233E-03	3.453E-01	7.710E-01	5.114E-01	3.377E-C1
1.000E+02	3.358E-02	2.783E-02	1.442E-02	4.901E-03	3.630E-01	9.623E-01	1.356E+00	1.546E+00	2.010E+00
1.000E+03	4.255E-02	2.838E-02	1.554E-02	3.684E-01	9.878E-01	1.593E+00	3.234E+00	4.166E+00	4.241E+00
1.000E+04	4.213E-02	2.951E-02	3.758E-01	9.934E-01	1.632E+00	3.542E+00	5.538E+00	6.475E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.609E-04	1.606E-04	1.584E-04	1.411E-04	4.731E-05	0.0	6.003E-05	6.172E-03	2.499E-C3
3.162E-01	2.038E-03	2.032E-03	1.574E-03	1.483E-03	1.412E-04	0.0	2.019E-02	1.076E-01	1.243E-C2
1.000E+00	6.731E-03	6.684E-03	6.235E-03	3.317E-03	1.437E-04	8.299E-04	2.200E-01	2.566E-01	6.001E-C2
3.162E+00	1.312E-02	1.250E-02	1.100E-02	3.776E-03	1.434E-04	5.475E-02	5.752E-01	4.687E-01	3.664E-01
1.000E+01	2.014E-02	1.936E-02	1.368E-02	3.781E-03	1.230E-03	3.461E-01	8.765E-01	5.855E-01	9.758E-C1
1.000E+02	3.358E-02	2.783E-02	1.442E-02	4.897E-03	3.638E-01	1.077E+00	2.092E+00	2.671E+00	3.047E+00
1.000E+03	4.255E-02	2.839E-02	1.554E-02	3.693E-01	1.103E+00	2.378E+00	4.312E+00	5.254E+00	5.332E+00
1.000E+04	4.213E-02	2.951E-02	3.807E-01	1.110E+00	2.414E+00	4.625E+00	6.616E+00	7.562E+00	7.641E+00

ABAUQUE POUR L'INTERPRETATION DE FCMFAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.419E-02	2.362E-02	2.103E-02	1.326E-02	4.525E-03	7.134E-04
3.162E-01	3.680E-01	3.079E-01	3.077E-01	3.055E-01	2.908E-01	2.369E-01	1.200E-01	4.033E-02	1.444E-02
1.000E+00	1.018E+00	1.018E+00	1.016E+00	1.000E+00	9.180E-01	6.590E-01	2.865E-01	7.542E-02	1.370E-02
3.162E+00	1.586E+00	1.585E+00	1.577E+00	1.917E+00	1.670E+00	1.044E+00	4.180E-01	8.109E-02	1.142E-02
1.000E+01	3.057E+00	3.054E+00	3.026E+00	2.866E+00	2.316E+00	1.303E+00	4.787E-01	8.582E-02	6.556E-03
1.000E+02	5.276E+00	5.245E+00	5.063E+00	4.402E+00	3.033E+00	1.548E+00	5.534E-01	1.554E-01	3.179E-02
1.000E+03	7.486E+00	7.301E+00	6.614E+00	5.131E+00	3.327E+00	1.913E+00	1.262E+00	1.056E+00	1.084E+00
1.000E+04	9.546E+00	8.655E+00	7.350E+00	5.475E+00	4.117E+00	4.655E+00	4.803E+00	3.725E+00	3.319E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.420E-02	2.364E-02	2.106E-02	1.333E-02	4.685E-03	6.457E-04
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.055E-01	2.909E-01	2.371E-01	1.202E-01	4.031E-02	1.308E-02
1.000E+00	1.018E+00	1.018E+00	1.016E+00	1.000E+00	9.181E-01	6.596E-01	2.875E-01	7.611E-02	1.082E-02
3.162E+00	1.586E+00	1.585E+00	1.577E+00	1.917E+00	1.671E+00	1.047E+00	4.223E-01	8.455E-02	5.822E-03
1.000E+01	3.057E+00	3.054E+00	3.026E+00	2.866E+00	2.318E+00	1.311E+00	4.937E-01	1.004E-01	1.506E-02
1.000E+02	5.276E+00	5.245E+00	5.064E+00	4.405E+00	3.052E+00	1.633E+00	7.212E-01	3.635E-01	2.657E-02
1.000E+03	7.487E+00	7.302E+00	6.618E+00	5.163E+00	3.522E+00	2.703E+00	2.657E+00	2.356E+00	2.162E+00
1.000E+04	9.547E+00	8.661E+00	7.353E+00	5.779E+00	5.638E+00	7.658E+00	6.544E+00	4.974E+00	4.463E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.421E-02	2.369E-02	2.123E-02	1.353E-02	4.752E-03	4.336E-04
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.056E-01	2.910E-01	2.377E-01	1.209E-01	4.023E-02	8.523E-04
1.000E+00	1.018E+00	1.018E+00	1.016E+00	1.000E+00	9.186E-01	6.617E-01	2.905E-01	7.627E-02	3.578E-04
3.162E+00	1.586E+00	1.585E+00	1.577E+00	1.917E+00	1.673E+00	1.054E+00	4.346E-01	8.755E-02	1.127E-03
1.000E+01	3.057E+00	3.054E+00	3.026E+00	2.867E+00	2.323E+00	1.335E+00	5.413E-01	1.511E-01	3.033E-02
1.000E+02	5.276E+00	5.245E+00	5.065E+00	4.414E+00	3.113E+00	1.895E+00	1.254E+00	1.085E+00	1.076E+00
1.000E+03	7.487E+00	7.303E+00	6.631E+00	5.261E+00	4.103E+00	4.642E+00	4.791E+00	3.713E+00	3.309E+00
1.000E+04	9.549E+00	8.678E+00	7.526E+00	6.614E+00	6.489E+00	1.027E+01	7.940E+00	6.172E+00	5.639E+00

LOG S/S' = -1.5

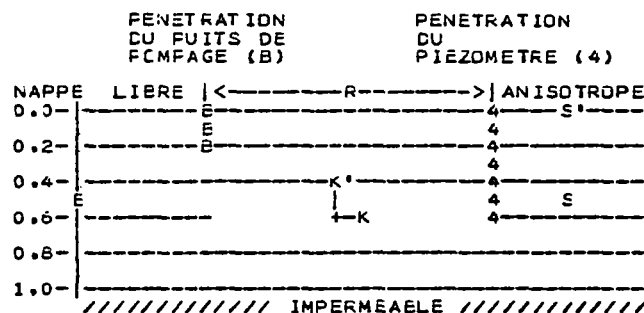
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.428E-02	2.427E-02	2.427E-02	2.423E-02	2.384E-02	2.183E-02	1.416E-02	4.326E-03	0.0
3.162E-01	3.080E-01	3.079E-01	3.077E-01	3.056E-01	2.915E-01	2.396E-01	1.232E-01	3.996E-02	0.0
1.000E+00	1.018E+00	1.018E+00	1.016E+00	1.000E+00	9.202E-01	6.681E-01	3.002E-01	6.534E-02	0.0
3.162E+00	1.586E+00	1.585E+00	1.577E+00	1.918E+00	1.678E+00	1.076E+00	4.748E-01	1.410E-01	2.666E-02
1.000E+01	3.057E+00	3.054E+00	3.026E+00	2.870E+00	2.340E+00	1.412E+00	6.932E-01	3.454E-01	2.814E-02
1.000E+02	5.276E+00	5.245E+00	5.069E+00	4.443E+00	3.299E+00	2.669E+00	2.665E+00	2.361E+00	2.132E+00
1.000E+03	7.487E+00	7.309E+00	6.673E+00	5.556E+00	5.005E+00	7.619E+00	6.507E+00	4.536E+00	4.452E+00
1.000E+04	9.555E+00	8.930E+00	7.901E+00	8.450E+00	1.189E+01	1.205E+01	9.183E+00	7.327E+00	6.776E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	2.428E-02	2.428E-02	2.429E-02	2.431E-02	2.431E-02	2.370E-02	1.610E-02	2.631E-03	0.0
3.162E-01	3.080E-01	3.079E-01	3.078E-01	3.059E-01	2.930E-01	2.456E-01	1.302E-01	3.686E-02	0.0
1.000E+00	1.018E+00	1.018E+00	1.016E+00	1.001E+00	9.251E-01	6.885E-01	3.303E-01	1.093E-01	1.752E-02
3.162E+00	1.586E+00	1.585E+00	1.578E+00	1.921E+00	1.694E+00	1.147E+00	6.015E-01	3.038E-01	2.494E-02
1.000E+01	3.057E+00	3.054E+00	3.027E+00	2.879E+00	2.395E+00	1.650E+00	1.170E+00	1.003E+00	9.556E-02
1.000E+02	5.276E+00	5.247E+00	5.081E+00	4.535E+00	3.853E+00	4.550E+00	4.681E+00	3.595E+00	3.217E+00
1.000E+03	7.489E+00	7.325E+00	6.799E+00	6.361E+00	5.398E+00	1.017E+01	7.824E+00	6.061E+00	5.552E+00
1.000E+04	9.574E+00	9.082E+00	8.616E+00	1.144E+01	1.452E+01	1.339E+01	1.031E+01	8.421E+00	7.876E+00

PUITS A PENETRATION DE 0.0 A C.2 ET PIEZOMETRE CUVERT DE 0.0 A 0.6
 ABAQUE POUR L'INTERPRETATION DE FCMPS EN NAPPE LIBRE ANISTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU B 4



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.046E-02	4.046E-02	4.045E-02	4.032E-02	3.929E-02	3.498E-02	2.203E-02	5.570E-03	4.961E-04
3.162E-01	5.133E-01	5.132E-01	5.128E-01	5.092E-01	4.846E-01	3.948E-01	1.948E-01	3.254E-02	1.017E-03
1.000E+00	1.656E+00	1.656E+00	1.653E+00	1.667E+00	1.530E+00	1.093E+00	4.089E-01	5.672E-02	1.026E-03
3.162E+00	3.310E+00	3.309E+00	3.295E+00	3.195E+00	2.784E+00	1.727E+00	5.138E-01	6.080E-02	1.070E-03
1.000E+01	5.095E+00	5.090E+00	5.042E+00	4.777E+00	3.859E+00	2.064E+00	5.569E-01	6.463E-02	1.406E-03
1.000E+02	8.793E+00	8.741E+00	8.439E+00	7.335E+00	4.940E+00	2.260E+00	6.255E-01	1.225E-01	3.673E-02
1.000E+03	1.248E+01	1.217E+01	1.102E+01	8.433E+00	5.185E+00	2.616E+00	1.294E+00	5.722E-01	1.050E+00
1.000E+04	1.591E+01	1.476E+01	1.213E+01	8.729E+00	5.967E+00	5.313E+00	4.632E+00	3.434E+00	3.224E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.046E-02	4.046E-02	4.045E-02	4.032E-02	3.938E-02	3.502E-02	2.203E-02	5.533E-03	4.664E-04
3.162E-01	5.133E-01	5.132E-01	5.128E-01	5.092E-01	4.847E-01	3.950E-01	1.949E-01	3.253E-02	9.821E-04
1.000E+00	1.656E+00	1.656E+00	1.653E+00	1.667E+00	1.530E+00	1.093E+00	4.097E-01	5.729E-02	1.023E-03
3.162E+00	3.310E+00	3.309E+00	3.295E+00	3.195E+00	2.784E+00	1.729E+00	5.175E-01	6.395E-02	1.346E-03
1.000E+01	5.095E+00	5.090E+00	5.042E+00	4.777E+00	3.861E+00	2.072E+00	5.709E-01	7.657E-02	4.556E-03
1.000E+02	8.793E+00	8.741E+00	8.439E+00	7.338E+00	4.958E+00	2.344E+00	7.831E-01	3.045E-01	2.954E-01
1.000E+03	1.248E+01	1.217E+01	1.103E+01	8.464E+00	5.378E+00	3.396E+00	2.654E+00	2.178E+00	2.051E+00
1.000E+04	1.591E+01	1.476E+01	1.217E+01	9.031E+00	7.476E+00	8.231E+00	6.250E+00	4.638E+00	4.373E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.046E-02	4.046E-02	4.045E-02	4.033E-02	3.941E-02	3.516E-02	2.212E-02	5.415E-03	3.739E-04
3.162E-01	5.133E-01	5.132E-01	5.129E-01	5.092E-01	4.848E-01	3.954E-01	1.953E-01	3.248E-02	5.792E-04
1.000E+00	1.656E+00	1.656E+00	1.653E+00	1.667E+00	1.530E+00	1.103E+00	4.123E-01	5.913E-02	1.166E-03
3.162E+00	3.310E+00	3.309E+00	3.295E+00	3.195E+00	2.786E+00	1.735E+00	5.293E-01	7.434E-02	4.225E-03
1.000E+01	5.095E+00	5.090E+00	5.043E+00	4.778E+00	3.866E+00	2.095E+00	6.157E-01	1.191E-01	3.740E-02
1.000E+02	8.793E+00	8.742E+00	8.440E+00	7.347E+00	5.017E+00	2.603E+00	1.286E+00	5.644E-01	1.042E+00
1.000E+03	1.248E+01	1.217E+01	1.104E+01	8.560E+00	5.955E+00	5.302E+00	4.621E+00	3.422E+00	3.214E+00
1.000E+04	1.591E+01	1.478E+01	1.230E+01	9.859E+00	1.029E+01	1.071E+01	7.566E+00	5.811E+00	5.521E+00

LOG S/S' = -1.5

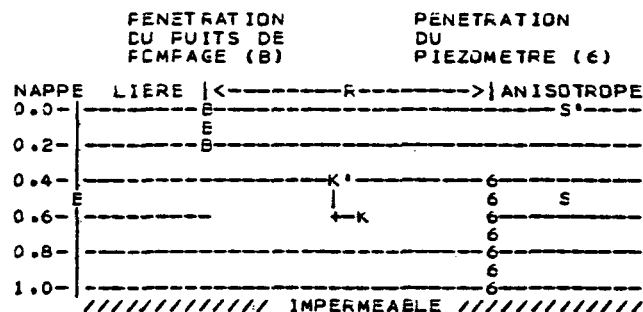
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.046E-02	4.046E-02	4.045E-02	4.033E-02	3.953E-02	3.558E-02	2.241E-02	5.034E-03	8.894E-05
3.162E-01	5.133E-01	5.132E-01	5.129E-01	5.093E-01	4.852E-01	3.969E-01	1.967E-01	3.233E-02	6.454E-04
1.000E+00	1.656E+00	1.656E+00	1.653E+00	1.667E+00	1.532E+00	1.105E+00	4.203E-01	6.517E-02	3.243E-03
3.162E+00	3.310E+00	3.309E+00	3.295E+00	3.196E+00	2.790E+00	1.755E+00	5.667E-01	1.110E-01	3.432E-02
1.000E+01	5.095E+00	5.090E+00	5.043E+00	4.780E+00	3.881E+00	2.169E+00	7.568E-01	2.891E-01	2.622E-01
1.000E+02	8.793E+00	8.742E+00	8.445E+00	7.375E+00	5.201E+00	3.365E+00	2.624E+00	2.148E+00	2.064E+00
1.000E+03	1.248E+01	1.218E+01	1.106E+01	8.851E+00	7.445E+00	8.195E+00	6.216E+00	4.605E+00	4.344E+00
1.000E+04	1.592E+01	1.483E+01	1.267E+01	1.168E+01	1.361E+01	1.238E+01	8.767E+00	6.954E+00	6.655E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.046E-02	4.046E-02	4.046E-02	4.042E-02	3.991E-02	3.597E-02	2.325E-02	3.762E-03	0.0
3.162E-01	5.133E-01	5.132E-01	5.129E-01	5.095E-01	4.864E-01	4.014E-01	2.008E-01	3.181E-02	7.030E-04
1.000E+00	1.656E+00	1.656E+00	1.653E+00	1.668E+00	1.536E+00	1.122E+00	4.456E-01	6.631E-02	2.563E-03
3.162E+00	3.310E+00	3.309E+00	3.296E+00	3.198E+00	2.804E+00	1.819E+00	6.853E-01	2.548E-01	2.525E-01
1.000E+01	5.095E+00	5.090E+00	5.044E+00	4.788E+00	3.931E+00	2.398E+00	1.210E+00	8.906E-01	5.711E-01
1.000E+02	8.793E+00	8.743E+00	8.455E+00	7.461E+00	5.743E+00	5.212E+00	4.519E+00	3.324E+00	3.128E+00
1.000E+03	1.248E+01	1.219E+01	1.120E+01	9.646E+00	1.020E+01	1.061E+01	7.462E+00	5.715E+00	5.441E+00
1.000E+04	1.594E+01	1.495E+01	1.357E+01	1.463E+01	1.611E+01	1.363E+01	9.878E+00	8.050E+00	7.757E+00

PUITS A PENETRATION DE 0.0 A 0.2 ET PIEZOMETRE OUVERT DE 0.4 A 1.0
 ABAQUE POUR L'INTERPRETATION DE FCMFAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCOVA

TABLEAU B 6



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.015E-06	9.599E-07	9.778E-07	1.027E-06	9.970E-07	2.356E-06	6.489E-04	4.672E-03	9.969E-04
3.162E-01	1.266E-05	1.259E-05	1.260E-05	1.215E-05	3.553E-06	1.047E-04	3.395E-02	5.084E-02	2.042E-03
1.000E+00	4.181E-05	4.174E-05	4.161E-05	3.379E-05	5.566E-06	1.122E-02	1.743E-01	9.626E-02	2.127E-03
3.162E+00	8.152E-05	8.147E-05	7.982E-05	4.373E-05	2.378E-04	1.110E-01	3.401E-01	1.063E-01	2.403E-03
1.000E+01	1.255E-04	1.252E-04	1.130E-04	4.602E-05	1.546E-02	3.211E-01	4.182E-01	1.139E-01	3.540E-03
1.000E+02	2.165E-04	2.035E-04	1.269E-04	1.601E-02	3.466E-01	5.947E-01	4.684E-01	2.145E-01	5.484E-02
1.000E+03	2.955E-04	2.175E-04	1.615E-02	3.494E-01	6.235E-01	6.609E-01	8.620E-01	1.107E+00	1.069E+00
1.000E+04	3.065E-04	1.628E-02	3.501E-01	6.267E-01	6.919E-01	1.176E+00	2.791E+00	3.397E+00	3.229E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.014E-06	9.692E-07	9.741E-07	1.100E-06	1.304E-06	7.353E-06	6.757E-04	4.587E-03	9.672E-04
3.162E-01	1.266E-05	1.261E-05	1.262E-05	1.237E-05	4.975E-06	1.205E-04	3.405E-02	5.100E-02	2.049E-03
1.000E+00	4.180E-05	4.177E-05	4.168E-05	3.437E-05	1.059E-05	1.127E-02	1.747E-01	9.567E-02	2.325E-03
3.162E+00	8.150E-05	8.153E-05	8.005E-05	4.532E-05	2.543E-04	1.111E-01	3.421E-01	1.128E-01	3.443E-03
1.000E+01	1.255E-04	1.253E-04	1.137E-04	5.113E-05	1.551E-02	3.218E-01	4.268E-01	1.365E-01	9.640E-03
1.000E+02	2.164E-04	2.042E-04	1.324E-04	1.607E-02	3.473E-01	6.070E-01	5.675E-01	4.557E-01	3.259E-01
1.000E+03	2.957E-04	2.225E-04	1.620E-02	3.501E-01	6.363E-01	7.947E-01	1.574E+00	2.194E+00	2.100E+00
1.000E+04	3.079E-04	1.633E-02	3.508E-01	6.396E-01	8.305E-01	2.032E+00	4.138E+00	4.587E+00	4.377E+00

LOG S/S' = -2.0

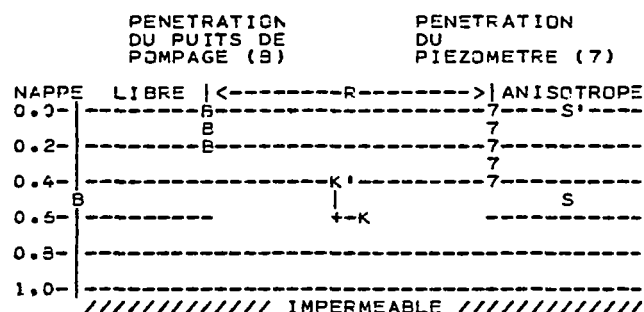
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.014E-06	9.838E-07	1.009E-06	1.231E-06	3.107E-06	2.321E-05	7.765E-04	5.031E-03	9.743E-04
3.162E-01	1.266E-05	1.263E-05	1.271E-05	1.283E-05	1.052E-05	1.707E-04	3.436E-02	5.149E-02	2.077E-03
1.000E+00	4.180E-05	4.180E-05	4.193E-05	3.565E-05	2.764E-05	1.143E-02	1.760E-01	1.041E-01	3.146E-03
3.162E+00	8.152E-05	8.161E-05	8.069E-05	5.034E-05	3.076E-04	1.116E-01	3.483E-01	1.335E-01	9.146E-03
1.000E+01	1.255E-04	1.255E-04	1.154E-04	6.777E-05	1.568E-02	3.239E-01	4.538E-01	1.209E-01	5.318E-02
1.000E+02	2.165E-04	2.055E-04	1.496E-04	1.624E-02	3.495E-01	6.454E-01	8.536E-01	1.095E+00	1.062E+00
1.000E+03	2.955E-04	2.356E-04	1.638E-02	3.523E-01	6.763E-01	1.167E+00	2.781E+00	3.387E+00	3.219E+00
1.000E+04	3.077E-04	1.648E-02	3.531E-01	6.798E-01	1.214E+00	3.348E+00	5.397E+00	5.755E+00	5.524E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.021E-06	9.713E-07	1.035E-06	1.623E-06	8.367E-06	7.317E-05	1.081E-03	5.160E-03	9.856E-04
3.162E-01	1.267E-05	1.264E-05	1.287E-05	1.426E-05	2.718E-05	3.268E-04	3.534E-02	5.300E-02	2.270E-03
1.000E+00	4.182E-05	4.185E-05	4.246E-05	4.088E-05	8.041E-05	1.193E-02	1.799E-01	1.181E-01	7.666E-03
3.162E+00	8.155E-05	8.191E-05	8.225E-05	6.698E-05	4.747E-04	1.133E-01	3.677E-01	1.583E-01	4.933E-02
1.000E+01	1.255E-04	1.261E-04	1.205E-04	1.208E-04	1.621E-02	3.305E-01	5.363E-01	4.368E-01	3.119E-01
1.000E+02	2.167E-04	2.101E-04	2.035E-04	1.677E-02	3.566E-01	7.612E-01	1.547E+00	2.164E+00	2.072E+00
1.000E+03	2.959E-04	2.931E-04	1.692E-02	3.594E-01	7.966E-01	2.004E+00	4.108E+00	4.555E+00	4.348E+00
1.000E+04	3.103E-04	1.694E-02	3.603E-01	8.006E-01	2.068E+00	4.707E+00	6.584E+00	6.896E+00	6.658E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	1.027E-06	9.942E-07	1.197E-06	3.456E-06	2.502E-05	2.311E-04	2.033E-03	5.474E-03	0.0
3.162E-01	1.268E-05	1.270E-05	1.337E-05	1.981E-05	7.995E-05	6.275E-04	3.840E-02	5.754E-02	3.753E-03
1.000E+00	4.184E-05	4.206E-05	4.399E-05	5.800E-05	2.473E-04	1.350E-02	1.921E-01	1.609E-01	3.842E-02
3.162E+00	8.159E-05	8.237E-05	8.740E-05	1.204E-04	1.002E-03	1.184E-01	4.265E-01	3.944E-01	2.605E-01
1.000E+01	1.256E-04	1.276E-04	1.374E-04	2.891E-04	1.788E-02	3.510E-01	7.702E-01	1.023E+00	9.900E-01
1.000E+02	2.167E-04	2.250E-04	3.755E-04	1.844E-02	3.783E-01	1.078E+00	2.693E+00	3.292E+00	3.133E+00
1.000E+03	2.962E-04	4.339E-04	1.664E-02	3.913E-01	1.125E+00	3.260E+00	5.306E+00	5.663E+00	5.443E+00
1.000E+04	3.173E-04	1.845E-02	3.826E-01	1.130E+00	3.336E+00	5.914E+00	7.702E+00	7.596E+00	7.760E+00

$$\text{LOG } S/S' = -3.0$$


LDG K'F2/KB2 -7.0

TT/R2S	R A S A T T E M E N T S					F E D U I T S				
1.000E-01	6.070E-02	6.068E-02	6.067E-02	6.049E-02	5.892E-02	5.245E-02	3.203E-02	4.008E-03	3.475E-04	
3.162E-01	7.699E-01	7.698E-01	7.693E-01	7.638E-01	7.269E-01	5.920E-01	2.487E-01	2.473E-02	7.194E-04	
1.000E+00	2.545E+00	2.544E+00	2.540E+00	2.500E+00	2.295E+00	1.630E+00	4.541E-01	4.161E-02	7.579E-04	
3.162E+00	4.966E+00	4.963E+00	4.943E+00	4.792E+00	4.175E+00	2.443E+00	5.332E-01	4.469E-02	8.920E-04	
1.000E+01	7.642E+00	7.634E+00	7.563E+00	7.165E+00	5.765E+00	2.770E+00	5.645E-01	4.814E-02	1.504E-03	
1.000E+02	1.319E+01	1.311E+01	1.266E+01	1.098E+01	7.050E+00	2.924E+00	6.303E-01	1.012E-01	4.042E-02	
1.000E+03	1.872E+01	1.825E+01	1.651E+01	1.228E+01	7.252E+00	3.277E+00	1.288E+00	9.152E-01	1.031E+00	
1.000E+04	2.387E+01	2.211E+01	1.782E+01	1.254E+01	6.033E+00	5.961E+00	4.562E+00	3.308E+00	3.177E+00	

$$\text{LOG } S/S' = -2.5$$

LOG K ¹ /R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	6.070E-02	6.068E-02	6.067E-02	6.049E-02	5.905E-02	5.248E-02	3.204E-02	4.885E-03	3.346E-04	
3.162E-01	7.699E-01	7.698E-01	7.693E-01	7.638E-01	7.270E-01	5.921E-01	2.488E-01	2.475E-02	7.232E-04	
1.000E+00	2.545E+00	2.544E+00	2.540E+00	2.500E+00	2.295E+00	1.631E+00	4.549E-01	4.219E-02	8.559E-04	
3.162E+00	4.966E+00	4.963E+00	4.943E+00	4.792E+00	4.176E+00	2.445E+00	5.369E-01	4.760E-02	1.256E-03	
1.000E+01	7.642E+00	7.634E+00	7.563E+00	7.166E+00	5.766E+00	2.778E+00	5.784E-01	5.903E-02	5.388E-03	
1.000E+02	1.319E+01	1.311E+01	1.265E+01	1.098E+01	7.069E+00	3.008E+00	7.857E-01	2.727E-01	2.926E-01	
1.000E+03	1.872E+01	1.825E+01	1.651E+01	1.231E+01	7.446E+00	4.054E+00	2.626E+00	2.085E+00	2.056E+00	
1.000E+04	2.387E+01	2.211E+01	1.786E+01	1.284E+01	9.538E+00	6.855E+00	6.134E+00	4.492E+00	4.319E+00	

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	6.070E-02	6.068E-02	6.067E-02	6.050E-02	5.907E-02	5.257E-02	3.207E-02	4.914E-03	2.936E-04	
3.162E-01	7.699E-01	7.698E-01	7.693E-01	7.638E-01	7.271E-01	5.924E-01	2.491E-01	2.482E-02	7.431E-04	
1.000E+00	2.544E+00	2.544E+00	2.540E+00	2.500E+00	2.295E+00	1.632E+00	4.574E-01	4.405E-02	1.309E-03	
3.162E+00	4.966E+00	4.963E+00	4.943E+00	4.792E+00	4.177E+00	2.450E+00	5.486E-01	5.723E-02	5.094E-03	
1.000E+01	7.642E+00	7.634E+00	7.554E+00	7.166E+00	5.771E+00	2.801E+00	6.227E-01	9.832E-02	3.917E-02	
1.000E+02	1.319E+01	1.311E+01	1.266E+01	1.099E+01	7.127E+00	3.266E+00	1.281E+00	9.081E-01	1.024E+00	
1.000E+03	1.872E+01	1.825E+01	1.652E+01	1.241E+01	6.021E+00	5.951E+00	4.552E+00	3.299E+00	3.168E+00	
1.000E+04	2.397E+01	2.213E+01	1.709E+01	1.367E+01	1.234E+01	1.129E+01	7.419E+00	5.653E+00	5.463E+00	

LOG S/S' = -1.5

LOG K ₁ R2/KB2	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0			1.0		
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	D	U	I	T	S								
1.000E-01	6.070E-02			6.068E-02				6.067E-02				6.051E-02				5.916E-02			5.297E-02			3.217E-02			4.584E-03		1.687E-04
3.162E-01	7.699E-01			7.698E-01				7.693E-01				7.639E-01				7.274E-01			5.935E-01			2.501E-01			2.505E-02		8.810E-04
1.000E+00	2.545E+00			2.544E+00				2.540E+00				2.500E+00				2.296E+00			1.636E+00			4.652E-01			5.161E-02		4.221E-03
3.162E+00	4.956E+00			4.963E+00				4.943E+00				4.793E+00				4.161E+00			2.469E+00			5.860E-01			9.165E-02		3.628E-02
1.000E+01	7.642E+00			7.634E+00				7.564E+00				7.169E+00				5.785E+00			2.873E+00			7.645E-01			2.592E-01		2.800E-01
1.000E+02	1.319E+01			1.311E+01				1.266E+01				1.102E+01				7.308E+00			4.025E+00			2.595E+00			2.057E+00		2.029E+00
1.000E+03	1.872E+01			1.826E+01				1.656E+01				1.270E+01				9.508E+00			8.821E+00			6.103E+00			4.428E+00		4.291E+00
1.000E+04	2.387E+01			2.218E+01				1.836E+01				1.549E+01				1.563E+01			1.290E+01			8.610E+00			6.791E+00		6.595E+00

LOG S/S' = -1.0

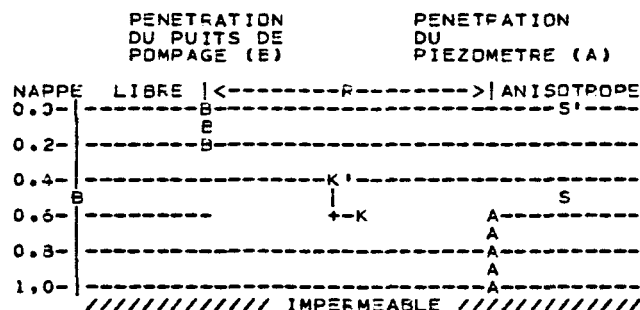
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A S A T T E M E N T S				R E D U I T S				
1.000E-01	6.073E-02	6.069E-02	6.068E-02	6.056E-02	5.943E-02	5.375E-02	3.247E-02	3.822E-03	0.0
3.162E-01	7.699E-01	7.699E-01	7.693E-01	7.640E-01	7.283E-01	5.966E-01	2.531E-01	2.577E-02	1.964E-02
1.000E+00	2.545E+00	2.544E+00	2.540E+00	2.501E+00	2.299E+00	1.650E+00	4.998E-01	7.170E-02	2.810E-02
3.162E+00	4.966E+00	4.964E+00	4.943E+00	4.795E+00	4.193E+00	2.528E+00	7.049E-01	2.295E-01	2.516E-01
1.000E+01	7.642E+00	7.634E+00	7.565E+00	7.175E+00	5.631E+00	3.097E+00	1.213E+00	8.410E-01	9.555E-01
1.000E+02	1.319E+01	1.311E+01	1.267E+01	1.110E+01	7.845E+00	5.864E+00	4.455E+00	3.207E+00	3.085E+00
1.000E+03	1.872E+01	1.827E+01	1.668E+01	1.349E+01	1.226E+01	1.120E+01	7.320E+00	5.555E+00	5.386E+00
1.000E+04	2.389E+01	2.232E+01	1.926E+01	1.849E+01	1.809E+01	1.413E+01	9.703E+00	7.898E+00	7.696E+00

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE OUVERT DE 0.6 A 1.0

TABLEAU B A

AEQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.845E-07	2.557E-07	9.594E-08	1.849E-07	4.519E-07	6.652E-07	1.692E-05	3.982E-03	1.096E-03
3.162E-01	3.021E-06	2.924E-06	2.804E-06	2.799E-06	1.409E-06	2.698E-06	7.551E-03	5.210E-02	2.257E-03
1.000E+00	9.829E-06	9.818E-06	9.614E-06	7.870E-06	2.608E-06	1.601E-04	1.037E-01	1.037E-01	2.415E-03
3.162E+00	1.926E-05	1.906E-05	1.886E-05	1.073E-05	5.381E-06	1.969E-02	2.726E-01	1.124E-01	2.923E-03
1.000E+01	2.966E-05	2.931E-05	2.661E-05	1.221E-05	2.090E-04	1.571E-01	3.565E-01	1.201E-01	4.788E-03
1.000E+02	5.104E-05	4.694E-05	3.109E-05	2.238E-04	1.645E-01	4.407E-01	3.955E-01	2.215E-01	6.389E-02
1.000E+03	6.553E-05	4.901E-05	5.534E-05	1.653E-01	4.513E-01	4.860E-01	6.848E-01	1.053E+00	1.058E+00
1.000E+04	6.554E-05	4.895E-05	8.441E-05	4.525E-01	4.973E-01	8.260E-01	2.228E+00	3.209E+00	3.182E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.987E-07	2.652E-07	9.529E-08	2.004E-07	7.685E-07	2.405E-06	2.865E-05	3.994E-03	1.086E-03
3.162E-01	3.047E-06	2.951E-06	2.789E-06	2.878E-06	2.147E-06	7.868E-06	7.588E-03	5.225E-02	2.330E-03
1.000E+00	9.871E-06	9.878E-06	9.507E-06	8.255E-06	4.591E-06	1.761E-04	1.025E-01	1.051E-01	2.837E-03
3.162E+00	1.932E-05	1.918E-05	1.841E-05	1.192E-05	1.111E-05	1.975E-02	2.737E-01	1.190E-01	4.684E-03
1.000E+01	2.972E-05	2.962E-05	2.605E-05	1.492E-05	2.260E-04	1.574E-01	3.623E-01	1.435E-01	1.313E-02
1.000E+02	5.120E-05	4.938E-05	2.923E-05	2.418E-04	1.648E-01	4.478E-01	4.672E-01	4.533E-01	3.352E-01
1.000E+03	6.557E-05	5.457E-05	5.192E-05	1.655E-01	4.585E-01	5.716E-01	1.227E+00	2.057E+00	2.067E+00
1.000E+04	6.559E-05	5.452E-05	8.077E-05	4.598E-01	5.845E-01	1.437E+00	3.445E+00	4.371E+00	4.322E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.693E-07	2.860E-07	7.211E-08	4.246E-07	9.152E-07	7.344E-06	6.571E-05	4.032E-03	1.052E-03
3.162E-01	2.952E-06	2.961E-06	2.704E-06	3.418E-06	3.403E-06	2.365E-05	7.706E-03	5.270E-02	2.569E-03
1.000E+00	9.760E-06	9.906E-06	9.491E-06	9.390E-06	9.467E-06	2.262E-04	1.030E-01	1.096E-01	4.362E-03
3.162E+00	1.919E-05	1.920E-05	1.854E-05	1.425E-05	2.719E-05	1.991E-02	2.771E-01	1.398E-01	1.260E-02
1.000E+01	2.940E-05	2.969E-05	2.645E-05	2.082E-05	2.775E-04	1.581E-01	3.802E-01	2.164E-01	6.218E-02
1.000E+02	4.951E-05	4.997E-05	3.066E-05	2.944E-04	1.655E-01	4.700E-01	6.749E-01	1.045E+00	1.051E+00
1.000E+03	6.191E-05	5.575E-05	5.400E-05	1.663E-01	4.812E-01	8.171E-01	2.216E+00	3.199E+00	3.173E+00
1.000E+04	6.192E-05	5.567E-05	8.330E-05	4.825E-01	8.343E-01	2.495E+00	4.647E+00	5.525E+00	5.466E+00

LOG S/S' = -1.5

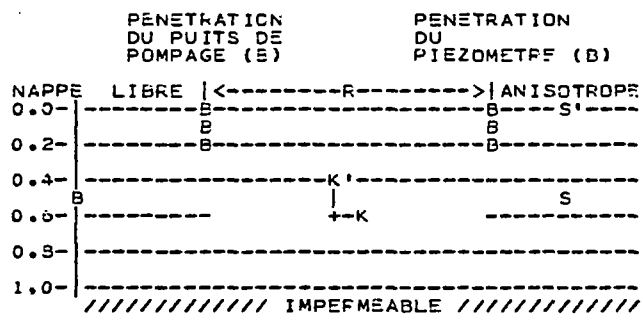
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.898E-07	2.647E-07	7.262E-08	6.228E-07	2.772E-06	2.323E-05	1.819E-04	4.147E-03	9.476E-04
3.162E-01	3.013E-06	2.935E-06	2.767E-06	3.954E-06	8.776E-06	7.390E-05	8.075E-03	5.410E-02	3.414E-03
1.000E+00	9.754E-06	9.813E-06	9.857E-06	1.104E-05	2.609E-05	3.852E-04	1.045E-01	1.234E-01	1.102E-02
3.162E+00	1.920E-05	1.899E-05	1.964E-05	1.963E-05	7.937E-05	2.041E-02	2.877E-01	2.044E-01	5.823E-02
1.000E+01	2.960E-05	2.925E-05	2.831E-05	3.744E-05	4.421E-04	1.602E-01	4.351E-01	4.346E-01	3.216E-01
1.000E+02	5.169E-05	4.805E-05	3.483E-05	4.594E-04	1.678E-01	5.374E-01	1.200E+00	2.030E+00	2.041E+00
1.000E+03	6.768E-05	5.243E-05	6.036E-05	1.686E-01	5.502E-01	1.409E+00	3.416E+00	4.341E+00	4.294E+00
1.000E+04	6.778E-05	5.227E-05	8.942E-05	5.516E-01	1.434E+00	3.717E+00	5.817E+00	6.661E+00	6.597E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.660E-07	2.382E-07	2.131E-07	9.322E-07	7.647E-06	7.339E-05	5.441E-04	4.461E-03	6.145E-04
3.162E-01	2.997E-06	2.855E-06	3.094E-06	5.294E-06	2.502E-05	2.321E-04	9.223E-03	5.836E-02	6.784E-03
1.000E+00	9.770E-06	9.699E-06	1.022E-05	1.602E-05	7.759E-05	8.843E-04	1.093E-01	1.655E-01	4.698E-02
3.162E+00	1.921E-05	1.891E-05	1.972E-05	3.582E-05	2.425E-04	2.200E-02	3.197E-01	3.926E-01	2.908E-01
1.000E+01	2.954E-05	2.945E-05	2.783E-05	9.910E-05	9.576E-04	1.670E-01	5.924E-01	9.735E-01	9.814E-01
1.000E+02	5.166E-05	4.753E-05	3.326E-05	9.767E-04	1.748E-01	7.277E-01	2.133E+00	3.110E+00	3.090E+00
1.000E+03	6.752E-05	5.149E-05	5.699E-05	1.756E-01	7.443E-01	2.408E+00	4.558E+00	5.439E+00	5.388E+00
1.000E+04	5.762E-05	5.146E-05	8.647E-05	7.462E-01	2.440E+00	4.856E+00	6.911E+00	7.760E+00	7.700E+00

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE COUVERT DE 0.0 A 0.2
ABAUQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU B B



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.198E-01	1.198E-01	1.197E-01	1.192E-01	1.147E-01	9.431E-02	3.874E-02	2.959E-03	1.811E-04
3.162E-01	1.520E+00	1.520E+00	1.518E+00	1.502E+00	1.391E+00	9.866E-01	2.271E-01	1.355E-02	3.834E-04
1.000E+00	5.024E+00	5.022E+00	5.008E+00	4.889E+00	4.274E+00	2.363E+00	3.603E-01	2.233E-02	4.223E-04
3.162E+00	9.803E+00	9.796E+00	9.734E+00	9.282E+00	7.433E+00	3.106E+00	4.037E-01	2.432E-02	6.438E-04
1.000E+01	1.509E+01	1.506E+01	1.485E+01	1.366E+01	9.569E+00	3.321E+00	4.220E-01	2.745E-02	1.453E-03
1.000E+02	2.603E+01	2.579E+01	2.443E+01	1.951E+01	1.066E+01	3.420E+00	4.363E-01	7.641E-02	4.118E-02
1.000E+03	3.688E+01	3.547E+01	3.035E+01	2.062E+01	1.081E+01	3.770E+00	1.135E+00	6.605E-01	1.013E+00
1.000E+04	4.654E+01	4.139E+01	2.147E+01	2.082E+01	1.158E+01	6.445E+00	4.361E+00	3.194E+00	3.131E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.198E-01	1.198E-01	1.197E-01	1.192E-01	1.147E-01	9.482E-02	3.874E-02	2.951E-03	1.831E-04
3.162E-01	1.520E+00	1.520E+00	1.518E+00	1.502E+00	1.391E+00	9.866E-01	2.272E-01	1.363E-02	4.195E-04
1.000E+00	5.024E+00	5.022E+00	5.008E+00	4.889E+00	4.274E+00	2.364E+00	3.611E-01	2.295E-02	6.187E-04
3.162E+00	9.803E+00	9.796E+00	9.734E+00	9.282E+00	7.433E+00	3.107E+00	4.075E-01	2.707E-02	1.417E-03
1.000E+01	1.509E+01	1.506E+01	1.485E+01	1.366E+01	9.570E+00	3.328E+00	4.360E-01	3.749E-02	5.837E-03
1.000E+02	2.603E+01	2.579E+01	2.443E+01	1.951E+01	1.068E+01	3.503E+00	6.393E-01	2.391E-01	2.897E-01
1.000E+03	3.688E+01	3.547E+01	3.035E+01	2.062E+01	1.100E+01	4.545E+00	2.457E+00	1.999E+00	2.022E+00
1.000E+04	4.654E+01	4.140E+01	2.152E+01	2.112E+01	1.309E+01	9.320E+00	5.994E+00	4.358E+00	4.265E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.198E-01	1.198E-01	1.197E-01	1.192E-01	1.147E-01	9.482E-02	3.874E-02	2.971E-03	1.890E-04
3.162E-01	1.520E+00	1.520E+00	1.518E+00	1.502E+00	1.391E+00	9.866E-01	2.276E-01	1.389E-02	5.416E-04
1.000E+00	5.024E+00	5.022E+00	5.008E+00	4.889E+00	4.274E+00	2.364E+00	3.638E-01	2.496E-02	1.304E-03
3.162E+00	9.803E+00	9.796E+00	9.734E+00	9.282E+00	7.433E+00	3.113E+00	4.197E-01	3.621E-02	5.585E-03
1.000E+01	1.509E+01	1.506E+01	1.485E+01	1.366E+01	9.574E+00	3.351E+00	4.805E-01	7.421E-02	4.002E-02
1.000E+02	2.603E+01	2.579E+01	2.443E+01	1.952E+01	1.074E+01	3.761E+00	1.129E+00	8.542E-01	1.006E+00
1.000E+03	3.688E+01	3.547E+01	3.037E+01	2.075E+01	1.157E+01	6.436E+00	4.352E+00	3.185E+00	3.122E+00
1.000E+04	4.655E+01	4.141E+01	2.165E+01	2.194E+01	1.589E+01	1.173E+01	7.149E+00	5.507E+00	5.406E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.198E-01	1.198E-01	1.197E-01	1.192E-01	1.147E-01	9.482E-02	3.876E-02	3.000E-03	2.083E-04
3.162E-01	1.520E+00	1.520E+00	1.518E+00	1.502E+00	1.391E+00	9.868E-01	2.286E-01	1.472E-02	9.854E-04
1.000E+00	5.024E+00	5.022E+00	5.008E+00	4.889E+00	4.274E+00	2.367E+00	3.723E-01	3.156E-02	4.839E-03
3.162E+00	9.803E+00	9.797E+00	9.734E+00	9.283E+00	7.436E+00	3.130E+00	4.583E-01	6.915E-02	3.733E-02
1.000E+01	1.509E+01	1.506E+01	1.485E+01	1.366E+01	9.585E+00	3.422E+00	6.223E-01	2.279E-01	2.766E-01
1.000E+02	2.603E+01	2.579E+01	2.444E+01	1.954E+01	1.091E+01	4.519E+00	2.433E+00	1.973E+00	1.996E+00
1.000E+03	3.688E+01	3.547E+01	3.040E+01	2.103E+01	1.308E+01	9.290E+00	5.666E+00	4.330E+00	4.233E+00
1.000E+04	4.655E+01	4.146E+01	2.201E+01	2.376E+01	1.916E+01	1.330E+01	8.322E+00	6.650E+00	6.537E+00

LOG S/S' = -1.0

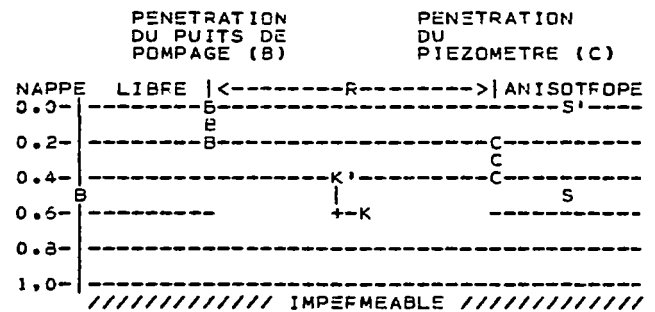
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.198E-01	1.198E-01	1.197E-01	1.192E-01	1.147E-01	9.433E-02	3.864E-02	3.067E-03	2.356E-04
3.162E-01	1.520E+00	1.520E+00	1.518E+00	1.502E+00	1.391E+00	9.374E-01	2.317E-01	1.739E-02	2.907E-03
1.000E+00	5.024E+00	5.022E+00	5.008E+00	4.889E+00	4.275E+00	2.376E+00	3.991E-01	5.472E-02	2.971E-02
3.162E+00	9.803E+00	9.797E+00	9.734E+00	9.283E+00	7.443E+00	3.183E+00	5.812E-01	2.034E-01	2.494E-01
1.000E+01	1.509E+01	1.506E+01	1.485E+01	1.366E+01	9.622E+00	3.643E+00	1.073E+00	7.945E-01	9.397E-01
1.000E+02	2.603E+01	2.580E+01	2.444E+01	1.962E+01	1.144E+01	6.356E+00	4.269E+00	3.104E+00	3.042E+00
1.000E+03	3.693E+01	3.548E+01	3.051E+01	2.181E+01	1.580E+01	1.104E+01	7.062E+00	5.427E+00	5.332E+00
1.000E+04	4.656E+01	4.159E+01	2.290E+01	2.669E+01	2.158E+01	1.450E+01	9.413E+00	7.739E+00	7.640E+00

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE CUVERT DE 0.2 A 0.4

TABLEAU B C

ABAUQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.566E-03	1.568E-03	1.586E-03	1.759E-03	3.214E-03	9.856E-03	2.539E-02	6.880E-03	5.283E-04
3.162E-01	1.987E-02	1.993E-02	2.050E-02	2.596E-02	6.284E-02	1.972E-01	2.704E-01	3.598E-02	1.102E-03
1.000E+00	6.570E-02	6.616E-02	7.075E-02	1.106E-01	3.159E-01	8.955E-01	5.479E-01	6.113E-02	1.222E-03
3.162E+00	1.234E-01	1.305E-01	1.512E-01	3.021E-01	9.177E-01	1.773E+00	6.524E-01	6.580E-02	1.611E-03
1.000E+01	1.981E-01	2.060E-01	2.767E-01	6.756E-01	1.961E+00	2.217E+00	7.062E-01	7.119E-02	3.049E-03
1.000E+02	3.502E-01	4.283E-01	8.825E-01	2.445E+00	3.433E+00	2.401E+00	7.660E-01	1.463E-01	5.277E-02
1.000E+03	5.742E-01	1.038E+00	2.665E+00	3.933E+00	3.621E+00	2.519E+00	1.278E+00	9.547E-01	1.025E+00
1.000E+04	1.186E+00	2.824E+00	4.155E+00	4.123E+00	3.751E+00	3.439E+00	3.567E+00	3.169E+00	3.133E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.566E-03	1.568E-03	1.586E-03	1.760E-03	3.214E-03	9.856E-03	2.539E-02	6.884E-03	5.325E-04
3.162E-01	1.987E-02	1.993E-02	2.050E-02	2.596E-02	6.284E-02	1.972E-01	2.704E-01	3.611E-02	1.175E-03
1.000E+00	6.570E-02	6.616E-02	7.075E-02	1.106E-01	3.159E-01	8.955E-01	5.485E-01	6.218E-02	1.562E-03
3.162E+00	1.234E-01	1.305E-01	1.512E-01	3.021E-01	9.177E-01	1.779E+00	6.544E-01	7.049E-02	2.985E-03
1.000E+01	1.981E-01	2.060E-01	2.767E-01	6.756E-01	1.961E+00	2.219E+00	7.182E-01	8.779E-02	9.653E-03
1.000E+02	3.502E-01	4.283E-01	8.825E-01	2.445E+00	3.435E+00	2.427E+00	8.957E-01	3.456E-01	3.098E-01
1.000E+03	5.742E-01	1.038E+00	2.665E+00	3.935E+00	3.650E+00	2.772E+00	2.183E+00	2.010E+00	2.026E+00
1.000E+04	1.186E+00	2.824E+00	4.157E+00	4.152E+00	4.030E+00	4.727E+00	4.915E+00	4.321E+00	4.267E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.566E-03	1.568E-03	1.586E-03	1.760E-03	3.213E-03	9.856E-03	2.539E-02	6.896E-03	5.450E-04
3.162E-01	1.987E-02	1.993E-02	2.050E-02	2.596E-02	6.283E-02	1.972E-01	2.705E-01	3.651E-02	1.411E-03
1.000E+00	6.570E-02	6.616E-02	7.075E-02	1.106E-01	3.159E-01	8.966E-01	5.502E-01	6.551E-02	2.790E-03
3.162E+00	1.234E-01	1.305E-01	1.512E-01	3.021E-01	9.177E-01	1.788E+00	6.749E-01	8.552E-02	9.288E-03
1.000E+01	1.981E-01	2.060E-01	2.767E-01	6.756E-01	1.961E+00	2.224E+00	7.557E-01	1.428E-01	5.139E-02
1.000E+02	3.502E-01	4.283E-01	8.825E-01	2.445E+00	3.441E+00	2.507E+00	1.271E+00	9.480E-01	1.018E+00
1.000E+03	5.742E-01	1.038E+00	2.665E+00	3.941E+00	3.739E+00	3.430E+00	3.558E+00	3.159E+00	3.124E+00
1.000E+04	1.186E+00	2.824E+00	4.163E+00	4.242E+00	4.740E+00	6.303E+00	6.127E+00	5.467E+00	5.407E+00

LOG S/S' = -1.5

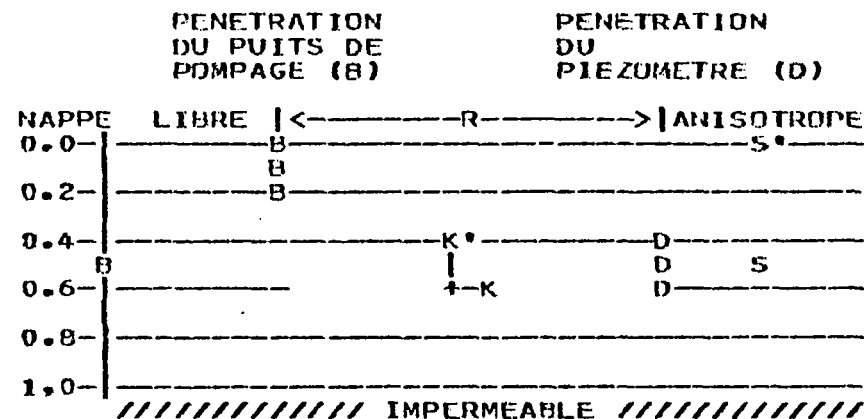
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.566E-03	1.568E-03	1.587E-03	1.760E-03	3.214E-03	9.857E-03	2.539E-02	6.933E-03	5.838E-04
3.162E-01	1.987E-02	1.993E-02	2.051E-02	2.596E-02	6.284E-02	1.972E-01	2.709E-01	3.777E-02	2.222E-03
1.000E+00	6.570E-02	6.616E-02	7.075E-02	1.106E-01	3.159E-01	8.969E-01	5.555E-01	7.611E-02	8.200E-03
3.162E+00	1.234E-01	1.305E-01	1.512E-01	3.021E-01	9.177E-01	1.782E+00	7.046E-01	1.348E-01	4.819E-02
1.000E+01	1.981E-01	2.060E-01	2.767E-01	6.756E-01	1.961E+00	2.240E+00	8.707E-01	3.313E-01	2.972E-01
1.000E+02	3.502E-01	4.283E-01	8.826E-01	2.445E+00	3.459E+00	2.742E+00	2.157E+00	1.984E+00	2.001E+00
1.000E+03	5.742E-01	1.038E+00	2.665E+00	3.960E+00	3.999E+00	4.699E+00	4.887E+00	4.293E+00	4.240E+00
1.000E+04	1.186E+00	2.824E+00	4.182E+00	4.505E+00	6.066E+00	7.669E+00	7.288E+00	6.609E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				F E D U I T S				
1.000E-01	1.566E-03	1.568E-03	1.587E-03	1.759E-03	3.213E-03	9.855E-03	2.539E-02	7.048E-03	6.709E-04
3.162E-01	1.987E-02	1.993E-02	2.051E-02	2.596E-02	6.283E-02	1.972E-01	2.721E-01	4.177E-02	5.330E-03
1.000E+00	6.570E-02	6.617E-02	7.075E-02	1.106E-01	3.159E-01	8.969E-01	5.721E-01	1.103E-01	3.909E-02
3.162E+00	1.234E-01	1.305E-01	1.512E-01	3.021E-01	9.177E-01	1.788E+00	7.951E-01	2.996E-01	2.689E-01
1.000E+01	1.981E-01	2.060E-01	2.767E-01	6.756E-01	1.961E+00	2.288E+00	1.199E+00	8.846E-01	9.522E-01
1.000E+02	3.502E-01	4.283E-01	8.826E-01	2.445E+00	3.515E+00	3.344E+00	3.474E+00	3.675E+00	3.044E+00
1.000E+03	5.742E-01	1.038E+00	2.665E+00	4.017E+00	4.652E+00	6.215E+00	6.040E+00	5.386E+00	5.332E+00
1.000E+04	1.186E+00	2.824E+00	4.239E+00	5.164E+00	7.604E+00	8.829E+00	8.375E+00	7.697E+00	7.640E+00

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE OUVERT DE 0.4 A 0.6
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABEAU B D



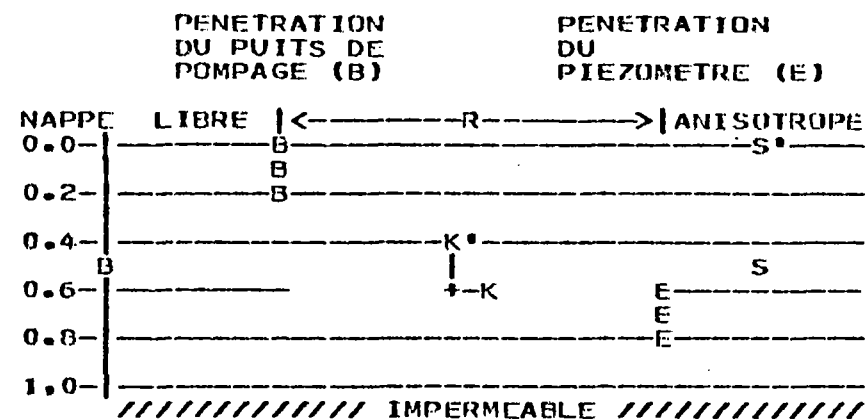
LOG S/S' = -2.0

LOG K*R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.659E-06	2.428E-06	2.421E-06	2.170E-06	1.889E-06	1.957E-07	1.881E-03	6.950E-03	8.558E-04	
1.000E+00	1.079E-04	1.078E-04	1.067E-04	8.389E-05	6.531E-06	3.329E-02	3.189E-01	9.246E-02	4.047E-03	
1.000E+01	3.238E-04	3.224E-04	2.873E-04	1.057E-04	4.591E-02	6.501E-01	5.698E-01	1.857E-01	6.033E-02	
1.000E+02	5.577E-04	5.206E-04	3.132E-04	4.754E-02	7.118E-01	9.428E-01	9.278E-01	9.824E-01	1.028E+00	
1.000E+03	7.582E-04	5.468E-04	4.790E-02	7.186E-01	1.009E+00	1.417E+00	2.653E+00	3.105E+00	3.125E+00	
1.000E+04	7.826E-04	4.827E-02	7.201E-01	1.017E+00	1.499E+00	3.376E+00	5.068E+00	5.402E+00	5.407E+00	

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE OUVERT DE 0.6 A 0.8

TABLEAU B E

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



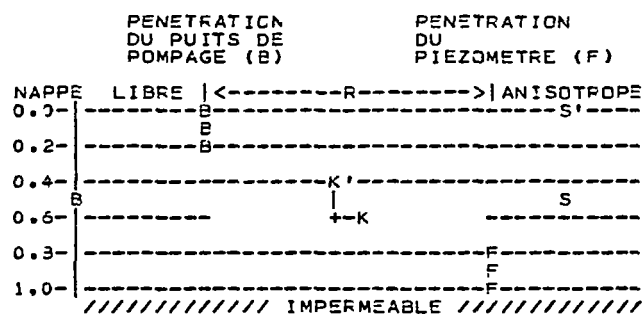
LOG S/S' = -2.0

LOG K *R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.194E-07	2.212E-07	4.861E-07	8.433E-07	3.668E-07	0.0	2.338E-05	4.839E-03	1.077E-03	
1.000E+00	1.126E-05	1.116E-05	1.207E-05	1.266E-05	2.216E-06	3.032E-04	1.401E-01	1.064E-01	4.941E-03	
1.000E+01	3.397E-05	3.450E-05	3.506E-05	1.790E-05	3.976E-04	2.224E-01	4.103E-01	2.069E-01	6.644E-02	
1.000E+02	5.938E-05	6.164E-05	4.089E-05	4.242E-04	2.338E-01	5.268E-01	6.819E-01	9.859E-01	1.034E+00	
1.000E+03	7.623E-05	6.778E-05	8.670E-05	2.350E-01	5.420E-01	8.452E-01	2.108E+00	3.052E+00	3.126E+00	
1.000E+04	7.739E-05	6.875E-05	1.439E-04	5.437E-01	8.659E-01	2.394E+00	4.426E+00	5.341E+00	5.407E+00	

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE COUVERT DE 0.6 A 1.0

TABLEAU B F

ABAUQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LCG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	0.0	2.545E-07	5.253E-08	8.826E-08	2.695E-07	0.0	0.0	3.122E-03	1.164E-03
3.162E-01	1.245E-06	1.335E-06	1.457E-06	1.535E-06	7.770E-07	1.588E-07	1.310E-03	5.214E-02	2.403E-03
1.000E+00	4.645E-06	4.738E-06	4.766E-06	4.071E-06	1.137E-06	1.214E-06	6.468E-02	1.063E-01	2.628E-03
3.162E+00	9.152E-06	9.724E-06	9.476E-06	5.623E-06	1.437E-06	3.097E-03	2.353E-01	1.152E-01	3.342E-03
1.000E+01	1.422E-05	1.477E-05	1.355E-05	6.337E-06	2.910E-06	9.216E-02	3.229E-01	1.227E-01	5.858E-03
1.000E+02	2.522E-05	2.432E-05	1.520E-05	7.690E-06	9.553E-02	3.792E-01	3.554E-01	2.109E-01	7.127E-02
1.000E+03	3.288E-05	2.434E-05	1.548E-05	9.594E-02	3.857E-01	4.150E-01	5.638E-01	9.868E-01	1.044E+00
1.000E+04	3.299E-05	2.433E-05	1.633E-05	3.865E-01	4.219E-01	6.708E-01	1.885E+00	3.028E+00	3.135E+00

LCG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	0.0	1.990E-07	4.080E-08	1.234E-07	5.513E-08	1.644E-07	1.600E-07	3.122E-03	1.172E-03
3.162E-01	1.261E-06	1.214E-06	1.478E-06	1.640E-06	3.736E-07	3.929E-07	1.310E-03	5.224E-02	2.538E-03
1.000E+00	4.645E-06	4.510E-06	4.835E-06	4.351E-06	7.578E-07	1.377E-06	6.469E-02	1.076E-01	3.253E-03
3.162E+00	9.235E-06	9.562E-06	9.677E-06	5.909E-06	1.272E-06	3.097E-03	2.355E-01	1.215E-01	5.748E-03
1.000E+01	1.435E-05	1.482E-05	1.402E-05	6.567E-06	2.559E-06	9.219E-02	3.268E-01	1.452E-01	1.614E-02
1.000E+02	2.541E-05	2.547E-05	1.579E-05	8.349E-06	9.561E-02	3.839E-01	4.109E-01	4.373E-01	3.414E-01
1.000E+03	3.327E-05	2.806E-05	1.666E-05	9.597E-02	3.905E-01	4.781E-01	1.022E+00	1.924E+00	2.033E+00
1.000E+04	3.336E-05	2.805E-05	1.750E-05	3.913E-01	4.856E-01	1.151E+00	2.993E+00	4.164E+00	4.267E+00

LCG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	0.0	2.528E-07	4.131E-08	2.411E-07	3.477E-07	8.536E-08	1.353E-07	3.122E-03	1.195E-03
3.162E-01	1.241E-06	1.329E-06	1.606E-06	1.824E-06	9.379E-07	2.755E-07	1.310E-03	5.256E-02	2.973E-03
1.000E+00	4.745E-06	4.752E-06	5.061E-06	4.434E-06	1.523E-06	1.234E-06	6.475E-02	1.117E-01	5.411E-03
3.162E+00	9.164E-06	9.895E-06	1.021E-05	5.833E-06	2.069E-06	3.097E-03	2.375E-01	1.414E-01	1.554E-02
1.000E+01	1.331E-05	1.539E-05	1.461E-05	6.674E-06	3.343E-06	9.227E-02	3.395E-01	2.147E-01	6.956E-02
1.000E+02	2.542E-05	2.577E-05	1.734E-05	8.385E-06	9.570E-02	3.936E-01	5.749E-01	4.616E-01	1.037E+00
1.000E+03	3.319E-05	2.571E-05	2.005E-05	9.606E-02	4.054E-01	6.619E-01	1.870E+00	3.019E+00	3.126E+00
1.000E+04	3.330E-05	2.589E-05	2.088E-05	4.063E-01	6.718E-01	2.044E+00	4.143E+00	5.305E+00	5.407E+00

LCG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	0.0	2.293E-07	1.593E-07	0.0	3.433E-07	0.0	6.435E-08	3.130E-03	1.266E-03
3.162E-01	1.196E-06	1.296E-06	1.663E-06	1.241E-06	8.468E-07	3.844E-08	1.310E-03	5.356E-02	4.416E-03
1.000E+00	4.579E-06	4.743E-06	5.074E-06	3.919E-06	1.404E-06	9.032E-07	6.493E-02	1.244E-01	1.393E-02
3.162E+00	9.028E-06	1.009E-05	1.125E-05	5.772E-06	1.899E-06	3.097E-03	2.430E-01	2.025E-01	6.557E-02
1.000E+01	1.409E-05	1.573E-05	1.553E-05	6.758E-06	3.159E-06	9.234E-02	3.733E-01	4.189E-01	3.281E-01
1.000E+02	2.562E-05	2.659E-05	1.760E-05	8.216E-06	9.598E-02	4.436E-01	5.957E-01	1.898E+00	2.008E+00
1.000E+03	3.610E-05	2.856E-05	1.880E-05	9.634E-02	4.511E-01	1.123E+00	2.965E+00	4.137E+00	4.260E+00
1.000E+04	3.613E-05	2.855E-05	1.986E-05	4.520E-01	1.137E+00	3.160E+00	5.288E+00	6.445E+00	6.537E+00

LCG S/S' = -1.0

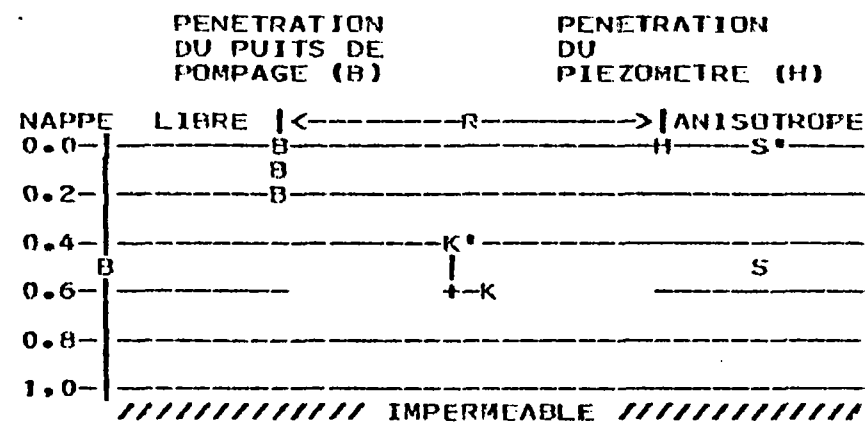
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	0.0	3.259E-07	2.064E-07	1.965E-07	1.969E-07	0.0	0.0	3.145E-03	1.462E-03
3.162E-01	1.206E-06	1.465E-06	1.748E-06	1.812E-06	5.945E-07	0.0	1.303E-03	5.664E-02	9.509E-03
1.000E+00	4.763E-06	4.992E-06	5.360E-06	4.679E-06	9.417E-07	0.0	6.548E-02	1.629E-01	5.419E-02
3.162E+00	9.154E-06	1.033E-05	1.033E-05	6.537E-06	7.933E-07	3.097E-03	2.595E-01	3.775E-01	2.982E-01
1.000E+01	1.422E-05	1.589E-05	1.439E-05	7.458E-06	1.638E-07	9.335E-02	4.905E-01	9.134E-01	9.709E-01
1.000E+02	2.520E-05	2.669E-05	1.635E-05	9.986E-06	9.682E-02	5.723E-01	1.786E+00	2.935E+00	3.046E+00
1.000E+03	3.119E-05	3.064E-05	1.763E-05	9.719E-02	5.817E-01	1.957E+00	4.057E+00	5.225E+00	5.332E+00
1.000E+04	3.136E-05	3.072E-05	1.855E-05	5.828E-01	1.975E+00	4.257E+00	6.369E+00	7.533E+00	7.640E+00

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE PONCTUEL OUVERT A LA PROFONDEUR 0.05

TABLEAU B H

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S* = -2.0

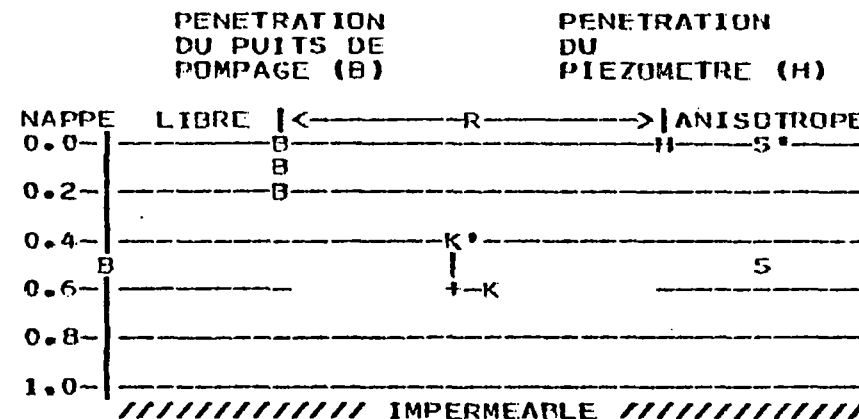
LOG K*R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.116E-01	1.116E-01	1.117E-01	1.132E-01	1.214E-01	9.859E-02	2.752E-02	1.598E-03	9.708E-05	
1.000E+00	4.680E+00	4.683E+00	4.721E+00	4.974E+00	4.634E+00	1.948E+00	2.179E-01	1.358E-02	9.135E-04	
1.000E+01	1.406E+01	1.413E+01	1.460E+01	1.456E+01	9.186E+00	2.567E+00	3.047E-01	5.436E-02	3.692E-02	
1.000E+02	2.435E+01	2.488E+01	2.508E+01	1.962E+01	9.954E+00	3.058E+00	9.613E-01	8.223E-01	1.002E+00	
1.000E+03	3.520E+01	3.546E+01	3.020E+01	2.042E+01	1.105E+01	6.511E+00	4.464E+00	3.187E+00	3.122E+00	
1.000E+04	4.579E+01	4.059E+01	3.101E+01	2.170E+01	1.675E+01	1.271E+01	7.328E+00	5.513E+00	5.406E+00	

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE PONCTUEL OUVERT A LA PROFONDEUR 0.1

TABEAU B II

ABaque POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELITSOVA



LOG S/S' = -2.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

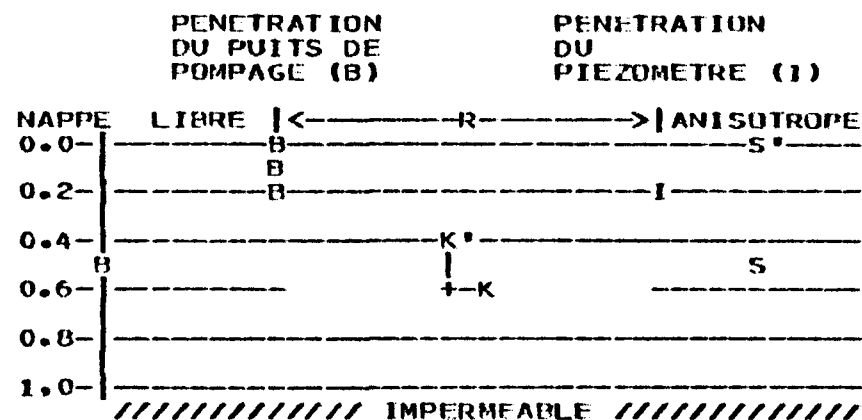
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.162E-01	1.162E-01	1.163E-01	1.172E-01	1.222E-01	1.218E-01	4.674E-02	3.111E-03	1.892E-04	
1.000E+00	4.874E+00	4.876E+00	4.900E+00	5.053E+00	5.177E+00	3.016E+00	3.996E-01	2.529E-02	1.308E-03	
1.000E+01	1.464E+01	1.468E+01	1.497E+01	1.544E+01	1.204E+01	4.105E+00	5.204E-01	7.507E-02	4.010E-02	
1.000E+02	2.533E+01	2.565E+01	2.630E+01	2.304E+01	1.329E+01	4.507E+00	1.193E+00	8.577E-01	1.006E+00	
1.000E+03	3.639E+01	3.708E+01	3.397E+01	2.431E+01	1.388E+01	7.006E+00	4.406E+00	3.187E+00	3.122E+00	
1.000E+04	4.784E+01	4.476E+01	3.526E+01	2.493E+01	1.720E+01	1.209E+01	7.199E+00	5.509E+00	5.406E+00	

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE PONCTUEL OUVERT A LA PROFONDEUR 0.2

TABLEAU B 1

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S* = -2.0

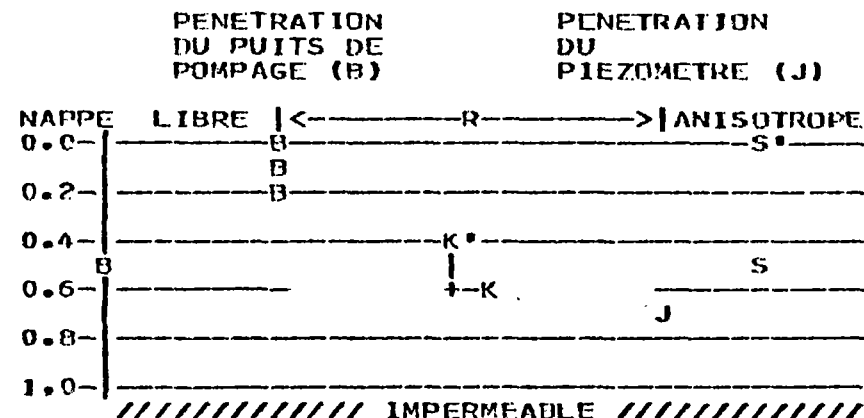
LOG K*R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	5.992E-02	5.991E-02	5.994E-02	6.018E-02	6.157E-02	6.225E-02	4.834E-02	5.568E-03	3.724E-04	
1.000E+00	2.512E+00	2.513E+00	2.519E+00	2.562E+00	2.609E+00	2.337E+00	5.895E-01	4.717E-02	2.076E-03	
1.000E+01	7.546E+00	7.558E+00	7.638E+00	7.786E+00	7.452E+00	3.870E+00	7.610E-01	1.126E-01	4.608E-02	
1.000E+02	1.304E+01	1.313E+01	1.333E+01	1.309E+01	9.183E+00	4.171E+00	1.373E+00	9.132E-01	1.013E+00	
1.000E+03	1.867E+01	1.888E+01	1.868E+01	1.484E+01	9.519E+00	5.566E+00	4.063E+00	3.178E+00	3.123E+00	
1.000E+04	2.442E+01	2.423E+01	2.043E+01	1.518E+01	1.110E+01	9.225E+00	6.731E+00	5.493E+00	5.407E+00	

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE PONCTUEL OUVERT A LA PROFONDEUR 0.7

TABLÉAU B J

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S* = -2.0

LOG K*R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

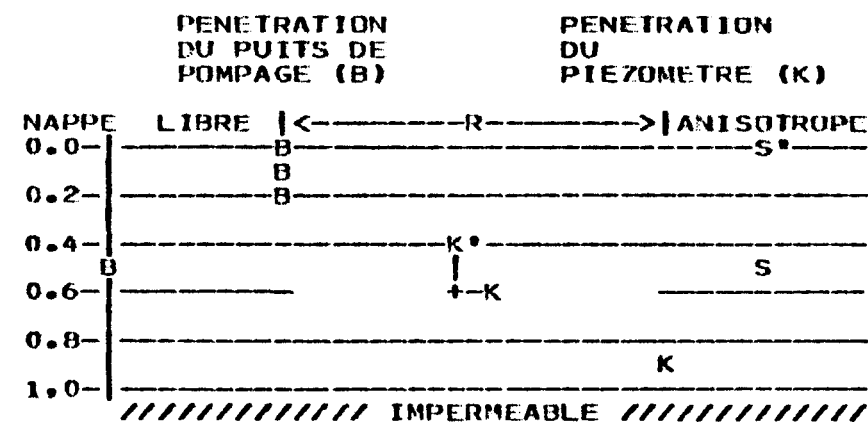
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	9.011E-05	8.999E-05	8.899E-05	7.895E-05	2.691E-05	0.0	8.222E-06	4.815E-03	1.081E-03	
1.000E+00	3.776E-03	3.749E-03	3.495E-03	1.860E-03	8.313E-05	1.019E-04	1.357E-01	1.067E-01	4.959E-03	
1.000E+01	1.130E-02	1.086E-02	7.781E-03	2.124E-03	2.155E-04	2.120E-01	4.064E-01	2.074E-01	6.656E-02	
1.000E+02	1.906E-02	1.561E-02	8.093E-03	2.261E-03	2.224E-01	5.169E-01	6.761E-01	9.862E-01	1.034E+00	
1.000E+03	2.386E-02	1.593E-02	8.229E-03	2.255E-01	5.311E-01	8.316E-01	2.095E+00	3.051E+00	3.126E+00	
1.000E+04	2.419E-02	1.606E-02	2.319E-01	5.347E-01	8.510E-01	2.371E+00	4.411E+00	5.340E+00	5.407E+00	

PUITS CREPINE DE 0.0 A 0.2 ET PIEZOMETRE PONCTUEL OUVERT A LA PROFONDEUR 0.9

TABLEAU B K

ABaque pour l'interprétation de pompages en nappe libre anisotrope.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA


$$\text{LOG } S/S^0 = -2.0$$

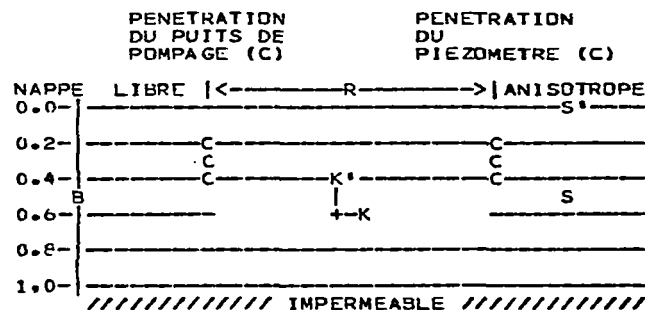
LOG K [*] R ₂ /KB ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
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TT/R2S R A B A T T E M E N T S R E D U I T S

1.000E-01	5.412E-05	5.439E-05	5.363E-05	4.831E-05	1.666E-05	1.737E-07	4.802E-07	3.047E-03	1.200E-03
1.000E+00	2.278E-03	2.262E-03	2.110E-03	1.128E-03	5.395E-05	1.279E-06	6.178E-02	1.119E-01	5.431E-03
1.000E+01	6.817E-03	6.552E-03	4.703E-03	1.294E-03	5.656E-05	8.744E-02	3.366E-01	2.150E-01	6.969E-02
1.000E+02	1.150E-02	9.427E-03	4.898E-03	1.297E-03	9.067E-02	3.938E-01	5.706E-01	9.814E-01	1.037E+00
1.000E+03	1.441E-02	9.627E-03	4.902E-03	9.223E-02	4.004E-01	6.549E-01	1.861E+00	3.018E+00	3.126E+00
1.000E+04	1.461E-02	9.629E-03	4.903E-03	4.025E-01	6.646E-01	2.031E+00	4.132E+00	5.303E+00	5.407E+00

PUITS A PENETRATION DE 0.2 A 0.4 ET PIEZOMETRE OUVERT DE 0.2 A 0.4
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU C C



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.598E-02	1.677E-02	1.532E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.841E-01	9.771E-02	3.156E-03
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.226E+00	1.699E-01	3.355E-03
3.162E+00	9.931E+00	9.927E+00	9.886E+00	9.584E+00	8.351E+00	5.177E+00	1.537E+00	1.806E-01	3.978E-03
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.157E+01	6.182E+00	1.655E+00	1.872E-01	6.179E-03
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.479E+01	6.667E+00	1.703E+00	2.742E-01	6.608E-02
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.525E+01	1.528E+01	6.731E+00	2.048E+00	1.057E+00	1.038E+00
1.000E+04	4.773E+01	4.426E+01	3.632E+01	2.575E+01	1.535E+01	7.190E+00	3.740E+00	3.161E+00	3.134E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.597E-02	1.677E-02	1.538E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.840E-01	9.783E-02	3.270E-03
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.226E+00	1.711E-01	3.898E-03
3.162E+00	9.931E+00	9.927E+00	9.886E+00	9.584E+00	8.351E+00	5.177E+00	1.538E+00	1.862E-01	6.081E-03
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.157E+01	6.183E+00	1.662E+00	2.069E-01	1.528E-02
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.479E+01	6.678E+00	1.790E+00	4.834E-01	3.308E-01
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.526E+01	1.530E+01	6.850E+00	2.670E+00	2.037E+00	2.031E+00
1.000E+04	4.773E+01	4.426E+01	3.632E+01	2.576E+01	1.547E+01	7.945E+00	4.938E+00	4.303E+00	4.267E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.597E-02	1.678E-02	1.556E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.841E-01	9.823E-02	3.641E-03
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.226E+00	1.748E-01	5.777E-03
3.162E+00	9.931E+00	9.927E+00	9.886E+00	9.584E+00	8.351E+00	5.177E+00	1.544E+00	2.038E-01	1.478E-02
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.157E+01	6.184E+00	1.685E+00	2.698E-01	6.448E-02
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.479E+01	6.711E+00	2.040E+00	1.050E+00	1.031E+00
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.526E+01	1.533E+01	7.181E+00	3.725E+00	3.152E+00	3.125E+00
1.000E+04	4.773E+01	4.426E+01	3.632E+01	2.580E+01	1.582E+01	9.096E+00	6.111E+00	5.445E+00	5.407E+00

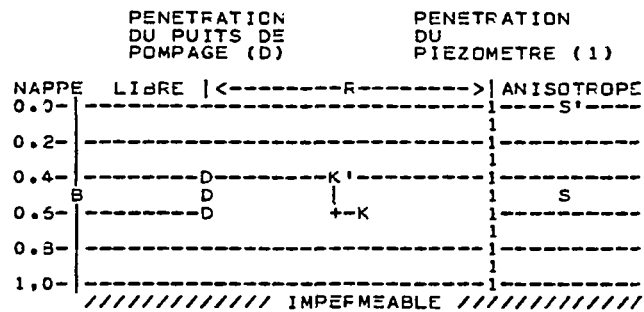
LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.597E-02	1.680E-02	1.612E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.841E-01	9.946E-02	4.874E-03
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.228E+00	1.865E-01	1.329E-02
3.162E+00	9.931E+00	9.927E+00	9.886E+00	9.584E+00	8.351E+00	5.177E+00	1.559E+00	2.593E-01	6.075E-02
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.157E+01	6.188E+00	1.756E+00	4.666E-01	3.178E-01
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.480E+01	6.813E+00	2.644E+00	2.012E+00	2.005E+00
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.526E+01	1.544E+01	7.916E+00	4.910E+00	4.275E+00	4.240E+00
1.000E+04	4.773E+01	4.426E+01	3.633E+01	2.590E+01	1.657E+01	1.031E+01	7.251E+00	6.586E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.597E-02	1.689E-02	1.753E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.843E-01	1.033E-01	9.270E-03
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.234E+00	2.229E-01	5.011E-02
3.162E+00	9.931E+00	9.927E+00	9.886E+00	9.584E+00	8.351E+00	5.178E+00	1.607E+00	4.292E-01	2.885E-01
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.157E+01	6.199E+00	1.956E+00	9.838E-01	9.646E-01
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.481E+01	7.088E+00	3.640E+00	3.068E+00	3.045E+00
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.527E+01	1.572E+01	9.009E+00	6.024E+00	5.365E+00	5.332E+00
1.000E+04	4.773E+01	4.426E+01	3.634E+01	2.619E+01	1.767E+01	1.143E+01	8.344E+00	7.674E+00	7.641E+00

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LGG S/S' = -3.0

LOG K'F2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.491E-02	2.492E-02	1.966E-02	3.337E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.094E-01	1.767E-01	6.791E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.233E-01	3.343E-01	6.878E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.021E+00	1.495E+00	3.559E-01	7.117E-03	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	2.956E+00	1.750E+00	3.640E-01	8.173E-03	
1.000E+02	5.416E+00	5.417E+00	5.416E+00	5.416E+00	5.228E+00	3.882E+00	1.815E+00	4.710E-01	6.191E-02	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.528E+00	6.165E+00	3.963E+00	2.203E+00	1.399E+00	1.118E+00	
1.000E+04	1.002E+01	1.002E+01	9.832E+00	8.466E+00	6.249E+00	4.470E+00	4.136E+00	3.785E+00	3.332E+00	

LGG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.491E-02	2.496E-02	1.970E-02	3.272E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.096E-01	1.769E-01	6.736E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.238E-01	3.357E-01	6.990E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.021E+00	1.498E+00	3.627E-01	8.025E-03	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	2.957E+00	1.758E+00	3.884E-01	1.422E-02	
1.000E+02	5.416E+00	5.417E+00	5.416E+00	5.417E+00	5.229E+00	3.894E+00	1.913E+00	7.232E-01	3.456E-01	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.529E+00	6.178E+00	4.095E+00	2.910E+00	2.530E+00	2.180E+00	
1.000E+04	1.002E+01	1.002E+01	9.832E+00	8.479E+00	6.385E+00	5.315E+00	5.528E+00	5.012E+00	4.494E+00	

LGG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					F E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.491E-02	2.494E-02	2.511E-02	1.983E-02	3.068E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.100E-01	1.775E-01	6.576E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	9.255E-01	3.403E-01	7.568E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.022E+00	1.504E+00	3.843E-01	1.360E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.137E+00	2.960E+00	1.785E+00	4.653E-01	5.991E-02	
1.000E+02	5.416E+00	5.417E+00	5.416E+00	5.417E+00	5.232E+00	3.932E+00	2.195E+00	1.391E+00	1.110E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.532E+00	6.217E+00	4.461E+00	4.127E+00	3.774E+00	3.322E+00	
1.000E+04	1.002E+01	1.002E+01	9.835E+00	8.519E+00	6.762E+00	6.637E+00	6.841E+00	6.205E+00	5.649E+00	

LGG S/S' = -1.5

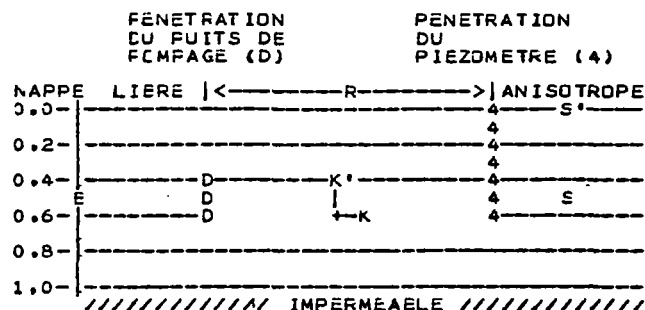
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.491E-02	2.501E-02	2.557E-02	2.022E-02	2.438E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.163E-01	3.115E-01	1.795E-01	6.199E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.045E+00	9.300E-01	3.544E-01	1.156E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.024E+00	1.525E+00	4.517E-01	5.529E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.137E+00	2.968E+00	1.866E+00	7.019E-01	3.302E-01	
1.000E+02	5.416E+00	5.417E+00	5.417E+00	5.418E+00	5.241E+00	4.046E+00	2.882E+00	2.459E+00	2.150E+00	
1.000E+03	7.717E+00	7.717E+00	7.718E+00	7.540E+00	6.336E+00	5.287E+00	5.498E+00	4.978E+00	4.462E+00	
1.000E+04	1.002E+01	1.002E+01	9.844E+00	8.637E+00	7.605E+00	8.059E+00	9.066E+00	7.360E+00	6.786E+00	

LGG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.494E-02	2.524E-02	2.702E-02	2.131E-02	5.212E-04	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.170E-01	3.161E-01	1.853E-01	6.064E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.045E+00	1.047E+00	9.466E-01	3.974E-01	4.215E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.039E+00	2.031E+00	1.587E+00	6.537E-01	2.953E-01	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.140E+00	2.993E+00	2.096E+00	1.307E+00	1.022E+00	
1.000E+02	5.416E+00	5.417E+00	5.417E+00	5.420E+00	5.267E+00	4.358E+00	4.036E+00	3.670E+00	3.228E+00	
1.000E+03	7.717E+00	7.717E+00	7.723E+00	7.567E+00	6.663E+00	6.548E+00	6.747E+00	6.104E+00	5.561E+00	
1.000E+04	1.002E+01	1.002E+01	9.872E+00	8.961E+00	8.895E+00	9.302E+00	9.207E+00	8.460E+00	7.885E+00	

PUITS A PENETRATION DE 0.4 A 0.6 ET PIEZOMETRE OUVERT DE 0.0 A 0.6
 ABAQUE POUR L'INTERPRETATION DE FCMAGES EN NAPPE LIBRE ANISTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSCVA

TABLEAU D 4



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.035E-02	3.815E-02	3.172E-02	1.676E-02	2.298E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.522E-01	1.287E-01	4.697E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	9.180E-01	2.372E-01	4.645E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.539E+00	1.335E+00	2.526E-01	5.291E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.411E+00	1.509E+00	2.595E-01	6.966E-03
1.000E+02	8.910E+00	8.885E+00	8.733E+00	8.181E+00	6.736E+00	4.075E+00	1.565E+00	3.565E-01	6.413E-02
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.040E+01	7.409E+00	4.146E+00	1.930E+00	1.209E+00	1.077E+00
1.000E+04	1.631E+01	1.573E+01	1.416E+01	1.107E+01	7.483E+00	4.628E+00	3.735E+00	3.449E+00	3.231E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.035E-02	3.815E-02	3.175E-02	1.677E-02	2.270E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.606E-01	3.523E-01	1.289E-01	4.733E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	9.184E-01	2.385E-01	5.188E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.539E+00	1.335E+00	2.587E-01	6.844E-03
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.411E+00	1.517E+00	2.818E-01	1.470E-02
1.000E+02	8.910E+00	8.885E+00	8.733E+00	8.181E+00	6.737E+00	4.086E+00	1.657E+00	5.862E-01	3.363E-01
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.040E+01	7.420E+00	4.271E+00	2.593E+00	2.262E+00	2.104E+00
1.000E+04	1.631E+01	1.573E+01	1.416E+01	1.108E+01	7.613E+00	5.426E+00	5.030E+00	4.632E+00	4.379E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.035E-02	3.817E-02	3.184E-02	1.681E-02	2.182E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.606E-01	3.526E-01	1.293E-01	4.855E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	9.196E-01	2.425E-01	4.465E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.543E+00	1.341E+00	2.781E-01	1.411E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.413E+00	1.542E+00	3.512E-01	6.234E-02
1.000E+02	8.910E+00	8.885E+00	8.733E+00	8.181E+00	6.739E+00	4.122E+00	1.922E+00	1.201E+00	1.070E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.040E+01	7.457E+00	4.619E+00	3.726E+00	3.435E+00	3.222E+00
1.000E+04	1.631E+01	1.573E+01	1.416E+01	1.112E+01	7.970E+00	6.660E+00	6.270E+00	5.799E+00	5.526E+00

LOG S/S' = -1.5

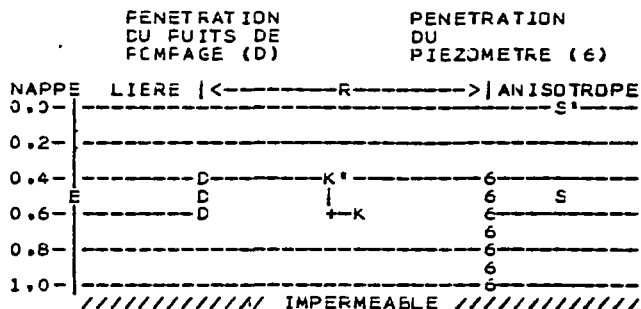
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.036E-02	3.821E-02	3.212E-02	1.694E-02	1.912E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.608E-01	3.535E-01	1.307E-01	5.337E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.420E+00	9.233E-01	2.550E-01	1.235E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.542E+00	1.359E+00	3.390E-01	5.618E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.420E+00	1.617E+00	5.668E-01	3.241E-01
1.000E+02	8.910E+00	8.885E+00	8.733E+00	8.181E+00	6.745E+00	4.229E+00	2.566E+00	2.233E+00	2.076E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.040E+01	7.569E+00	5.398E+00	5.000E+00	4.601E+00	4.349E+00
1.000E+04	1.631E+01	1.573E+01	1.417E+01	1.123E+01	8.766E+00	7.965E+00	7.451E+00	6.942E+00	6.659E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.091E-02	4.037E-02	3.836E-02	3.300E-02	1.727E-02	1.080E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.056E-01	4.612E-01	3.563E-01	1.347E-01	7.621E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.421E+00	9.347E-01	2.935E-01	4.634E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.091E+00	2.546E+00	1.413E+00	5.232E-01	2.921E-01
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.545E+00	3.439E+00	1.821E+00	1.125E+00	9.578E-01
1.000E+02	8.910E+00	8.885E+00	8.733E+00	8.183E+00	6.766E+00	4.522E+00	3.638E+00	3.344E+00	3.135E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.043E+01	7.872E+00	6.572E+00	6.179E+00	5.706E+00	5.445E+00
1.000E+04	1.631E+01	1.573E+01	1.419E+01	1.153E+01	9.950E+00	9.152E+00	8.568E+00	8.041E+00	7.761E+00

PUITS A PENETRATION DE 0.4 A 0.6 ET PIEZOMETRE OUVERT DE 0.4 A 1.0
 ABAQUE POUR L'INTERPRETATION DE FCMPS EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU D 6



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.098E-02	4.035E-02	3.815E-02	3.173E-02	2.421E-02	4.533E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.631E-01	2.329E-01	9.243E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.097E+00	4.452E-01	5.519E-03
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.568E+00	1.852E+00	4.733E-01	1.033E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.681E+00	2.193E+00	4.610E-01	1.319E-02
1.000E+02	9.910E+00	8.885E+00	8.733E+00	8.181E+00	7.019E+00	4.906E+00	2.246E+00	5.603E-01	5.509E-02
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.257E+00	4.962E+00	2.456E+00	1.358E+00	1.097E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.192E+01	8.314E+00	5.195E+00	3.694E+00	3.455E+00	3.237E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.098E-02	4.035E-02	3.815E-02	3.174E-02	2.424E-02	4.508E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.605E-01	3.631E-01	2.331E-01	9.344E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.097E+00	4.464E-01	1.018E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.568E+00	1.853E+00	4.796E-01	1.301E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.681E+00	2.196E+00	5.038E-01	2.470E-02
1.000E+02	9.910E+00	8.885E+00	8.733E+00	8.181E+00	7.019E+00	4.910E+00	2.247E+00	5.007E-01	3.694E-01
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.261E+00	5.019E+00	2.867E+00	2.314E+00	2.114E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.192E+01	8.372E+00	5.640E+00	4.820E+00	4.624E+00	4.383E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.098E-02	4.035E-02	3.815E-02	3.178E-02	2.434E-02	4.427E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.606E-01	3.633E-01	2.335E-01	9.668E-03
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.098E+00	4.502E-01	1.246E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.568E+00	1.855E+00	4.993E-01	2.390E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.682E+00	2.208E+00	5.742E-01	5.295E-02
1.000E+02	9.910E+00	8.885E+00	8.733E+00	8.181E+00	7.019E+00	4.923E+00	2.447E+00	1.350E+00	1.089E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.274E+00	5.186E+00	3.686E+00	3.445E+00	2.227E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.194E+01	8.540E+00	6.498E+00	6.009E+00	5.787E+00	5.530E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.098E-02	4.035E-02	3.817E-02	3.191E-02	2.464E-02	4.183E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.606E-01	3.637E-01	2.349E-01	1.078E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.419E+00	1.099E+00	4.620E-01	2.150E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.568E+00	1.861E+00	5.598E-01	7.801E-02
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.543E+00	3.684E+00	2.242E+00	7.796E-01	3.545E-01
1.000E+02	9.910E+00	8.885E+00	8.733E+00	8.181E+00	7.021E+00	4.962E+00	2.839E+00	2.285E+00	2.066E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.068E+01	8.316E+00	5.612E+00	4.792E+00	4.594E+00	4.353E+00
1.000E+04	1.631E+01	1.573E+01	1.444E+01	1.198E+01	8.976E+00	7.624E+00	7.176E+00	6.929E+00	6.663E+00

LOG S/S' = -1.0

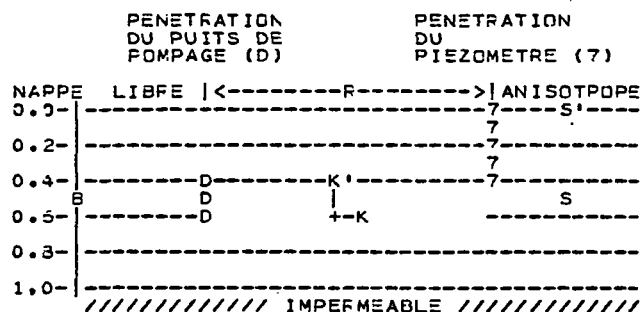
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E C U I T S				
1.000E-01	4.099E-02	4.098E-02	4.098E-02	4.098E-02	4.036E-02	3.822E-02	3.231E-02	2.551E-02	3.413E-03
3.162E-01	5.199E-01	5.199E-01	5.197E-01	5.179E-01	5.055E-01	4.608E-01	3.649E-01	2.392E-01	1.494E-02
1.000E+00	1.718E+00	1.718E+00	1.717E+00	1.703E+00	1.635E+00	1.420E+00	1.103E+00	4.575E-01	6.385E-02
3.162E+00	3.353E+00	3.353E+00	3.346E+00	3.296E+00	3.090E+00	2.570E+00	1.881E+00	7.318E-01	3.209E-01
1.000E+01	5.161E+00	5.158E+00	5.135E+00	5.002E+00	4.544E+00	3.689E+00	2.342E+00	1.274E+00	1.017E+00
1.000E+02	9.910E+00	8.885E+00	8.733E+00	8.181E+00	7.026E+00	5.077E+00	3.599E+00	3.354E+00	3.141E+00
1.000E+03	1.267E+01	1.251E+01	1.194E+01	1.069E+01	8.430E+00	6.411E+00	5.921E+00	5.699E+00	5.449E+00
1.000E+04	1.631E+01	1.573E+01	1.445E+01	1.209E+01	9.772E+00	8.760E+00	8.290E+00	8.030E+00	7.764E+00

FUIITS PENETRANT DE 0.4 A 0.6 ET PIEZOMETRE DE 0.3 A 0.4

TABLEAU D 7

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'F2/KB2	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0			1.0		
TT/R2S	R A B A T T E M E N T S									R E D U I T S																	
1.000E-01	7.857E-04	7.863E-04	7.955E-04	8.822E-04	1.609E-03	4.929E-03	1.459E-02	1.280E-02	1.601E-03																		
3.162E-01	9.967E-03	9.996E-03	1.029E-02	1.301E-02	3.142E-02	9.868E-02	2.287E-01	9.225E-02	3.286E-03																		
1.000E+00	3.296E-02	3.319E-02	3.548E-02	5.537E-02	1.579E-01	4.817E-01	6.619E-01	1.678E-01	3.449E-03																		
3.162E+00	6.439E-02	6.547E-02	7.581E-02	1.512E-01	4.595E-01	1.201E+00	9.592E-01	1.791E-01	3.956E-03																		
1.000E+01	9.937E-02	1.033E-01	1.386E-01	3.379E-01	1.026E+00	1.868E+00	1.082E+00	1.860E-01	5.806E-03																		
1.000E+02	1.757E-01	2.147E-01	4.416E-01	1.270E+00	2.543E+00	2.341E+00	1.133E+00	2.786E-01	6.342E-02																		
1.000E+03	2.879E-01	5.198E-01	1.380E+00	2.600E+00	3.022E+00	2.407E+00	1.491E+00	1.122E+00	1.056E+00																		
1.000E+04	5.936E-01	1.460E+00	2.913E+00	3.280E+00	3.090E+00	2.881E+00	3.252E+00	3.281E+00	3.182E+00																		

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0					-6.0					-5.0					-4.0					-3.0					-2.0					-1.0					0.0					1.0																																																																																																																																																					
TT/R2S	R										A										B										A										T										T										E										M										E										N										T										S										R										E										D										U										I										T										S									
1.000E-01	7.356E-04										7.864E-04										7.956E-04										8.825E-04										1.608E-03										4.932E-03										1.461E-02										1.281E-02										1.590E-03																																																																																																													
3.162E-01	9.967E-03										9.996E-03										1.029E-02										1.301E-02										3.142E-02										9.889E-02										2.288E-01										9.237E-02										3.358E-03																																																																																																													
1.000E+00	3.296E-02										3.319E-02										3.548E-02										5.537E-02										1.579E-01										4.817E-01										6.621E-01										1.690E-01										3.869E-03																																																																																																													
3.162E+00	6.439E-02										6.547E-02										7.581E-02										1.512E-01										4.596E-01										1.201E+00										9.609E-01										1.850E-01										5.701E-03																																																																																																													
1.000E+01	9.937E-02										1.033E-01										1.386E-01										3.379E-01										1.026E+00										1.868E+00										1.090E+00										2.071E-01										1.396E-02																																																																																																													
1.000E+02	1.757E-01										2.147E-01										4.416E-01										1.270E+00										2.543E+00										2.352E+00										1.223E+00										4.999E-01										3.324E-01																																																																																																													
1.000E+03	2.879E-01										5.198E-01										1.380E+00										2.601E+00										3.033E+00										2.530E+00										2.139E+00										2.124E+00										2.067E+00																																																																																																													
1.000E+04	5.936E-01										1.460E+00										2.914E+00										3.292E+00										3.217E+00										3.664E+00										4.509E+00										4.445E+00										4.322E+00																																																																																																													

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	7.856E-04	7.863E-04	7.957E-04	8.824E-04	1.610E-03	4.941E-03	1.466E-02	1.283E-02	1.556E-03	
3.162E-01	9.967E-03	9.996E-03	1.029E-02	1.301E-02	3.143E-02	9.892E-02	2.289E-01	9.277E-02	3.592E-03	
1.000E+00	3.296E-02	3.319E-02	3.548E-02	5.537E-02	1.580E-01	4.818E-01	6.631E-01	1.729E-01	5.376E-03	
3.162E+00	6.439E-02	6.547E-02	7.581E-02	1.512E-01	4.596E-01	1.201E+00	9.663E-01	2.037E-01	1.344E-02	
1.000E+01	9.937E-02	1.033E-01	1.386E-01	3.379E-01	1.027E+00	1.870E+00	1.114E+00	2.738E-01	6.175E-02	
1.000E+02	1.757E-01	2.147E-01	4.416E-01	1.270E+00	2.545E+00	2.357E+00	1.483E+00	1.095E+00	1.049E+00	
1.000E+03	2.879E-01	5.156E-01	1.381E+00	2.803E+00	3.073E+00	2.872E+00	3.243E+00	3.272E+00	3.173E+00	
1.000E+04	5.936E-01	1.460E+00	2.916E+00	3.328E+00	3.571E+00	4.867E+00	5.718E+00	5.600E+00	5.466E+00	

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0					-6.0					-5.0					-4.0					-3.0					-2.0					-1.0					0.0					1.0				
TT/R2S	R A B A T T E M E N T S										R E D U I T S																																		
1.000E-01	7.855E-04					7.864E-04					7.957E-04					8.822E-04					1.613E-03					4.969E-03					1.482E-02					1.238E-02					1.451E-03				
3.162E-01	9.967E-03					9.997E-03					1.029E-02					1.301E-02					3.144E-02					9.901E-02					2.295E-01					9.402E-02					4.412E-03				
1.000E+00	3.296E-02					3.319E-02					3.548E-02					5.537E-02					1.580E-01					4.821E-01					6.659E-01					1.852E-01					1.187E-02				
3.162E+00	6.439E-02					6.547E-02					7.581E-02					1.512E-01					4.597E-01					1.202E+00					9.831E-01					2.625E-01					5.787E-02				
1.000E+01	9.937E-02					1.033E-01					1.386E-01					3.379E-01					1.027E+00					1.875E+00					1.189E+00					4.818E-01					3.189E-01				
1.000E+02	1.757E-01					2.147E-01					4.416E-01					1.270E+00					2.555E+00					2.492E+00					2.113E+00					2.096E+00					2.040E+00				
1.000E+03	2.879E-01					5.198E-01					1.381E+00					2.808E+00					3.180E+00					3.636E+00					4.480E+00					4.415E+00					4.294E+00				
1.000E+04	5.936E-01					1.461E+00					2.921E+00					3.438E+00					4.351E+00					6.134E+00					6.890E+00					6.736E+00					6.597E+00				

LOG S/S' = -1.0

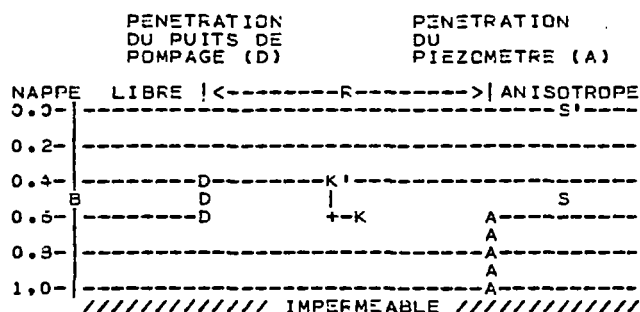
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-C1	7.857E-04	7.865E-04	7.953E-04	8.838E-04	1.622E-03	5.058E-03	1.532E-02	1.299E-02	1.117E-03	
3.162E-01	9.967E-03	9.997E-03	1.029E-02	1.301E-02	3.147E-02	9.929E-02	2.311E-01	9.782E-02	7.655E-03	
1.000E+00	3.296E-02	3.319E-02	3.548E-02	5.538E-02	1.581E-01	4.830E-01	6.748E-01	2.232E-01	4.680E-02	
3.162E+00	6.439E-02	6.547E-02	7.581E-02	1.512E-01	4.603E-01	1.205E+00	1.034E+00	2.413E-01	2.883E-01	
1.000E+01	9.937E-02	1.033E-01	1.385E-01	3.330E-01	1.028E+00	1.891E+00	1.397E+00	1.024E+00	9.797E-01	
1.000E+02	1.757E-01	2.147E-01	4.417E-01	1.271E+00	2.566E+00	2.779E+00	3.156E+00	3.182E+00	3.090E+00	
1.000E+03	2.879E-01	5.199E-01	1.382E+00	2.625E+00	3.477E+00	4.780E+00	5.629E+00	5.514E+00	5.388E+00	
1.000E+04	5.936E-01	1.462E+00	2.939E+00	3.737E+00	5.506E+00	7.290E+00	7.984E+00	7.835E+00	7.700E+00	

PUITS PENETRANT DE 0.4 A 0.6 ET PIEZOMETRE DE 0.6 A 1.0

TABLEAU D A

ABaque POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

CANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				F E D U I T S				
1.000E-01	7.862E-04	7.869E-04	7.960E-04	8.826E-04	1.609E-03	4.928E-03	1.461E-02	2.390E-02	4.974E-03
3.162E-01	9.974E-03	1.000E-02	1.029E-02	1.302E-02	3.142E-02	9.888E-02	2.451E-01	2.454E-01	1.012E-02
1.000E+00	3.298E-02	3.321E-02	3.550E-02	5.538E-02	1.579E-01	4.820E-01	9.309E-01	4.796E-01	1.048E-02
3.162E+00	6.443E-02	6.551E-02	7.585E-02	1.512E-01	4.595E-01	1.243E+00	1.738E+00	5.098E-01	1.153E-02
1.000E+01	9.943E-02	1.034E-01	1.387E-01	3.379E-01	1.027E+00	2.274E+00	2.109E+00	5.170E-01	1.511E-02
1.000E+02	1.758E-01	2.143E-01	4.416E-01	1.270E+00	2.967E+00	3.599E+00	2.161E+00	6.039E-01	9.336E-02
1.000E+03	2.890E-01	5.199E-01	1.381E+00	3.226E+00	4.297E+00	3.642E+00	2.330E+00	1.319E+00	1.083E+00
1.000E+04	5.937E-01	1.461E+00	3.340E+00	4.558E+00	4.351E+00	3.825E+00	3.390E+00	3.300E+00	3.187E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				F E D U I T S				
1.000E-01	7.861E-04	7.869E-04	7.960E-04	8.827E-04	1.609E-03	4.929E-03	1.462E-02	2.391E-02	4.967E-03
3.162E-01	9.974E-03	1.000E-02	1.029E-02	1.302E-02	3.142E-02	9.888E-02	2.451E-01	2.485E-01	1.029E-02
1.000E+00	3.298E-02	3.321E-02	3.550E-02	5.538E-02	1.579E-01	4.820E-01	9.309E-01	4.806E-01	1.136E-02
3.162E+00	6.443E-02	6.551E-02	7.585E-02	1.512E-01	4.595E-01	1.243E+00	1.738E+00	5.156E-01	1.492E-02
1.000E+01	9.943E-02	1.034E-01	1.387E-01	3.379E-01	1.027E+00	2.274E+00	2.111E+00	5.380E-01	2.869E-02
1.000E+02	1.758E-01	2.148E-01	4.416E-01	1.270E+00	2.967E+00	3.592E+00	2.200E+00	8.107E-01	3.755E-01
1.000E+03	2.890E-01	5.199E-01	1.381E+00	3.226E+00	4.300E+00	3.686E+00	2.667E+00	2.207E+00	2.078E+00
1.000E+04	5.937E-01	1.461E+00	3.340E+00	4.561E+00	4.395E+00	4.184E+00	4.413E+00	4.443E+00	4.326E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				F E D U I T S				
1.000E-01	7.361E-04	7.869E-04	7.960E-04	8.828E-04	1.609E-03	4.931E-03	1.463E-02	2.396E-02	4.944E-03
3.162E-01	9.974E-03	1.000E-02	1.029E-02	1.302E-02	3.142E-02	9.888E-02	2.451E-01	2.488E-01	1.082E-02
1.000E+00	3.298E-02	3.321E-02	3.550E-02	5.538E-02	1.579E-01	4.820E-01	9.311E-01	4.838E-01	1.433E-02
3.162E+00	6.443E-02	6.551E-02	7.585E-02	1.512E-01	4.596E-01	1.243E+00	1.739E+00	5.335E-01	2.786E-02
1.000E+01	9.943E-02	1.034E-01	1.387E-01	3.379E-01	1.027E+00	2.274E+00	2.119E+00	6.027E-01	9.121E-02
1.000E+02	1.758E-01	2.148E-01	4.416E-01	1.270E+00	2.967E+00	3.600E+00	2.320E+00	1.311E+00	1.075E+00
1.000E+03	2.890E-01	5.199E-01	1.381E+00	3.227E+00	4.308E+00	3.816E+00	3.372E+00	3.291E+00	3.178E+00
1.000E+04	5.937E-01	1.461E+00	3.341E+00	4.570E+00	4.526E+00	4.917E+00	5.549E+00	5.591E+00	5.469E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				F E D U I T S				
1.000E-01	7.862E-04	7.869E-04	7.961E-04	8.826E-04	1.610E-03	4.937E-03	1.468E-02	2.412E-02	4.874E-03
3.162E-01	9.974E-03	1.000E-02	1.029E-02	1.302E-02	3.143E-02	9.890E-02	2.453E-01	2.496E-01	1.256E-02
1.000E+00	3.298E-02	3.321E-02	3.550E-02	5.538E-02	1.579E-01	4.821E-01	9.317E-01	4.936E-01	2.536E-02
3.162E+00	6.443E-02	6.551E-02	7.585E-02	1.512E-01	4.596E-01	1.243E+00	1.742E+00	5.891E-01	8.623E-02
1.000E+01	9.943E-02	1.034E-01	1.387E-01	3.379E-01	1.027E+00	2.275E+00	2.142E+00	7.898E-01	3.610E-01
1.000E+02	1.758E-01	2.148E-01	4.417E-01	1.270E+00	2.968E+00	3.627E+00	2.639E+00	2.180E+00	2.051E+00
1.000E+03	2.890E-01	5.199E-01	1.381E+00	3.227E+00	4.337E+00	4.156E+00	4.384E+00	4.414E+00	4.298E+00
1.000E+04	5.937E-01	1.461E+00	3.341E+00	4.597E+00	4.874E+00	5.945E+00	6.700E+00	6.726E+00	6.600E+00

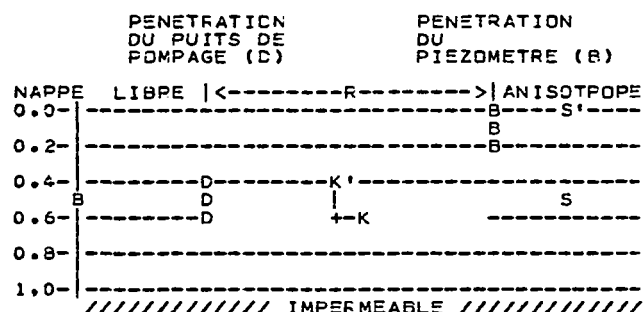
LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				F E D U I T S				
1.000E-01	7.852E-04	7.870E-04	7.962E-04	8.828E-04	1.611E-03	4.956E-03	1.485E-02	2.457E-02	4.633E-03
3.162E-01	9.974E-03	1.000E-02	1.029E-02	1.302E-02	3.143E-02	9.896E-02	2.456E-01	2.522E-01	1.850E-02
1.000E+00	3.298E-02	3.321E-02	3.551E-02	5.539E-02	1.580E-01	4.823E-01	9.333E-01	5.232E-01	7.195E-02
3.162E+00	6.443E-02	6.551E-02	7.585E-02	1.512E-01	4.596E-01	1.244E+00	1.752E+00	7.422E-01	3.283E-01
1.000E+01	9.943E-02	1.034E-01	1.387E-01	3.379E-01	1.027E+00	2.277E+00	2.212E+00	1.233E+00	1.006E+00
1.000E+02	1.759E-01	2.148E-01	4.417E-01	1.271E+00	2.970E+00	3.704E+00	3.287E+00	3.204E+00	3.095E+00
1.000E+03	2.890E-01	5.199E-01	1.381E+00	3.229E+00	4.413E+00	4.831E+00	5.462E+00	5.508E+00	5.391E+00
1.000E+04	5.937E-01	1.461E+00	3.344E+00	4.675E+00	5.546E+00	7.029E+00	7.789E+00	7.826E+00	7.703E+00

PUITS FENETRANT DE 0.4 A 0.6 ET PIEZOMETRE DE 0.3 A 0.2

TABLEAU D B

ABAUQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.576E-06	2.385E-06	2.519E-06	2.412E-06	1.452E-06	6.549E-07	1.881E-03	6.939E-03	8.324E-04
3.162E-01	3.247E-05	3.230E-05	3.210E-05	3.046E-05	6.343E-06	2.922E-04	8.664E-02	4.829E-02	1.721E-03
1.000E+00	1.069E-04	1.069E-04	1.063E-04	8.511E-05	6.159E-06	3.329E-02	3.181E-01	8.727E-02	1.892E-03
3.162E+00	2.083E-04	2.082E-04	2.037E-04	1.083E-04	6.853E-04	2.933E-01	4.740E-01	9.403E-02	2.437E-03
1.000E+01	3.208E-04	3.201E-04	2.876E-04	1.085E-04	4.591E-02	6.485E-01	5.385E-01	1.007E-01	4.396E-03
1.000E+02	5.532E-04	5.195E-04	3.143E-04	4.754E-02	7.101E-01	8.972E-01	5.931E-01	1.900E-01	6.188E-02
1.000E+03	7.547E-04	5.472E-04	4.790E-02	7.169E-01	9.619E-01	9.570E-01	9.363E-01	9.894E-01	1.035E+00
1.000E+04	7.843E-04	4.826E-02	7.164E-01	9.692E-01	1.024E+00	1.425E+00	2.668E+00	3.114E+00	3.134E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.602E-06	2.394E-06	2.500E-06	2.467E-06	8.101E-07	9.201E-08	1.881E-03	6.941E-03	8.381E-04
3.162E-01	3.246E-05	3.226E-05	3.208E-05	3.057E-05	5.234E-06	2.916E-04	8.664E-02	4.842E-02	1.824E-03
1.000E+00	1.069E-04	1.069E-04	1.063E-04	8.495E-05	4.755E-06	3.329E-02	3.183E-01	8.852E-02	2.369E-03
3.162E+00	2.083E-04	2.081E-04	2.035E-04	1.074E-04	6.838E-04	2.933E-01	4.756E-01	9.979E-02	4.310E-03
1.000E+01	3.207E-04	3.198E-04	2.871E-04	1.069E-04	4.591E-02	6.489E-01	5.460E-01	1.210E-01	1.279E-02
1.000E+02	5.529E-04	5.183E-04	3.130E-04	4.754E-02	7.105E-01	9.083E-01	6.717E-01	4.042E-01	3.256E-01
1.000E+03	7.531E-04	5.449E-04	4.790E-02	7.173E-01	9.735E-01	1.079E+00	1.573E+00	1.984E+00	2.030E+00
1.000E+04	7.785E-04	4.826E-02	7.168E-01	9.803E-01	1.150E+00	2.197E+00	3.887E+00	4.259E+00	4.267E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.593E-06	2.430E-06	2.447E-06	2.305E-06	2.118E-06	1.886E-08	1.881E-03	6.950E-03	8.559E-04
3.162E-01	3.250E-05	3.231E-05	3.197E-05	3.002E-05	5.927E-06	2.915E-04	8.666E-02	4.883E-02	2.156E-03
1.000E+00	1.069E-04	1.068E-04	1.061E-04	8.361E-05	6.565E-06	3.329E-02	3.189E-01	9.246E-02	4.047E-03
3.162E+00	2.083E-04	2.081E-04	2.029E-04	1.056E-04	6.859E-04	2.934E-01	4.807E-01	1.180E-01	1.234E-02
1.000E+01	3.207E-04	3.197E-04	2.859E-04	1.049E-04	4.591E-02	6.501E-01	5.698E-01	1.857E-01	6.033E-02
1.000E+02	5.526E-04	5.170E-04	3.115E-04	4.754E-02	7.118E-01	9.427E-01	6.278E-01	9.824E-01	1.028E+00
1.000E+03	7.518E-04	5.421E-04	4.790E-02	7.186E-01	1.009E+00	1.417E+00	2.653E+00	3.105E+00	3.125E+00
1.000E+04	7.748E-04	4.826E-02	7.201E-01	1.017E+00	1.499E+00	3.376E+00	5.068E+00	5.402E+00	5.407E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.671E-06	2.432E-06	2.470E-06	1.770E-06	1.205E-06	1.112E-07	1.881E-03	6.977E-03	9.114E-04
3.162E-01	3.251E-05	3.231E-05	3.195E-05	2.920E-05	5.894E-06	2.917E-04	8.671E-02	5.013E-02	3.273E-03
1.000E+00	1.069E-04	1.067E-04	1.057E-04	8.273E-05	5.347E-06	3.329E-02	3.208E-01	1.049E-01	1.097E-02
3.162E+00	2.083E-04	2.077E-04	2.017E-04	1.046E-04	6.842E-04	2.936E-01	4.966E-01	1.755E-01	5.675E-02
1.000E+01	3.206E-04	3.190E-04	2.840E-04	1.039E-04	4.591E-02	6.539E-01	6.425E-01	3.878E-01	3.127E-01
1.000E+02	5.516E-04	5.147E-04	3.099E-04	4.753E-02	7.158E-01	1.046E+00	1.547E+00	1.958E+00	2.004E+00
1.000E+03	7.486E-04	5.391E-04	4.790E-02	7.227E-01	1.117E+00	2.169E+00	3.859E+00	4.231E+00	4.240E+00
1.000E+04	7.726E-04	4.826E-02	7.242E-01	1.125E+00	2.268E+00	4.609E+00	6.221E+00	6.543E+00	6.537E+00

LOG S/S' = -1.0

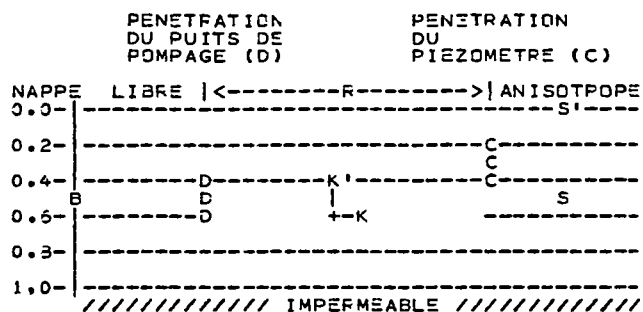
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	2.556E-06	2.356E-06	2.320E-06	2.870E-06	1.443E-06	0.0	1.679E-03	7.057E-03	1.051E-03
3.162E-01	3.246E-05	3.219E-05	3.149E-05	3.048E-05	6.258E-06	2.909E-04	8.687E-02	5.419E-02	7.347E-03
1.000E+00	1.069E-04	1.065E-04	1.046E-04	8.393E-05	5.513E-06	3.329E-02	3.269E-01	1.434E-01	4.651E-02
3.162E+00	2.083E-04	2.073E-04	2.022E-04	1.057E-04	6.838E-04	2.941E-01	5.446E-01	3.510E-01	2.836E-01
1.000E+01	3.205E-04	3.178E-04	2.823E-04	1.048E-04	4.590E-02	6.655E-01	8.433E-01	9.165E-01	9.615E-01
1.000E+02	5.510E-04	5.135E-04	3.064E-04	4.754E-02	7.284E-01	1.329E+00	2.569E+00	3.022E+00	3.045E+00
1.000E+03	7.493E-04	5.396E-04	4.789E-02	7.354E-01	1.410E+00	3.289E+00	4.981E+00	5.322E+00	5.332E+00
1.000E+04	7.745E-04	4.826E-02	7.368E-01	1.419E+00	3.398E+00	5.737E+00	7.304E+00	7.631E+00	7.640E+00

PUITS PENETRANT DE 0.4 A 0.6 ET PIEZOMETRE DE 0.2 A 0.4

TABEAU D C

AEQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

CANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.568E-03	1.570E-03	1.589E-03	1.762E-03	3.215E-03	9.856E-03	2.729E-02	1.864E-02	2.409E-03
3.162E-01	1.990E-02	1.996E-02	2.054E-02	2.599E-02	6.284E-02	1.975E-01	3.708E-01	1.362E-01	4.925E-03
1.000E+00	6.582E-02	6.628E-02	7.086E-02	1.106E-01	3.159E-01	9.301E-01	1.005E+00	2.494E-01	5.189E-03
3.162E+00	1.286E-01	1.307E-01	1.514E-01	3.022E-01	9.184E-01	2.108E+00	1.444E+00	2.640E-01	6.002E-03
1.000E+01	1.584E-01	2.064E-01	2.770E-01	6.757E-01	2.007E+00	3.087E+00	1.624E+00	2.710E-01	8.814E-03
1.000E+02	3.503E-01	4.288E-01	8.829E-01	2.492E+00	4.375E+00	3.782E+00	1.667E+00	3.619E-01	7.650E-02
1.000E+03	5.750E-01	1.039E+00	2.713E+00	4.883E+00	5.079E+00	3.831E+00	1.914E+00	1.110E+00	1.047E+00
1.000E+04	1.186E+00	2.873E+00	5.108E+00	5.588E+00	5.128E+00	4.121E+00	3.254E+00	3.134E+00	3.135E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.568E-03	1.570E-03	1.589E-03	1.762E-03	3.215E-03	9.856E-03	2.729E-02	1.864E-02	2.416E-03
3.162E-01	1.990E-02	1.996E-02	2.054E-02	2.599E-02	6.284E-02	1.975E-01	3.708E-01	1.362E-01	5.074E-03
1.000E+00	6.582E-02	6.628E-02	7.086E-02	1.106E-01	3.159E-01	9.301E-01	1.005E+00	2.494E-01	5.995E-03
3.162E+00	1.286E-01	1.307E-01	1.514E-01	3.022E-01	9.184E-01	2.108E+00	1.444E+00	2.698E-01	9.688E-03
1.000E+01	1.584E-01	2.064E-01	2.770E-01	6.757E-01	2.007E+00	3.087E+00	1.629E+00	2.918E-01	1.989E-02
1.000E+02	3.503E-01	4.288E-01	8.829E-01	2.492E+00	4.375E+00	3.788E+00	1.728E+00	5.695E-01	3.467E-01
1.000E+03	5.750E-01	1.039E+00	2.713E+00	4.884E+00	5.085E+00	3.903E+00	2.379E+00	2.036E+00	2.035E+00
1.000E+04	1.186E+00	2.873E+00	5.108E+00	5.594E+00	5.202E+00	4.645E+00	4.362E+00	4.266E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.568E-03	1.571E-03	1.589E-03	1.762E-03	3.215E-03	9.856E-03	2.729E-02	1.864E-02	2.438E-03
3.162E-01	1.990E-02	1.996E-02	2.054E-02	2.599E-02	6.284E-02	1.975E-01	3.708E-01	1.366E-01	5.552E-03
1.000E+00	6.582E-02	6.628E-02	7.086E-02	1.106E-01	3.159E-01	9.301E-01	1.005E+00	2.531E-01	8.295E-03
3.162E+00	1.286E-01	1.307E-01	1.514E-01	3.022E-01	9.184E-01	2.108E+00	1.447E+00	2.881E-01	1.928E-02
1.000E+01	1.584E-01	2.064E-01	2.770E-01	6.757E-01	2.007E+00	3.087E+00	1.644E+00	3.568E-01	7.472E-02
1.000E+02	3.503E-01	4.288E-01	8.829E-01	2.492E+00	4.376E+00	3.806E+00	1.906E+00	1.103E+00	1.040E+00
1.000E+03	5.750E-01	1.039E+00	2.713E+00	4.884E+00	5.103E+00	4.112E+00	3.246E+00	3.125E+00	3.127E+00
1.000E+04	1.186E+00	2.873E+00	5.108E+00	5.612E+00	5.415E+00	5.566E+00	5.506E+00	5.408E+00	5.407E+00

LOG S/S' = -1.5

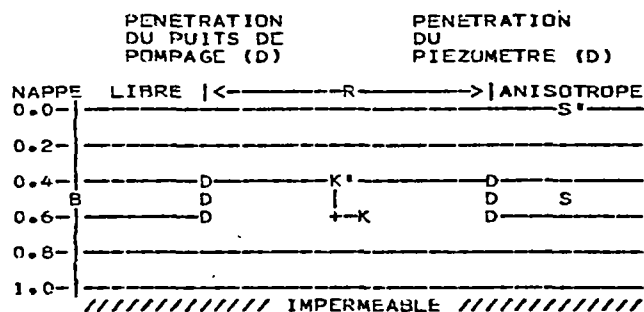
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.568E-03	1.570E-03	1.589E-03	1.762E-03	3.215E-03	9.856E-03	2.729E-02	1.865E-02	2.508E-03
3.162E-01	1.990E-02	1.996E-02	2.054E-02	2.599E-02	6.284E-02	1.975E-01	3.708E-01	1.376E-01	7.123E-03
1.000E+00	6.582E-02	6.628E-02	7.086E-02	1.106E-01	3.159E-01	9.301E-01	1.005E+00	2.644E-01	1.746E-02
3.162E+00	1.286E-01	1.307E-01	1.514E-01	3.022E-01	9.184E-01	2.108E+00	1.455E+00	3.446E-01	7.059E-02
1.000E+01	1.584E-01	2.064E-01	2.770E-01	6.757E-01	2.007E+00	3.088E+00	1.688E+00	5.512E-01	3.333E-01
1.000E+02	3.503E-01	4.288E-01	8.829E-01	2.492E+00	4.377E+00	3.861E+00	2.353E+00	2.010E+00	2.009E+00
1.000E+03	5.750E-01	1.039E+00	2.713E+00	4.885E+00	5.160E+00	4.617E+00	4.334E+00	4.240E+00	4.240E+00
1.000E+04	1.186E+00	2.873E+00	5.108E+00	5.669E+00	5.930E+00	6.676E+00	6.648E+00	6.548E+00	6.537E+00

LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	1.568E-03	1.571E-03	1.589E-03	1.762E-03	3.215E-03	9.856E-03	2.729E-02	1.869E-02	2.690E-03
3.162E-01	1.990E-02	1.996E-02	2.054E-02	2.599E-02	6.284E-02	1.975E-01	3.708E-01	1.406E-01	1.253E-02
1.000E+00	6.582E-02	6.628E-02	7.086E-02	1.106E-01	3.159E-01	9.301E-01	1.005E+00	2.991E-01	5.878E-02
3.162E+00	1.286E-01	1.307E-01	1.514E-01	3.022E-01	9.184E-01	2.108E+00	1.479E+00	5.098E-01	3.032E-01
1.000E+01	1.584E-01	2.064E-01	2.770E-01	6.757E-01	2.007E+00	3.091E+00	1.815E+00	1.034E+00	9.738E-01
1.000E+02	3.503E-01	4.288E-01	8.829E-01	2.492E+00	4.360E+00	4.015E+00	3.161E+00	3.042E+00	3.046E+00
1.000E+03	5.750E-01	1.039E+00	2.713E+00	4.883E+00	5.317E+00	5.479E+00	5.419E+00	5.327E+00	5.332E+00
1.000E+04	1.186E+00	2.873E+00	5.112E+00	5.827E+00	6.794E+00	7.767E+00	7.728E+00	7.635E+00	7.641E+00

PUITS A PENETRATION DE 0.4 A 0.6 ET PIEZOMETRE OUVERT DE 0.4 A 0.6
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU D D



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.599E-02	2.471E-02	3.725E-03	
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.991E-01	2.018E-01	7.623E-03	
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.430E+00	3.760E-01	7.961E-03	
3.162E+00	9.932E+00	9.927E+00	9.886E+00	9.585E+00	8.351E+00	5.216E+00	2.081E+00	3.992E-01	6.963E-03	
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.158E+01	6.496E+00	2.360E+00	4.062E-01	1.246E-02	
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.512E+01	7.539E+00	2.406E+00	4.950E-01	8.779E-02	
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.558E+01	1.618E+01	7.587E+00	2.593E+00	1.197E+00	1.057E+00	
1.000E+04	4.773E+01	4.426E+01	3.665E+01	2.664E+01	1.623E+01	7.795E+00	3.704E+00	3.148E+00	3.137E+00	

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.599E-02	2.471E-02	3.733E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.991E-01	2.018E-01	7.808E-03
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.430E+00	3.770E-01	8.845E-03
3.162E+00	9.932E+00	9.927E+00	9.886E+00	9.585E+00	8.351E+00	5.216E+00	2.081E+00	4.048E-01	1.230E-02
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.158E+01	6.496E+00	2.363E+00	4.265E-01	2.559E-02
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.512E+01	7.542E+00	2.451E+00	6.929E-01	3.624E-01
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.558E+01	1.618E+01	7.637E+00	2.960E+00	2.074E+00	2.038E+00
1.000E+04	4.773E+01	4.426E+01	3.665E+01	2.664E+01	1.628E+01	8.193E+00	4.732E+00	4.274E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.599E-02	2.472E-02	3.758E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.991E-01	2.020E-01	8.399E-03
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.430E+00	3.802E-01	1.181E-02
3.162E+00	9.932E+00	9.927E+00	9.886E+00	9.585E+00	8.351E+00	5.216E+00	2.082E+00	4.223E-01	2.487E-02
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.158E+01	6.496E+00	2.373E+00	4.893E-01	8.583E-02
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.512E+01	7.553E+00	2.585E+00	1.190E+00	1.050E+00
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.558E+01	1.619E+01	7.786E+00	3.695E+00	3.139E+00	3.128E+00
1.000E+04	4.773E+01	4.426E+01	3.665E+01	2.665E+01	1.643E+01	8.962E+00	5.848E+00	5.411E+00	5.407E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.179E-01	1.047E-01	6.599E-02	2.472E-02	3.836E-03
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.991E-01	2.027E-01	1.032E-02
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.430E+00	3.901E-01	2.268E-02
3.162E+00	9.932E+00	9.927E+00	9.886E+00	9.585E+00	8.351E+00	5.216E+00	2.086E+00	4.758E-01	8.129E-02
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.158E+01	6.497E+00	2.401E+00	6.732E-01	3.487E-01
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.512E+01	7.586E+00	2.933E+00	2.048E+00	2.012E+00
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.558E+01	1.623E+01	8.165E+00	4.704E+00	4.246E+00	4.241E+00
1.000E+04	4.773E+01	4.426E+01	3.665E+01	2.669E+01	1.681E+01	9.988E+00	6.982E+00	6.550E+00	6.537E+00

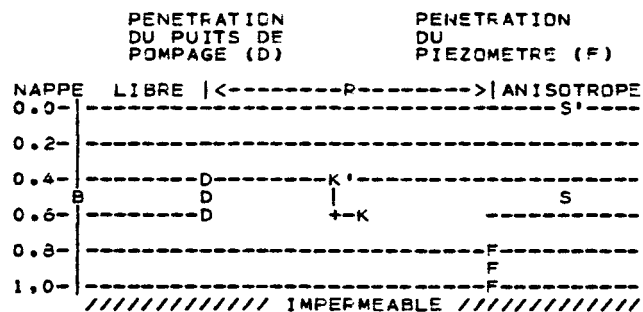
LOG S/S' = -1.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S		
1.000E-01	1.214E-01	1.214E-01	1.213E-01	1.210E-01	1.178E-01	1.047E-01	6.599E-02	2.473E-02
3.162E-01	1.540E+00	1.540E+00	1.539E+00	1.528E+00	1.454E+00	1.184E+00	5.991E-01	2.048E-01
1.000E+00	5.089E+00	5.088E+00	5.079E+00	5.000E+00	4.590E+00	3.293E+00	1.431E+00	4.200E-01
3.162E+00	9.932E+00	9.927E+00	9.886E+00	9.585E+00	8.351E+00	5.216E+00	2.098E+00	6.288E-01
1.000E+01	1.528E+01	1.527E+01	1.513E+01	1.433E+01	1.157E+01	6.497E+00	2.485E+00	1.120E+00
1.000E+02	2.638E+01	2.622E+01	2.532E+01	2.200E+01	1.512E+01	7.681E+00	3.610E+00	3.056E+00
1.000E+03	3.743E+01	3.650E+01	3.306E+01	2.558E+01	1.632E+01	8.876E+00	5.762E+00	5.331E+00
1.000E+04	4.773E+01	4.426E+01	3.665E+01	2.679E+01	1.752E+01	1.105E+01	8.060E+00	7.638E+00

PUITS PENETRANT DE 0.4 A 0.6 ET PIEZOMETRE DE 0.3 A 1.0

TABLEAU D F

ABaque POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELITSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	3.379E-06	3.239E-06	3.369E-06	3.255E-06	2.237E-06	1.567E-07	1.927E-03	2.285E-02	5.242E-03
3.162E-01	4.253E-05	4.251E-05	4.237E-05	4.080E-05	9.303E-06	2.914E-04	1.168E-01	2.564E-01	1.067E-02
1.000E+00	1.415E-04	1.411E-04	1.402E-04	1.129E-04	9.412E-06	3.389E-02	7.269E-01	4.993E-01	1.109E-02
3.162E+00	2.759E-04	2.755E-04	2.693E-04	1.433E-04	6.881E-04	3.720E-01	1.562E+00	5.309E-01	1.233E-02
1.000E+01	4.244E-04	4.232E-04	3.803E-04	1.435E-04	4.670E-02	1.276E+00	1.951E+00	5.375E-01	1.650E-02
1.000E+02	7.320E-04	6.870E-04	4.160E-04	4.838E-02	1.368E+00	2.643E+00	2.001E+00	6.220E-01	9.950E-02
1.000E+03	9.931E-04	7.236E-04	4.881E-02	1.377E+00	2.749E+00	2.695E+00	2.144E+00	1.274E+00	1.066E+00
1.000E+04	1.034E-03	4.925E-02	1.380E+00	2.761E+00	2.801E+00	2.846E+00	3.064E+00	3.154E+00	3.138E+00

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	3.344E-06	3.301E-06	3.397E-06	3.324E-06	2.254E-06	3.565E-07	1.926E-03	2.285E-02	5.251E-03
3.162E-01	4.256E-05	4.258E-05	4.243E-05	4.098E-05	9.163E-06	2.918E-04	1.168E-01	2.564E-01	1.089E-02
1.000E+00	1.414E-04	1.413E-04	1.403E-04	1.134E-04	9.267E-06	3.389E-02	7.269E-01	5.002E-01	1.216E-02
3.162E+00	2.756E-04	2.758E-04	2.697E-04	1.438E-04	6.880E-04	3.720E-01	1.562E+00	5.360E-01	1.631E-02
1.000E+01	4.242E-04	4.236E-04	3.812E-04	1.442E-04	4.670E-02	1.276E+00	1.953E+00	5.567E-01	3.174E-02
1.000E+02	7.318E-04	6.876E-04	4.173E-04	4.838E-02	1.368E+00	2.645E+00	2.035E+00	8.070E-01	3.783E-01
1.000E+03	9.990E-04	7.245E-04	4.881E-02	1.377E+00	2.751E+00	2.730E+00	2.432E+00	2.104E+00	2.042E+00
1.000E+04	1.036E-03	4.925E-02	1.380E+00	2.763E+00	2.837E+00	3.149E+00	4.019E+00	4.272E+00	4.268E+00

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	3.326E-06	3.221E-06	3.391E-06	3.314E-06	2.194E-06	2.552E-07	1.928E-03	2.285E-02	5.279E-03
3.162E-01	4.255E-05	4.251E-05	4.247E-05	4.096E-05	9.076E-06	2.915E-04	1.168E-01	2.565E-01	1.160E-02
1.000E+00	1.414E-04	1.412E-04	1.405E-04	1.136E-04	9.059E-06	3.389E-02	7.269E-01	5.027E-01	1.571E-02
3.162E+00	2.757E-04	2.757E-04	2.702E-04	1.440E-04	6.875E-04	3.720E-01	1.562E+00	5.521E-01	3.090E-02
1.000E+01	4.243E-04	4.234E-04	3.817E-04	1.442E-04	4.669E-02	1.276E+00	1.958E+00	6.158E-01	9.737E-02
1.000E+02	7.323E-04	6.883E-04	4.176E-04	4.838E-02	1.368E+00	2.651E+00	2.135E+00	1.266E+00	1.059E+00
1.000E+03	1.000E-03	7.249E-04	4.881E-02	1.377E+00	2.757E+00	2.837E+00	3.056E+00	3.145E+00	3.129E+00
1.000E+04	1.037E-03	4.926E-02	1.380E+00	2.769E+00	2.944E+00	3.794E+00	5.108E+00	5.406E+00	5.407E+00

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	3.432E-06	3.239E-06	3.337E-06	3.154E-06	2.325E-06	1.944E-07	1.928E-03	2.285E-02	5.366E-03
3.162E-01	4.266E-05	4.254E-05	4.262E-05	4.083E-05	9.190E-06	2.914E-04	1.168E-01	2.569E-01	1.388E-02
1.000E+00	1.415E-04	1.413E-04	1.409E-04	1.132E-04	9.319E-06	3.389E-02	7.269E-01	5.107E-01	2.835E-02
3.162E+00	2.759E-04	2.763E-04	2.705E-04	1.437E-04	6.880E-04	3.720E-01	1.564E+00	6.011E-01	9.242E-02
1.000E+01	4.246E-04	4.247E-04	3.824E-04	1.440E-04	4.670E-02	1.276E+00	1.975E+00	7.862E-01	3.643E-01
1.000E+02	7.336E-04	6.901E-04	4.182E-04	4.838E-02	1.366E+00	2.659E+00	2.405E+00	2.078E+00	2.016E+00
1.000E+03	1.002E-03	7.256E-04	4.882E-02	1.377E+00	2.778E+00	3.121E+00	3.991E+00	4.244E+00	4.241E+00
1.000E+04	1.039E-03	4.926E-02	1.380E+00	2.788E+00	3.237E+00	4.743E+00	6.234E+00	6.545E+00	6.537E+00

LOG S/S' = -1.0

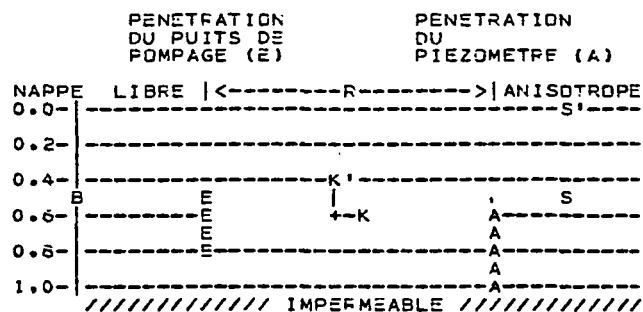
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	3.357E-06	3.320E-06	3.468E-06	3.187E-06	2.135E-06	3.354E-07	1.926E-03	2.285E-02	5.605E-03
3.162E-01	4.258E-05	4.272E-05	4.274E-05	4.078E-05	8.983E-06	2.914E-04	1.168E-01	2.578E-01	2.134E-02
1.000E+00	1.415E-04	1.416E-04	1.410E-04	1.133E-04	9.748E-06	3.389E-02	7.270E-01	5.347E-01	7.821E-02
3.162E+00	2.758E-04	2.768E-04	2.712E-04	1.438E-04	6.868E-04	3.720E-01	1.567E+00	7.390E-01	3.327E-01
1.000E+01	4.246E-04	4.252E-04	3.829E-04	1.438E-04	4.669E-02	1.276E+00	2.025E+00	1.195E+00	9.921E-01
1.000E+02	7.339E-04	6.903E-04	4.187E-04	4.833E-02	1.368E+00	2.724E+00	2.971E+00	3.062E+00	5.049E+00
1.000E+03	1.002E-03	7.261E-04	4.981E-02	1.378E+00	2.831E+00	3.708E+00	5.022E+00	5.326E+00	3.332E+00
1.000E+04	1.039E-03	4.926E-02	1.381E+00	2.843E+00	3.819E+00	5.779E+00	7.309E+00	7.632E+00	7.641E+00

PUITS A PENETRATION DE 0.5 A 0.8 ET PIEZOMETRE CUVERT DE 0.6 A 1.0

TABLEAU E A

ABAUQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.141E-02	3.891E-02	3.230E-02	5.942E-03
3.162E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.219E-01	4.674E-01	3.055E-01	1.212E-02
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.679E+00	1.442E+00	5.827E-01	1.254E-02
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.384E+00	3.155E+00	2.432E+00	6.184E-01
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.133E+00	4.633E+00	2.876E+00	6.251E-01
1.000E+02	9.027E+00	9.026E+00	9.027E+00	8.929E+00	8.929E+00	8.362E+00	6.236E+00	2.931E+00	7.104E-01
1.000E+03	1.286E+01	1.286E+01	1.276E+01	1.219E+01	9.983E+00	6.293E+00	3.073E+00	1.368E+00	1.079E+00
1.000E+04	1.670E+01	1.660E+01	1.603E+01	1.381E+01	1.004E+01	6.443E+00	3.994E+00	3.268E+00	3.163E+00

LOG S/S' = -2.5

LOG K'F2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.141E-02	3.891E-02	3.201E-02	5.943E-03	
3.162E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.219E-01	4.674E-01	3.055E-01	1.233E-02	
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.679E+00	1.442E+00	5.835E-01	1.361E-02	
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.384E+00	3.155E+00	2.432E+00	6.236E-01	
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.133E+00	4.633E+00	2.876E+00	6.445E-01	
1.000E+02	9.027E+00	9.026E+00	9.027E+00	8.929E+00	8.929E+00	8.362E+00	6.238E+00	2.965E+00	8.970E-01	
1.000E+03	1.286E+01	1.286E+01	1.276E+01	1.219E+01	9.985E+00	6.328E+00	3.360E+00	2.207E+00	2.062E+00	
1.000E+04	1.670E+01	1.660E+01	1.603E+01	1.381E+01	1.008E+01	6.745E+00	4.957E+00	4.395E+00	4.298E+00	

LOG S/S' = -2.0

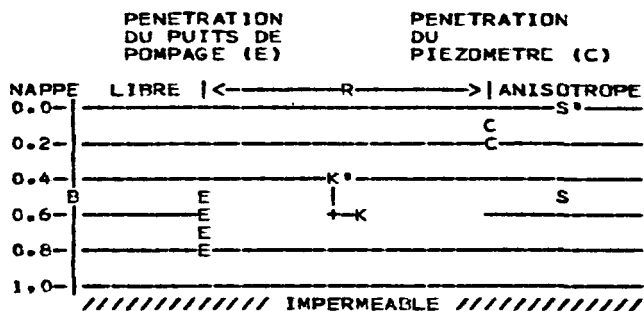
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.141E-02	3.892E-02	3.204E-02	5.948E-03	
3.162E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.219E-01	4.675E-01	3.057E-01	1.301E-02	
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.679E+00	1.442E+00	5.861E-01	1.715E-02	
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.364E+00	3.155E+00	2.433E+00	6.397E-01	
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.133E+00	4.633E+00	2.883E+00	7.040E-01	
1.000E+02	9.027E+00	9.026E+00	9.027E+00	8.929E+00	8.929E+00	8.362E+00	6.244E+00	3.064E+00	1.361E+00	
1.000E+03	1.286E+01	1.286E+01	1.276E+01	1.219E+01	9.991E+00	6.434E+00	3.985E+00	3.259E+00	3.154E+00	
1.000E+04	1.670E+01	1.660E+01	1.603E+01	1.382E+01	1.018E+01	7.390E+00	6.058E+00	5.535E+00	5.438E+00	

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.141E-02	3.894E-02	3.211E-02	5.963E-03	
3.162E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.219E-01	4.675E-01	3.062E-01	1.519E-02	
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.679E+00	1.442E+00	5.941E-01	2.991E-02	
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.384E+00	3.155E+00	2.434E+00	6.890E-01	
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.133E+00	4.633E+00	2.900E+00	8.758E-01	3.698E-01	
1.000E+02	9.027E+00	9.026E+00	9.027E+00	8.929E+00	8.362E+00	6.262E+00	3.333E+00	2.180E+00	2.035E+00	
1.000E+03	1.286E+01	1.286E+01	1.276E+01	1.219E+01	1.001E+01	6.717E+00	4.929E+00	4.367E+00	4.270E+00	
1.000E+04	1.670E+01	1.660E+01	1.603E+01	1.384E+01	1.047E+01	6.346E+00	7.193E+00	6.677E+00	6.569E+00	

LOG S/S' = -1.0

LGG K'R2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A E A T T E M E N T S					R E D U I T S				
1.000E-01	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.149E-02	4.142E-02	3.900E-02	3.233E-02	5.979E-03	
3.162E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.265E-01	5.219E-01	4.677E-01	3.076E-01	2.237E-02	
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.679E+00	1.443E+00	6.181E-01	7.992E-02	
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.384E+00	3.155E+00	2.439E+00	8.276E-01	3.374E-01	
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.133E+00	4.634E+00	2.950E+00	1.268E+00	1.003E+00	
1.000E+02	9.027E+00	9.026E+00	9.027E+00	8.929E+00	8.363E+00	6.316E+00	3.900E+00	3.174E+00	3.073E+00	
1.000E+03	1.286E+01	1.286E+01	1.276E+01	1.219E+01	1.006E+01	7.304E+00	5.972E+00	5.454E+00	5.362E+00	
1.000E+04	1.670E+01	1.660E+01	1.603E+01	1.389E+01	1.106E+01	9.396E+00	9.274E+00	7.765E+00	7.672E+00	



LOG S/S' = -3.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.138E-06	1.026E-06	8.143E-07	1.010E-06	1.183E-06	0.0	3.156E-04	8.101E-03	1.499E-03	
3.162E-01	1.232E-05	1.215E-05	1.173E-05	1.154E-05	3.376E-06	0.0	4.307E-02	7.688E-02	3.090E-03	
1.000E+00	3.936E-05	3.978E-05	3.943E-05	3.266E-05	4.448E-06	4.738E-03	2.728E-01	1.464E-01	3.367E-03	
3.162E+00	7.672E-05	7.671E-05	7.497E-05	4.220E-05	1.020E-05	1.252E-01	5.229E-01	1.569E-01	4.239E-03	
1.000E+01	1.186E-04	1.183E-04	1.066E-04	4.370E-05	6.304E-03	4.687E-01	6.350E-01	1.638E-01	7.229E-03	
1.000E+02	2.045E-04	1.926E-04	1.192E-04	6.526E-03	4.986E-01	8.740E-01	6.688E-01	2.528E-01	7.601E-02	
1.000E+03	2.791E-04	2.055E-04	6.620E-03	5.018E-01	9.086E-01	9.120E-01	8.887E-01	9.709E-01	1.027E+00	
1.000E+04	2.931E-04	6.728E-03	5.028E-01	9.124E-01	9.471E-01	1.165E+00	2.119E+00	2.927E+00	3.087E+00	

LOG S/S' = -2.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.155E-06	1.129E-06	8.222E-07	1.116E-06	6.278E-07	0.0	3.053E-04	8.092E-03	1.523E-03	
3.162E-01	1.231E-05	1.221E-05	1.181E-05	1.191E-05	2.269E-06	0.0	4.304E-02	7.696E-02	3.274E-03	
1.000E+00	3.934E-05	3.993E-05	3.972E-05	3.368E-05	2.086E-06	4.724E-03	2.728E-01	1.475E-01	4.148E-03	
3.162E+00	7.670E-05	7.696E-05	7.568E-05	4.375E-05	4.242E-06	1.252E-01	5.234E-01	1.627E-01	7.119E-03	
1.000E+01	1.185E-04	1.188E-04	1.084E-04	4.417E-05	6.287E-03	4.687E-01	6.389E-01	1.843E-01	1.880E-02	
1.000E+02	2.045E-04	1.943E-04	1.205E-04	6.512E-03	4.986E-01	8.787E-01	7.226E-01	4.538E-01	3.421E-01	
1.000E+03	2.813E-04	2.074E-04	6.606E-03	5.018E-01	9.134E-01	9.746E-01	1.308E+00	1.860E+00	1.998E+00	
1.000E+04	2.963E-04	6.720E-03	5.028E-01	9.172E-01	1.011E+00	1.630E+00	3.175E+00	4.040E+00	4.212E+00	

LOG S/S' = -2.0

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.152E-06	1.083E-06	8.756E-07	1.338E-06	0.0	0.0	2.711E-04	8.065E-03	1.596E-03	
3.162E-01	1.232E-05	1.225E-05	1.201E-05	1.241E-05	2.894E-08	0.0	4.293E-02	7.720E-02	3.862E-03	
1.000E+00	3.939E-05	3.996E-05	4.042E-05	3.439E-05	0.0	4.676E-03	2.726E-01	1.511E-01	6.779E-03	
3.162E+00	7.676E-05	7.724E-05	7.724E-05	4.338E-05	0.0	1.250E-01	5.250E-01	1.807E-01	1.825E-02	
1.000E+01	1.187E-04	1.195E-04	1.107E-04	4.032E-05	6.237E-03	4.685E-01	6.510E-01	2.479E-01	7.433E-02	
1.000E+02	2.054E-04	1.969E-04	1.184E-04	6.463E-03	4.984E-01	8.933E-01	8.804E-01	9.641E-01	1.021E+00	
1.000E+03	2.836E-04	2.070E-04	6.558E-03	5.016E-01	9.283E-01	1.156E+00	2.110E+00	2.918E+00	3.079E+00	
1.000E+04	2.980E-04	6.687E-03	5.026E-01	9.321E-01	1.194E+00	2.478E+00	4.286E+00	5.168E+00	5.348E+00	

LOG S/S' = -1.5

LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.190E-06	1.070E-06	1.006E-06	8.390E-07	0.0	0.0	1.639E-04	7.982E-03	1.824E-03	
3.162E-01	1.237E-05	1.228E-05	1.258E-05	1.141E-05	0.0	0.0	4.260E-02	7.797E-02	5.770E-03	
1.000E+00	3.945E-05	4.012E-05	4.150E-05	3.183E-05	0.0	4.526E-03	2.721E-01	1.624E-01	1.660E-02	
3.162E+00	7.688E-05	7.794E-05	7.886E-05	3.709E-05	0.0	1.246E-01	5.299E-01	2.363E-01	7.043E-02	
1.000E+01	1.189E-04	1.212E-04	1.112E-04	2.307E-05	6.081E-03	4.680E-01	6.882E-01	4.364E-01	3.293E-01	
1.000E+02	2.072E-04	1.989E-04	1.033E-04	6.305E-03	4.979E-01	9.379E-01	1.262E+00	1.835E+00	1.973E+00	
1.000E+03	2.867E-04	1.976E-04	6.396E-03	5.011E-01	9.737E-01	1.602E+00	3.148E+00	4.014E+00	4.186E+00	
1.000E+04	3.003E-04	6.571E-03	5.020E-01	9.777E-01	1.646E+00	3.534E+00	5.407E+00	6.302E+00	6.486E+00	

LOG S/S' = -1.0

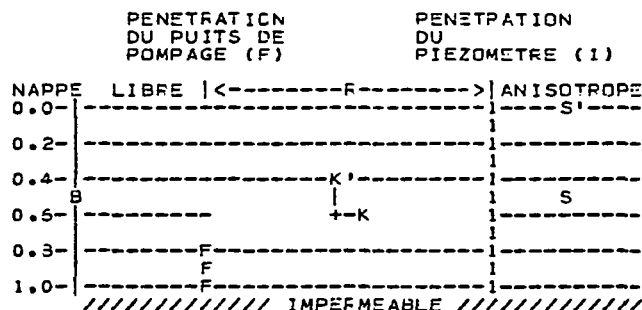
LOG K'R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S		
1.000E-01	1.162E-06	1.055E-06	1.274E-06	0.0	0.0	0.0	0.0	7.756E-03
3.162E-01	1.234E-05	1.242E-05	1.309E-05	8.878E-06	0.0	0.0	4.155E-02	8.046E-02
1.000E+00	3.953E-05	4.069E-05	4.220E-05	2.592E-05	0.0	4.049E-03	2.707E-01	1.969E-01
3.162E+00	7.714E-05	7.934E-05	7.843E-05	2.039E-05	0.0	1.231E-01	5.449E-01	3.972E-01
1.000E+01	1.197E-04	1.232E-04	1.068E-04	0.0	5.585E-03	4.664E-01	7.951E-01	8.997E-01
1.000E+02	2.101E-04	1.963E-04	5.287E-05	5.807E-03	4.962E-01	1.064E+00	2.027E+00	0.0
1.000E+03	2.892E-04	1.588E-04	5.883E-03	4.994E-01	1.102E+00	2.391E+00	4.201E+00	0.0
1.000E+04	3.010E-04	6.193E-03	5.002E-01	1.106E+00	2.440E+00	4.592E+00	6.476E+00	0.0

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE COMPLET

TABLEAU F 1

ABAGUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'F2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.490E-02	2.492E-02	2.409E-02	4.679E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	2.392E-01	9.520E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.031E+00	4.591E-01	9.686E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	1.807E+00	4.685E-01	1.015E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.118E+00	2.160E+00	4.973E-01	1.195E-02	
1.000E+02	5.417E+00	5.417E+00	5.416E+00	5.417E+00	5.398E+00	4.390E+00	2.219E+00	6.105E-01	7.573E-02	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.698E+00	6.674E+00	4.443E+00	2.474E+00	1.496E+00	1.133E+00	
1.000E+04	1.002E+01	1.002E+01	1.000E+01	8.976E+00	6.738E+00	4.728E+00	3.940E+00	3.732E+00	3.336E+00	

LOG S/S' = -2.5

LOG K'F2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.491E-02	2.494E-02	2.415E-02	4.617E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	2.394E-01	9.506E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.031E+00	4.606E-01	9.994E-03	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	1.808E+00	4.958E-01	1.177E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.119E+00	2.165E+00	5.234E-01	2.051E-02	
1.000E+02	5.417E+00	5.417E+00	5.416E+00	5.417E+00	5.398E+00	4.385E+00	2.281E+00	6.623E-01	3.675E-01	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.699E+00	6.680E+00	4.513E+00	2.963E+00	2.558E+00	2.188E+00	
1.000E+04	1.002E+01	1.002E+01	1.000E+01	8.982E+00	6.809E+00	5.265E+00	5.207E+00	5.000E+00	4.499E+00	

LOG S/S' = -2.0

LOG K'F2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.490E-02	2.492E-02	2.503E-02	2.436E-02	4.420E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.163E-01	2.402E-01	9.475E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.032E+00	4.655E-01	1.120E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	1.811E+00	5.189E-01	1.970E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.120E+00	2.179E+00	6.042E-01	7.350E-02	
1.000E+02	5.417E+00	5.417E+00	5.416E+00	5.417E+00	5.399E+00	4.403E+00	2.466E+00	1.487E+00	1.125E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.703E+00	6.697E+00	4.719E+00	3.931E+00	3.772E+00	3.327E+00	
1.000E+04	1.002E+01	1.002E+01	1.000E+01	8.999E+00	7.016E+00	6.278E+00	6.485E+00	6.190E+00	5.654E+00	

LOG S/S' = -1.5

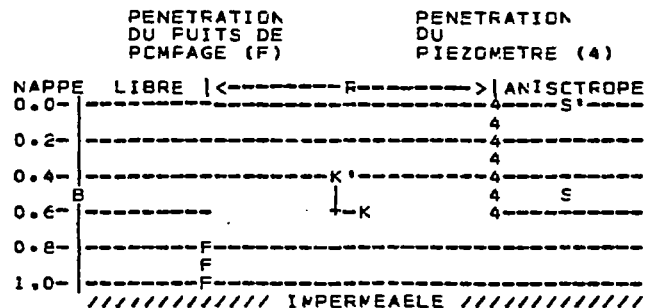
LOG K'F2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.491E-02	2.495E-02	2.529E-02	2.499E-02	3.803E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.161E-01	3.171E-01	2.426E-01	9.491E-03	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.045E+00	1.035E+00	4.805E-01	1.724E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.039E+00	1.821E+00	5.895E-01	6.833E-02	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.123E+00	2.225E+00	6.402E-01	3.514E-01	
1.000E+02	5.417E+00	5.417E+00	5.417E+00	5.417E+00	5.403E+00	4.456E+00	2.944E+00	2.528E+00	2.158E+00	
1.000E+03	7.717E+00	7.717E+00	7.717E+00	7.703E+00	6.751E+00	5.237E+00	5.178E+00	4.968E+00	4.467E+00	
1.000E+04	1.002E+01	1.002E+01	1.001E+01	9.053E+00	7.540E+00	7.549E+00	7.701E+00	7.346E+00	6.790E+00	

LOG S/S' = -1.0

LOG K'F2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.491E-02	2.490E-02	2.491E-02	2.490E-02	2.492E-02	2.505E-02	2.611E-02	2.686E-02	1.919E-03	
3.162E-01	3.159E-01	3.159E-01	3.159E-01	3.159E-01	3.160E-01	3.164E-01	3.197E-01	2.469E-01	1.055E-02	
1.000E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.044E+00	1.046E+00	1.043E+00	5.252E-01	5.358E-02	
3.162E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.038E+00	2.042E+00	1.652E+00	7.901E-01	3.153E-01	
1.000E+01	3.136E+00	3.136E+00	3.136E+00	3.137E+00	3.138E+00	3.133E+00	2.359E+00	1.406E+00	1.046E+00	
1.000E+02	5.417E+00	5.417E+00	5.417E+00	5.418E+00	5.413E+00	4.608E+00	3.944E+00	3.672E+00	3.234E+00	
1.000E+03	7.717E+00	7.717E+00	7.718E+00	7.713E+00	6.905E+00	6.191E+00	6.395E+00	6.094E+00	5.566E+00	
1.000E+04	1.002E+01	1.002E+01	1.002E+01	9.208E+00	8.498E+00	8.774E+00	8.842E+00	8.449E+00	7.889E+00	

FUITES A PENETRATION DE 0.8 A 1.0 ET PIEZOMETRE CUVERT DE 0.0 A 0.6
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE COULTON - STRELTSCOVA

TABLEAU F 4



LOG S/S' = -3.0

LOG K'R ₂ /K _{E2}	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ₂ S	R A E A T T E M E N T S				R E D U I T S				
1.000E-01	1.535E-06	1.234E-06	1.075E-06	1.420E-06	9.923E-07	1.018E-06	6.574E-04	1.236E-02	3.240E-03
3.162E-01	1.738E-05	1.706E-05	1.662E-05	1.626E-05	4.034E-06	1.002E-04	4.484E-02	1.550E-01	6.596E-03
1.000E+00	5.708E-05	5.691E-05	5.651E-05	4.547E-05	4.842E-06	1.141E-02	3.537E-01	3.061E-01	6.110E-03
3.162E+00	1.111E-04	1.109E-04	1.084E-04	5.650E-05	2.334E-04	1.392E-01	8.591E-01	3.270E-01	7.455E-03
1.000E+01	1.711E-04	1.707E-04	1.533E-04	5.548E-05	1.571E-02	5.917E-01	1.102E+00	3.350E-01	9.775E-03
1.000E+02	2.950E-04	2.770E-04	1.695E-04	1.628E-02	6.293E-01	1.426E+00	1.150E+00	4.387E-01	7.579E-02
1.000E+03	4.026E-04	2.936E-04	1.645E-02	6.334E-01	1.473E+00	1.477E+00	1.388E+00	1.256E+00	1.089E+00
1.000E+04	4.191E-04	1.661E-02	6.348E-01	1.478E+00	1.524E+00	1.743E+00	2.750E+00	3.404E+00	3.234E+00

LOG S/S' = -2.5

LOG K'R ₂ /K _{E2}	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ₂ S	R A E A T T E M E N T S				R E D U I T S				
1.000E-01	1.533E-06	1.296E-06	1.098E-06	1.375E-06	1.023E-06	2.909E-06	6.728E-04	1.239E-02	3.213E-03
3.162E-01	1.733E-05	1.717E-05	1.690E-05	1.621E-05	4.283E-06	1.061E-04	4.489E-02	1.551E-01	6.667E-03
1.000E+00	5.705E-05	5.700E-05	5.657E-05	4.553E-05	6.207E-06	1.143E-02	3.538E-01	3.075E-01	7.324E-03
3.162E+00	1.110E-04	1.109E-04	1.086E-04	5.662E-05	2.389E-04	1.393E-01	8.599E-01	3.337E-01	9.622E-03
1.000E+01	1.709E-04	1.707E-04	1.538E-04	6.100E-05	1.573E-02	5.919E-01	1.106E+00	3.589E-01	1.565E-02
1.000E+02	2.950E-04	2.772E-04	1.718E-04	1.630E-02	6.295E-01	1.431E+00	1.208E+00	6.701E-01	3.565E-01
1.000E+03	4.029E-04	2.942E-04	1.647E-02	6.336E-01	1.478E+00	1.543E+00	1.848E+00	2.245E+00	2.110E+00
1.000E+04	4.188E-04	1.662E-02	6.350E-01	1.483E+00	1.591E+00	2.245E+00	3.928E+00	4.579E+00	4.381E+00

LOG S/S' = -2.0

LOG K'R ₂ /K _{E2}	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ₂ S	R A E A T T E M E N T S				R E D U I T S				
1.000E-01	1.542E-06	1.271E-06	1.070E-06	1.514E-06	1.673E-06	8.684E-06	7.211E-04	1.249E-02	3.129E-03
3.162E-01	1.736E-05	1.710E-05	1.694E-05	1.649E-05	6.323E-06	1.244E-04	4.504E-02	1.556E-01	6.500E-03
1.000E+00	5.708E-05	5.692E-05	5.675E-05	4.605E-05	1.238E-05	1.148E-02	3.543E-01	3.118E-01	9.149E-03
3.162E+00	1.110E-04	1.109E-04	1.085E-04	6.045E-05	2.579E-04	1.394E-01	8.624E-01	3.575E-01	1.595E-02
1.000E+01	1.710E-04	1.707E-04	1.544E-04	6.668E-05	1.579E-02	5.925E-01	1.120E+00	4.329E-01	7.380E-02
1.000E+02	2.950E-04	2.773E-04	1.775E-04	1.630E-02	6.301E-01	1.447E+00	1.379E+00	1.248E+00	1.082E+00
1.000E+03	4.030E-04	2.954E-04	1.653E-02	6.342E-01	1.494E+00	1.735E+00	2.741E+00	3.394E+00	3.225E+00
1.000E+04	4.185E-04	1.665E-02	6.356E-01	1.499E+00	1.785E+00	2.186E+00	5.136E+00	5.743E+00	5.528E+00

LOG S/S' = -1.5

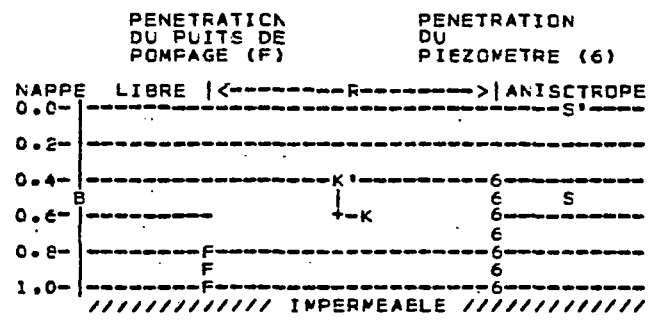
LOG K'R ₂ /K _{E2}	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ₂ S	R A E A T T E M E N T S				R E D U I T S				
1.000E-01	1.555E-06	1.269E-06	1.162E-06	1.458E-06	3.748E-06	2.701E-05	8.729E-04	1.279E-02	2.868E-03
3.162E-01	1.740E-05	1.715E-05	1.696E-05	1.671E-05	1.250E-05	1.827E-04	4.552E-02	1.572E-01	7.730E-03
1.000E+00	5.713E-05	5.709E-05	5.699E-05	4.745E-05	3.150E-05	1.167E-02	3.559E-01	3.250E-01	1.683E-02
3.162E+00	1.111E-04	1.112E-04	1.095E-04	6.604E-05	3.178E-04	1.400E-01	8.702E-01	4.191E-01	6.516E-02
1.000E+01	1.712E-04	1.712E-04	1.561E-04	6.510E-05	1.597E-02	5.945E-01	1.161E+00	6.495E-01	3.423E-01
1.000E+02	2.957E-04	2.780E-04	1.977E-04	1.655E-02	6.321E-01	1.495E+00	1.820E+00	2.217E+00	2.082E+00
1.000E+03	4.032E-04	3.034E-04	1.673E-02	6.362E-01	1.543E+00	2.217E+00	3.900E+00	4.549E+00	4.352E+00
1.000E+04	4.170E-04	1.673E-02	6.376E-01	1.548E+00	2.272E+00	4.266E+00	6.309E+00	6.885E+00	6.661E+00

LOG S/S' = -1.0

LOG K'R ₂ /K _{E2}	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ₂ S	R A E A T T E M E N T S				R E D U I T S				
1.000E-01	1.532E-06	1.313E-06	1.198E-06	2.185E-06	9.442E-06	8.553E-05	1.347E-03	1.365E-02	2.059E-03
3.162E-01	1.741E-05	1.717E-05	1.713E-05	1.673E-05	3.097E-05	3.671E-04	4.702E-02	1.619E-01	1.108E-02
1.000E+00	5.707E-05	5.709E-05	5.733E-05	5.365E-05	5.040E-05	1.225E-02	3.608E-01	3.648E-01	5.594E-02
3.162E+00	1.110E-04	1.113E-04	1.112E-04	6.525E-05	5.049E-04	1.419E-01	8.940E-01	6.029E-01	3.093E-01
1.000E+01	1.709E-04	1.713E-04	1.621E-04	1.451E-04	1.657E-02	6.005E-01	1.281E+00	1.172E+00	1.009E+00
1.000E+02	2.952E-04	2.809E-04	2.616E-04	1.714E-02	6.383E-01	1.633E+00	2.655E+00	3.302E+00	3.138E+00
1.000E+03	4.015E-04	3.328E-04	1.737E-02	6.424E-01	1.683E+00	3.098E+00	5.048E+00	5.655E+00	5.447E+00
1.000E+04	4.170E-04	1.701E-02	6.444E-01	1.688E+00	3.158E+00	5.521E+00	7.425E+00	7.986E+00	7.763E+00

PUITS A PENETRATION DE 0.8 A 1.0 ET PIEZOMETRE CUVERT DE 0.4 A 1.0
ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIERE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOLLTON - STRELTSOVA

TABEAU F 6



LOG S/S' = -3.0

LOG K'R₂/K_B2

TT/R2S	R	A	B	A	T	E	M	E	N	T	S	R	E	D	U	I	T	S		
1.000E-01	4.151E-02	4.151E-02	4.151E-02	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.151E-02	4.142E-02	3.532E-02	6.332E-03					
3.162E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.205E-01	3.290E-01	1.291E-02					
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.607E+00	6.252E-01	1.327E-02					
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.381E+00	2.673E+00	6.634E-01	1.434E-02					
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.031E+00	3.148E+00	6.738E-01	1.799E-02					
1.000E+02	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	8.823E+00	6.754E+00	3.208E+00	7.649E-01	9.675E-02				
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.057E+01	6.815E+00	3.368E+00	1.465E+00	1.105E+00				
1.000E+04	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.063E+01	6.984E+00	4.401E+00	3.503E+00	3.240E+00				

LOG S/S' = -2.5

LOG K'R₂/K_B2

TT/R2S	R	A	B	A	T	E	M	E	N	T	S	R	E	D	U	I	T	S		
1.000E-01	4.151E-02	4.151E-02	4.151E-02	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.151E-02	4.143E-02	3.535E-02	6.369E-03					
3.162E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.205E-01	3.291E-01	1.305E-02					
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.607E+00	6.252E-01	1.414E-02					
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.381E+00	2.673E+00	6.633E-01	1.777E-02					
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.031E+00	3.149E+00	6.923E-01	3.192E-02					
1.000E+02	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	8.823E+00	6.756E+00	3.245E+00	9.702E-01	3.882E-01				
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.057E+01	6.856E+00	3.685E+00	2.368E+00	2.120E+00				
1.000E+04	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.067E+01	7.324E+00	5.433E+00	4.664E+00	4.385E+00				

LOG S/S' = -2.0

LOG K'R₂/K_B2

TT/R2S	R	A	B	A	T	E	M	E	N	T	S	R	E	D	U	I	T	S		
1.000E-01	4.151E-02	4.151E-02	4.151E-02	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.151E-02	4.145E-02	3.546E-02	6.239E-03					
3.162E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.206E-01	3.295E-01	1.352E-02					
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.607E+00	6.254E-01	1.710E-02					
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.381E+00	2.674E+00	6.875E-01	3.099E-02					
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.031E+00	3.156E+00	7.583E-01	9.642E-02					
1.000E+02	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	8.824E+00	6.764E+00	3.357E+00	1.477E+00	1.101E+00				
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.058E+01	6.976E+00	4.382E+00	3.494E+00	3.231E+00				
1.000E+04	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.079E+01	8.041E+00	6.593E+00	5.824E+00	5.532E+00				

LOG S/S' = -1.5

LOG K'R₂/K_B2

TT/R2S	R	A	B	A	T	E	M	E	N	T	S	R	E	D	U	I	T	S		
1.000E-01	4.151E-02	4.151E-02	4.151E-02	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.152E-02	4.154E-02	3.578E-02	6.017E-03					
3.162E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.209E-01	3.307E-01	1.505E-02					
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.608E+00	6.394E-01	2.817E-02					
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.382E+00	2.677E+00	7.430E-01	9.100E-02					
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.032E+00	3.178E+00	9.484E-01	3.728E-01					
1.000E+02	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	8.825E+00	6.787E+00	3.661E+00	2.360E+00	2.052E+00				
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.060E+01	7.296E+00	5.405E+00	4.635E+00	4.356E+00				
1.000E+04	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.112E+01	9.080E+00	7.762E+00	6.966E+00	6.665E+00				

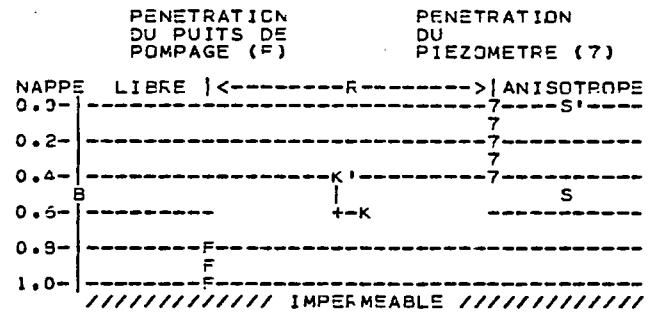
LOG S/S' = -1.0

LOG K'R₂/K_B2

TT/R2S	R	A	B	A	T	E	M	E	N	T	S	R	E	D	U	I	T	S		
1.000E-01	4.151E-02	4.151E-02	4.151E-02	4.151E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.150E-02	4.155E-02	4.180E-02	3.673E-02	5.304E-03					
3.162E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.266E-01	5.267E-01	5.217E-01	3.343E-01	2.041E-02					
1.000E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.740E+00	1.741E+00	1.611E+00	6.691E-01	7.248E-02					
3.162E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.396E+00	3.397E+00	2.687E+00	8.987E-01	3.384E-01					
1.000E+01	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.227E+00	5.035E+00	3.241E+00	1.461E+00	1.026E+00					
1.000E+02	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	9.028E+00	8.827E+00	6.856E+00	4.296E+00	3.465E+00	3.144E+00				
1.000E+03	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.286E+01	1.067E+01	7.955E+00	6.506E+00	5.738E+00	5.451E+00				
1.000E+04	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.670E+01	1.177E+01	1.019E+01	8.863E+00	8.068E+00	7.767E+00				

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE SOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	5.488E-07	3.040E-07	1.384E-07	2.496E-07	8.956E-08	4.917E-07	1.586E-05	7.105E-03	2.256E-03
3.162E-01	4.333E-06	4.058E-06	4.017E-06	3.374E-06	7.420E-07	1.620E-06	3.856E-03	1.042E-01	4.610E-03
1.000E+00	1.347E-05	1.379E-05	1.375E-05	1.032E-05	8.651E-07	1.566E-04	1.670E-01	2.094E-01	4.833E-03
3.162E+00	2.668E-05	2.623E-05	2.620E-05	1.335E-05	2.071E-06	2.278E-02	5.075E-01	2.245E-01	5.523E-03
1.000E+01	4.136E-05	4.082E-05	3.702E-05	1.314E-05	2.032E-04	2.492E-01	6.767E-01	2.323E-01	7.973E-03
1.000E+02	7.106E-05	6.606E-05	4.118E-05	2.201E-04	2.601E-01	8.167E-01	7.170E-01	3.325E-01	7.396E-02
1.000E+03	8.932E-05	7.143E-05	6.311E-05	2.612E-01	8.337E-01	8.606E-01	9.495E-01	1.123E+00	1.067E+00
1.000E+04	8.965E-05	6.944E-05	9.324E-05	8.357E-01	8.780E-01	1.121E+00	2.275E+00	3.214E+00	3.184E+00

LOG S/S' = -2.5

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	5.611E-07	2.972E-07	9.334E-08	2.072E-07	2.277E-07	1.616E-06	2.428E-05	7.120E-03	2.245E-03
3.162E-01	4.343E-06	4.050E-06	3.871E-06	3.270E-06	1.070E-06	5.048E-06	8.883E-03	1.043E-01	4.713E-03
1.000E+00	1.357E-05	1.387E-05	1.333E-05	1.016E-05	1.774E-06	1.671E-04	1.670E-01	2.107E-01	5.411E-03
3.162E+00	2.645E-05	2.628E-05	2.561E-05	1.330E-05	5.285E-06	2.281E-02	5.081E-01	2.310E-01	7.840E-03
1.000E+01	4.110E-05	4.079E-05	3.638E-05	1.391E-05	2.136E-04	2.494E-01	6.808E-01	2.554E-01	1.814E-02
1.000E+02	7.099E-05	6.645E-05	4.006E-05	2.305E-04	2.602E-01	8.215E-01	7.738E-01	5.562E-01	3.496E-01
1.000E+03	8.968E-05	7.218E-05	6.301E-05	2.613E-01	8.386E-01	9.246E-01	1.398E+00	2.084E+00	2.071E+00
1.000E+04	9.002E-05	7.006E-05	9.314E-05	8.407E-01	9.430E-01	1.611E+00	3.419E+00	4.369E+00	4.324E+00

LOG S/S' = -2.0

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	5.343E-07	3.255E-07	9.234E-08	3.044E-07	4.940E-07	4.849E-06	5.121E-05	7.167E-03	2.215E-03
3.162E-01	4.334E-06	4.131E-06	3.872E-06	3.505E-06	2.066E-06	1.536E-05	8.967E-03	1.047E-01	5.054E-03
1.000E+00	1.355E-05	1.390E-05	1.335E-05	1.055E-05	5.144E-06	1.999E-04	1.673E-01	2.148E-01	7.430E-03
3.162E+00	2.666E-05	2.658E-05	2.532E-05	1.437E-05	1.592E-05	2.292E-02	5.103E-01	2.514E-01	1.751E-02
1.000E+01	4.141E-05	4.135E-05	3.542E-05	1.721E-05	2.471E-04	2.497E-01	6.939E-01	3.269E-01	7.209E-02
1.000E+02	7.088E-05	6.673E-05	3.766E-05	2.643E-04	2.606E-01	8.367E-01	9.410E-01	1.116E+00	1.059E+00
1.000E+03	8.775E-05	7.215E-05	6.126E-05	2.617E-01	8.540E-01	1.112E+00	2.266E+00	3.205E+00	3.175E+00
1.000E+04	8.812E-05	7.003E-05	9.118E-05	8.561E-01	1.132E+00	2.525E+00	4.596E+00	5.521E+00	5.467E+00

LOG S/S' = -1.5

LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	4.959E-07	2.958E-07	1.092E-08	3.781E-07	1.766E-06	1.530E-05	1.354E-04	7.311E-03	2.122E-03
3.162E-01	4.245E-06	4.013E-06	3.582E-06	3.758E-06	5.661E-06	4.840E-05	9.234E-03	1.059E-01	6.208E-03
1.000E+00	1.328E-05	1.361E-05	1.333E-05	1.145E-05	1.606E-05	3.043E-04	1.683E-01	2.277E-01	1.561E-02
3.162E+00	2.615E-05	2.606E-05	2.541E-05	1.772E-05	4.990E-05	2.325E-02	5.169E-01	3.138E-01	6.777E-02
1.000E+01	4.081E-05	4.032E-05	3.569E-05	2.793E-05	3.539E-04	2.509E-01	7.339E-01	5.366E-01	3.356E-01
1.000E+02	7.026E-05	6.441E-05	3.882E-05	3.715E-04	2.618E-01	8.931E-01	1.371E+00	2.057E+00	2.044E+00
1.000E+03	8.903E-05	7.102E-05	6.265E-05	2.629E-01	9.011E-01	1.583E+00	3.390E+00	4.340E+00	4.295E+00
1.000E+04	8.936E-05	6.876E-05	9.258E-05	9.033E-01	1.608E+00	3.671E+00	5.760E+00	6.657E+00	6.598E+00

LOG S/S' = -1.0

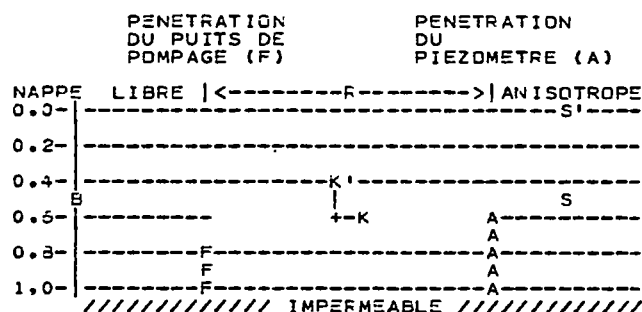
LOG K'R ² /KB ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R ² S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	5.721E-07	3.318E-07	1.092E-07	7.183E-07	4.850E-06	4.814E-05	3.979E-04	7.724E-03	1.820E-03
3.162E-01	4.357E-06	4.041E-06	3.741E-06	4.822E-06	1.594E-05	1.519E-04	1.006E-02	1.097E-01	1.048E-02
1.000E+00	1.342E-05	1.348E-05	1.323E-05	1.490E-05	4.911E-05	6.310E-04	1.712E-01	2.663E-01	5.544E-02
3.162E+00	2.633E-05	2.543E-05	2.501E-05	2.643E-05	1.532E-04	2.428E-02	5.371E-01	4.923E-01	3.042E-01
1.000E+01	4.077E-05	3.888E-05	3.586E-05	6.166E-05	6.875E-04	2.547E-01	8.496E-01	1.043E+00	9.900E-01
1.000E+02	6.957E-05	6.165E-05	3.952E-05	7.062E-04	2.656E-01	1.016E+00	2.181E+00	3.116E+00	3.092E+00
1.000E+03	8.681E-05	6.665E-05	6.287E-05	2.668E-01	1.036E+00	2.438E+00	4.509E+00	5.437E+00	5.389E+00
1.000E+04	8.714E-05	6.634E-05	9.303E-05	1.039E+00	2.468E+00	4.795E+00	6.853E+00	7.756E+00	7.701E+00

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE COUVERT DE 0.6 A 1.0

TABLEAU F A

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -3.0

LOG K ₁ F ₂ /KE ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ₂ S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	6.227E-02	6.225E-02	6.225E-02	6.226E-02	6.226E-02	6.225E-02	6.226E-02	6.117E-02	4.156E-02	6.905E-03
3.162E-01	7.898E-01	7.898E-01	7.898E-01	7.898E-01	7.898E-01	7.898E-01	7.897E-01	7.224E-01	3.652E-01	1.409E-02
1.000E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.594E+00	2.046E+00	6.880E-01	1.453E-02
3.162E+00	5.094E+00	5.094E+00	5.094E+00	5.094E+00	5.095E+00	5.094E+00	4.886E+00	3.228E+00	7.292E-01	1.582E-02
1.000E+01	7.841E+00	7.841E+00	7.841E+00	7.841E+00	7.841E+00	7.818E+00	6.908E+00	3.745E+00	7.360E-01	2.017E-02
1.000E+02	1.354E+01	1.354E+01	1.354E+01	1.352E+01	1.352E+01	1.255E+01	8.809E+00	3.806E+00	8.213E-01	1.065E-01
1.000E+03	1.929E+01	1.929E+01	1.927E+01	1.830E+01	1.447E+01	8.671E+00	3.939E+00	1.477E+00	1.093E+00	
1.000E+04	2.505E+01	2.503E+01	2.405E+01	2.022E+01	1.454E+01	9.012E+00	4.832E+00	3.397E+00	3.190E+00	

LOG S/S' = -2.5

LOG K ₁ R ₂ /K ₂ B ₂	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0		1.0		
TT/R ₂ S	R		A	B		A	T		T	E	M		E	N	T		S	F		E	D	U		I	T	S
1.000E-01	6.227E-02			6.225E-02			6.226E-02				6.226E-02				6.225E-02			6.226E-02			6.117E-02			4.157E-02		6.900E-03
3.162E-01	7.898E-01			7.898E-01			7.899E-01				7.899E-01				7.899E-01			7.897E-01			7.224E-01			3.653E-01		1.429E-02
1.000E+00	2.611E+00			2.611E+00			2.611E+00				2.611E+00				2.611E+00			2.594E+00			2.046E+00			6.888E-01		1.562E-02
3.162E+00	5.094E+00			5.094E+00			5.094E+00				5.095E+00				5.094E+00			4.886E+00			3.228E+00			7.344E-01		1.994E-02
1.000E+01	7.841E+00			7.841E+00			7.841E+00				7.841E+00				7.818E+00			6.908E+00			3.746E+00			7.553E-01		3.606E-02
1.000E+02	1.354E+01			1.354E+01			1.354E+01				1.352E+01				1.255E+01			8.810E+00			3.837E+00			1.007E+00		3.927E-01
1.000E+03	1.929E+01			1.929E+01			1.927E+01				1.830E+01				1.447E+01			8.904E+00			4.214E+00			2.318E+00		2.083E+00
1.000E+04	2.505E+01			2.503E+01			2.405E+01				2.022E+01				1.457E+01			9.298E+00			5.792E+00			4.522E+00		4.327E+00

LOG S/S' = -2.0

LOG K ₁ R ₂ /K ₂ B ₂	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ₂ S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	6.227E-02	6.225E-02	6.226E-02	6.226E-02	6.225E-02	6.226E-02	6.118E-02	4.162E-02	6.882E-03	
3.162E-01	7.398E-01	7.858E-01	7.898E-01	7.898E-01	7.898E-01	7.897E-01	7.224E-01	3.655E-01	1.495E-02	
1.000E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.594E+00	2.047E+00	6.913E-01	1.924E-02	
3.162E+00	5.094E+00	5.094E+00	5.094E+00	5.095E+00	5.094E+00	4.886E+00	3.228E+00	7.504E-01	3.510E-02	
1.000E+01	7.841E+00	7.841E+00	7.841E+00	7.841E+00	7.818E+00	6.908E+00	3.751E+00	8.147E-01	1.042E-01	
1.000E+02	1.354E+01	1.354E+01	1.354E+01	1.352E+01	1.255E+01	8.816E+00	3.930E+00	1.469E+00	1.086E+00	
1.000E+03	1.929E+01	1.929E+01	1.927E+01	1.830E+01	1.448E+01	9.003E+00	4.823E+00	3.378E+00	3.181E+00	
1.000E+04	2.505E+01	2.503E+01	2.405E+01	2.023E+01	1.467E+01	9.925E+00	6.902E+00	5.658E+00	5.470E+00	

LOG S/S' = -1.5

LOG K ₁ R ₂ /K ₂ B ₂	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0		1.0		
TT/R ₂ S	R		A	B		A	T	T	E	M	E	N	T	S	R		E	D	U	I	T	S				
1.000E-01	6.227E-02			6.225E-02						6.226E-02				6.226E-02	6.225E-02			6.226E-02			6.122E-02	4.177E-02		6.825E-03		
3.162E-01	7.898E-01			7.858E-01						7.898E-01				7.698E-01	7.898E-01			7.897E-01			7.225E-01	3.661E-01		1.709E-02		
1.000E+00	2.611E+00			2.611E+00						2.611E+00				2.611E+00	2.611E+00			2.594E+00			2.047E+00	6.990E-01		3.218E-02		
3.162E+00	5.094E+00			5.094E+00						5.094E+00				5.095E+00	5.094E+00			4.886E+00			3.230E+00	7.992E-01		9.878E-02		
1.000E+01	7.841E+00			7.841E+00						7.841E+00				7.841E+00	7.818E+00			6.909E+00			3.766E+00	9.857E-01		3.778E-01		
1.000E+02	1.354E+01			1.354E+01						1.354E+01				1.352E+01	1.255E+01			8.832E+00			4.187E+00	2.291E+00		2.056E+00		
1.000E+03	1.929E+01			1.929E+01						1.927E+01				1.830E+01	1.450E+01			9.270E+00			5.764E+00	4.493E+00		4.299E+00		
1.000E+04	2.505E+01			2.503E+01						2.405E+01				2.024E+01	1.495E+01			1.088E+01			8.045E+00	6.802E+00		6.601E+00		

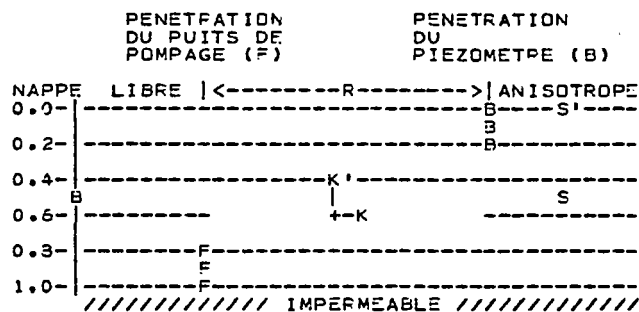
LOG S/S' = -1.0

LOG K ₁ R ₂ /K ₂	-7.0		-6.0		-5.0		-4.0		-3.0		-2.0		-1.0		0.0		1.0	
TT/R ₂ S	R E D U I T S																	
1.000E-01	6.227E-02	6.225E-02	6.225E-02	6.226E-02	6.225E-02	6.224E-02	6.227E-02	6.133E-02	4.223E-02	6.619E-03								
3.162E-01	7.398E-01	7.898E-01	7.898E-01	7.898E-01	7.898E-01	7.898E-01	7.229E-01	3.680E-01	2.413E-02									
1.000E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.611E+00	2.594E+00	2.048E+00	7.222E-01	8.320E-02								
3.162E+00	5.094E+00	5.094E+00	5.094E+00	5.094E+00	5.095E+00	5.094E+00	4.886E+00	3.235E+00	9.352E-01	3.444E-01								
1.000E+01	7.841E+00	7.841E+00	7.841E+00	7.841E+00	7.841E+00	7.818E+00	6.910E+00	3.811E+00	1.395E+00	1.016E+00								
1.000E+02	1.354E+01	1.354E+01	1.354E+01	1.354E+01	1.352E+01	1.255E+01	8.879E+00	4.738E+00	3.292E+00	3.097E+00								
1.000E+03	1.929E+01	1.929E+01	1.927E+01	1.830E+01	1.454E+01	9.839E+00	6.816E+00	5.585E+00	5.392E+00									
1.000E+04	2.505E+01	2.503E+01	2.406E+01	2.029E+01	1.551E+01	1.194E+01	9.131E+00	7.902E+00	7.704E+00									

TABLEAU F B

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE CUVERT DE 0.0 A 0.2
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELITSOVA

TABLEAU F B


$$LCG \ S/S' = -3.0$$

LOG K ¹ R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S				R E D U I T S				
1.000E-01	5.412E-09	2.669E-07	6.847E-06	1.226E-07	2.361E-07	0.0	2.161E-08	3.122E-03	1.164E-03
3.162E-01	1.296E-06	1.387E-06	1.625E-06	1.619E-06	7.117E-07	1.472E-07	1.310E-03	5.214E-02	2.403E-03
1.000E+00	4.762E-06	4.678E-06	5.137E-06	4.255E-06	1.060E-06	1.182E-06	6.463E-02	1.063E-01	2.628E-03
3.162E+00	9.524E-06	1.026E-05	9.918E-06	5.871E-06	1.315E-06	3.097E-03	2.353E-01	1.152E-01	3.342E-03
1.000E+01	1.474E-05	1.526E-05	1.419E-05	6.577E-06	2.751E-06	9.216E-02	3.229E-01	1.227E-01	5.858E-03
1.000E+02	2.565E-05	2.493E-05	1.614E-05	8.082E-06	9.559E-02	3.792E-02	3.554E-01	2.199E-01	7.127E-02
1.000E+03	3.336E-05	2.513E-05	1.604E-05	9.594E-02	3.857E-01	4.150E-01	5.838E-01	9.568E-01	1.044E+00
1.000E+04	3.346E-05	2.512E-05	1.608E-05	3.865E-01	4.219E-01	6.709E-01	1.885E+00	3.028E+00	3.135E+00

LCC S/S' = -2.5

LOG K ¹ R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	0.0	1.935E-07	3.730E-08	1.646E-07	7.690E-09	1.628E-07	2.095E-07	3.122E-03	1.172E-03
3.162E-01	1.299E-06	1.251E-06	1.551E-06	1.681E-06	3.063E-07	3.647E-07	1.310E-03	5.224E-02	2.538E-03
1.000E+00	4.817E-06	4.717E-06	5.089E-06	4.456E-06	6.439E-07	1.366E-06	6.469E-02	1.077E-01	3.254E-03
3.162E+00	9.440E-06	9.850E-06	1.012E-05	5.921E-06	1.096E-06	3.097E-03	2.358E-01	1.215E-01	5.748E-03
1.000E+01	1.464E-05	1.515E-05	1.450E-05	6.600E-06	2.364E-06	9.219E-02	3.268E-01	1.452E-01	1.614E-02
1.000E+02	2.585E-05	2.572E-05	1.600E-05	8.030E-06	9.561E-02	3.839E-01	4.109E-01	4.373E-01	3.414E-01
1.000E+03	3.344E-05	2.772E-05	1.739E-05	9.597E-02	3.905E-01	4.781E-01	1.022E+00	1.924E+00	2.033E+00
1.000E+04	3.354E-05	2.771E-05	1.824E-05	3.913E-01	4.858E-01	1.151E+00	2.993E+00	4.164E+00	4.267E+00

LCG S/S' = -2.0

LOG K ¹ R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0											
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	D	U	I	T	S	
1.000E-C1	3.047E-09			2.317E-07				3.862E-06			1.793E-07		3.913E-07		0.0			1.832E-07	3.125E-03	1.195E-03
3.162E-01	1.329E-06			1.353E-06				1.669E-06			1.719E-06		9.824E-07		1.546E-07			1.310E-03	5.256E-02	2.973E-03
1.000E+00	4.922E-06			4.815E-06				5.314E-06			4.308E-06		1.572E-06		1.131E-06			6.475E-02	1.117E-01	5.411E-03
3.162E+00	9.810E-06			1.010E-05				1.044E-05			5.671E-06		2.106E-06		3.097E-03			2.375E-01	1.414E-01	1.558E-02
1.000E+C1	1.510E-05			1.540E-05				1.511E-05			6.468E-06		3.449E-06		9.227E-02			3.395E-01	2.147E-01	6.556E-02
1.000E+02	2.637E-05			2.489E-05				1.784E-05			8.213E-06		9.570E-02		3.986E-01			5.749E-01	9.816E-01	1.037E+00
1.000E+03	3.479E-05			2.421E-05				2.067E-05			9.636E-02		4.054E-01		6.619E-01			1.870E+00	3.019E+00	3.126E+00
1.000E+04	3.439E-05			2.419E-05				2.150E-05			4.063E-01		6.718E-01		2.044E+00			4.143E+00	5.305E+00	5.407E+00

$$\text{LOG } S/S' = -1.5$$

LOG K'R2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	D	U	I	T	S
1.000E-01	0.0			2.367E-07	1.048E-07	0.0		3.253E-07	0.0		1.431E-07	3.130E-03	1.268E-03						
3.162E-01	1.184E-06			1.285E-06	1.600E-06	1.247E-06		7.942E-07	0.0		1.310E-03	5.356E-02	4.416E-03						
1.000E+00	4.642E-06			4.637E-06	5.674E-06	3.917E-06		1.310E-06	8.595E-07		6.493E-02	1.244E-01	1.393E-02						
3.162E+00	9.195E-06			1.024E-05	1.118E-05	5.756E-06		1.718E-06	3.097E-03		2.433E-01	2.025E-01	6.557E-02						
1.000E+01	1.423E-05			1.581E-05	1.544E-05	6.694E-06		2.929E-06	9.254E-02		3.783E-01	4.159E-01	3.281E-01						
1.000E+02	2.690E-05			2.643E-05	1.752E-05	8.204E-06		9.598E-02	4.436E-01		9.957E-01	1.898E+00	2.008E+00						
1.000E+03	3.684E-05			2.796E-05	1.913E-05	9.634E-02		4.511E-01	1.123E+00		2.965E+00	4.137E+00	4.240E+00						
1.000E+04	3.686E-05			2.805E-05	2.020E-05	9.520E-02		1.137E+00	3.160E+00		5.298E+00	6.445E+00	6.537E+00						

$$\text{LOG } S/S' = -1.0$$

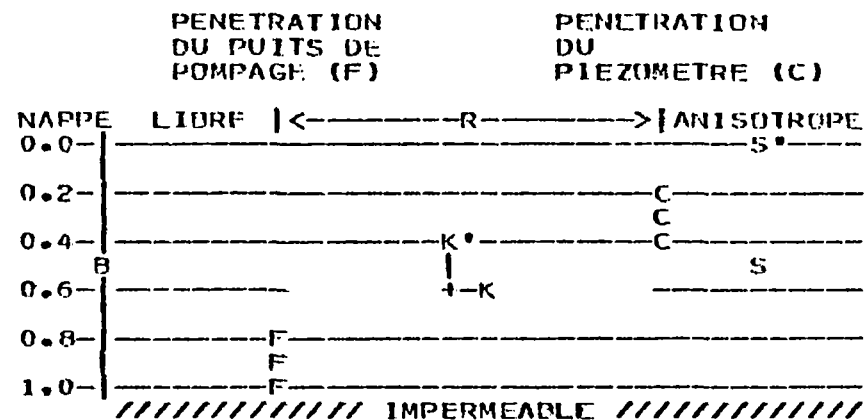
LOG K'R2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0										
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	D	U	I	T	S
1.000E-01	6.820E-03	3.209E-07	1.602E-07	2.978E-07	1.695E-07	0.0	0.0	3.145E-03	1.463E-03										
3.162E-01	1.397E-06	1.496E-06	1.666E-06	1.906E-06	5.652E-07	0.0	1.303E-03	5.654E-02	9.509E-02										
1.000E+00	5.018E-06	5.147E-06	5.253E-06	6.719E-06	3.672E-07	0.0	6.546E-02	1.629E-01	5.419E-03										
3.162E+00	9.784E-06	1.055E-05	1.033E-05	6.439E-06	6.424E-07	3.091E-03	2.595E-01	3.775E-01	2.982E-01										
1.000E+01	1.465E-05	1.602E-05	1.426E-05	7.290E-06	0.0	9.335E-02	4.905E-01	9.134E-01	9.708E-01										
1.000E+02	2.524E-05	2.563E-05	1.571E-05	6.808E-06	9.682E-02	5.723E-01	1.786E+00	2.935E+00	3.046E+00										
1.000E+03	3.003E-05	2.777E-05	1.611E-05	9.719E-02	5.817E-01	1.957E+00	4.057E+00	5.225E+00	5.332E+00										
1.000E+04	3.053E-05	2.785E-05	1.697E-05	3.828E-01	1.976E+00	4.257E+00	6.369E+00	7.533E+00	7.640E+00										

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE OUVERT DE 0.2 A 0.4

TABLEAU F C

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S* = -2.0

LOG K*R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

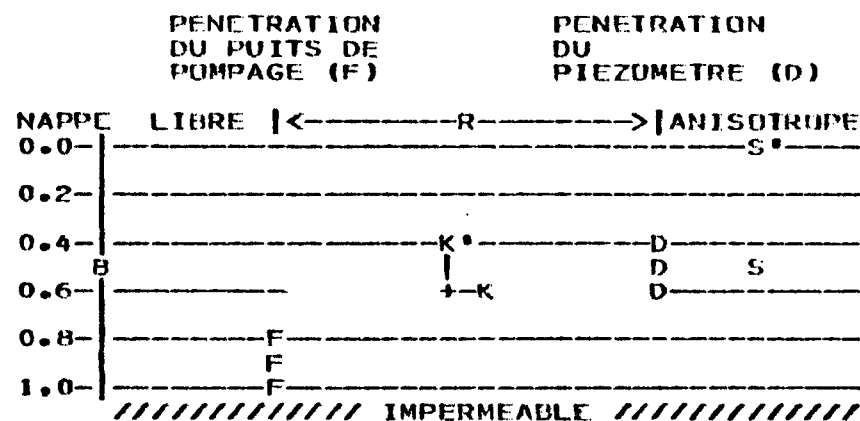
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	8.309E-07	6.636E-07	1.664E-07	6.481E-07	0.0	0.0	2.399E-05	1.108E-02	3.398E-03	
1.000E+00	2.146E-05	2.221E-05	2.200E-05	1.777E-05	2.161E-07	3.026E-04	2.692E-01	3.166E-01	1.102E-02	
1.000E+01	6.428E-05	6.607E-05	5.894E-05	2.203E-05	3.948E-04	4.062E-01	1.041E+00	4.253E-01	8.522E-02	
1.000E+02	1.106E-04	1.097E-04	6.202E-05	4.272E-04	4.245E-01	1.265E+00	1.237E+00	1.126E+00	1.050E+00	
1.000E+03	1.393E-04	1.182E-04	1.084E-04	4.264E-01	1.293E+00	1.477E+00	2.303E+00	3.071E+00	3.128E+00	
1.000E+04	1.390E-04	1.177E-04	1.648E-04	1.296E+00	1.506E+00	2.596E+00	4.446E+00	5.343E+00	5.407E+00	

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE OUVERT DE 0.4 A 0.6

TABLEAU F D

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



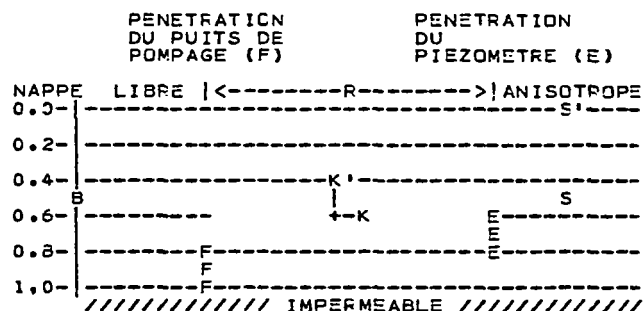
LOG S/S' = -2.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	3.392E-06	3.212E-06	3.261E-06	3.189E-06	2.101E-06	2.812E-07	1.927E-03	2.285E-02	5.279E-03	
1.000E+00	1.428E-04	1.425E-04	1.413E-04	1.137E-04	9.452E-06	3.389E-02	7.269E-01	5.027E-01	1.571E-02	
1.000E+01	4.284E-04	4.273E-04	3.838E-04	1.452E-04	4.670E-02	1.276E+00	1.958E+00	6.158E-01	9.737E-02	
1.000E+02	7.392E-04	6.935E-04	4.203E-04	4.838E-02	1.368E+00	2.651E+00	2.135E+00	1.266E+00	1.059E+00	
1.000E+03	1.008E-03	7.312E-04	4.882E-02	1.377E+00	2.757E+00	2.837E+00	3.056E+00	3.145E+00	3.129E+00	
1.000E+04	1.046E-03	4.926E-02	1.380E+00	2.769E+00	2.944E+00	3.794E+00	5.108E+00	5.406E+00	5.407E+00	

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE CUVERT DE 0.6 A 0.8
ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA

TABLEAU 2 E



LOG S/S' = -3.0

LOG K'R2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.571E-03	1.573E-03	1.592E-03	1.765E-03	3.217E-03	9.856E-03	2.919E-02	3.661E-02	6.561E-03	
3.162E-01	1.994E-02	2.000E-02	2.058E-02	2.603E-02	6.285E-02	1.978E-01	4.738E-01	3.405E-01	1.339E-02	
1.000E+00	6.594E-02	6.640E-02	7.099E-02	1.107E-01	3.159E-01	9.637E-01	1.593E+00	6.466E-01	1.386E-02	
3.162E+00	1.289E-01	1.310E-01	1.517E-01	3.023E-01	9.191E-01	2.444E+00	2.696E+00	6.857E-01	1.526E-02	
1.000E+01	1.988E-01	2.067E-01	2.773E-01	6.758E-01	2.053E+00	4.141E+00	3.186E+00	6.920E-01	1.992E-02	
1.000E+02	3.515E-01	4.294E-01	8.832E-01	2.540E+00	5.510E+00	5.924E+00	3.244E+00	7.722E-01	1.078E-01	
1.000E+03	5.759E-01	1.040E+00	2.761E+00	6.026E+00	7.313E+00	5.983E+00	3.368E+00	1.391E+00	1.072E+00	
1.000E+04	1.187E+00	2.921E+00	6.253E+00	7.832E+00	7.372E+00	6.113E+00	4.202E+00	3.227E+00	3.139E+00	

LOG S/S' = -2.5

LOG K'F2/KB2	-7.0					-6.0					-5.0					-4.0					-3.0					-2.0					-1.0					0.0					1.0				
TT/R2S	R A B A T T E M E N T S										R E D U I T S																																		
1.000E-01	1.571E-03					1.573E-03					1.592E-03					1.765E-03					3.217E-03					9.856E-03					2.919E-02					3.661E-02					6.570E-03				
3.162E-01	1.994E-02					2.000E-02					2.058E-02					2.603E-02					6.285E-02					1.978E-01					4.738E-01					3.405E-01					1.363E-02				
1.000E+00	6.594E-02					6.640E-02					7.099E-02					1.107E-01					3.159E-01					9.637E-01					1.593E+00					6.473E-01					1.506E-02				
3.162E+00	1.289E-01					1.310E-01					1.517E-01					3.023E-01					9.191E-01					2.444E+00					2.696E+00					6.904E-01					1.970E-02				
1.000E+01	1.988E-01					2.067E-01					2.773E-01					6.758E-01					2.053E+00					4.141E+00					3.189E+00					7.101E-01					3.659E-02				
1.000E+02	3.515E-01					4.294E-01					8.832E-01					2.540E+00					5.510E+00					5.925E+00					3.273E+00					9.471E-01					3.888E-01				
1.000E+03	5.759E-01					1.040E+00					2.761E+00					6.026E+00					7.314E+00					6.013E+00					3.623E+00					2.192E+00					2.044E+00				
1.000E+04	1.187E+00					2.921E+00					6.253E+00					7.834E+00					7.402E+00					6.379E+00					5.115E+00					4.340E+00					4.269E+00				

LOG S/S' = -2.0

LOG K'R2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.571E-03	1.573E-03	1.592E-03	1.765E-03	3.217E-03	9.856E-03	2.919E-02	3.661E-02	6.599E-03	
3.162E-01	1.994E-02	2.000E-02	2.058E-02	2.603E-02	6.285E-02	1.978E-01	4.738E-01	3.406E-01	1.442E-02	
1.000E+00	6.594E-02	6.640E-02	7.099E-02	1.107E-01	3.159E-01	9.637E-01	1.593E+00	6.494E-01	1.901E-02	
3.162E+00	1.289E-01	1.310E-01	1.517E-01	3.023E-01	9.191E-01	2.444E+00	2.696E+00	7.052E-01	3.566E-02	
1.000E+01	1.988E-01	2.067E-01	2.773E-01	6.758E-01	2.053E+00	4.141E+00	3.192E+00	7.657E-01	1.056E-01	
1.000E+02	3.515E-01	4.294E-01	8.832E-01	2.540E+00	5.510E+00	5.930E+00	3.359E+00	1.383E+00	1.065E+00	
1.000E+03	5.759E-01	1.040E+00	2.761E+00	6.026E+00	7.318E+00	6.104E+00	4.194E+00	3.218E+00	3.130E+00	
1.000E+04	1.187E+00	2.921E+00	6.253E+00	7.838E+00	7.494E+00	6.966E+00	6.188E+00	5.473E+00	5.407E+00	

LOG S/S' = -1.5

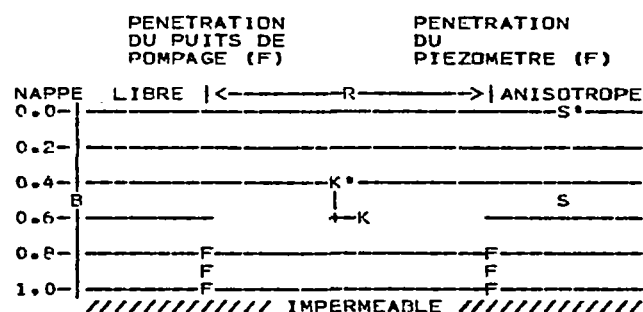
LOG K'R2/KE2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	1.571E-03	1.573E-03	1.592E-03	1.765E-03	3.217E-03	9.856E-03	2.919E-02	3.661E-02	6.687E-03
3.162E-01	1.994E-02	2.000E-02	2.058E-02	2.603E-02	6.285E-02	1.978E-01	4.738E-01	3.407E-01	1.694E-02
1.000E+00	6.594E-02	6.640E-02	7.099E-02	1.107E-01	3.159E-01	9.637E-01	1.593E+00	6.559E-01	3.284E-02
3.162E+00	1.289E-01	1.310E-01	1.517E-01	3.023E-01	9.191E-01	2.444E+00	2.697E+00	7.503E-01	1.004E-01
1.000E+01	1.988E-01	2.067E-01	2.773E-01	6.758E-01	2.053E+00	4.141E+00	3.204E+00	9.258E-01	3.746E-01
1.000E+02	3.515E-01	4.294E-01	8.832E-01	2.540E+00	5.510E+00	5.943E+00	3.596E+00	2.166E+00	2.018E+00
1.000E+03	5.759E-01	1.040E+00	2.761E+00	6.026E+00	7.334E+00	6.351E+00	5.087E+00	4.312E+00	4.242E+00
1.000E+04	1.187E+00	2.921E+00	6.253E+00	7.852E+00	7.749E+00	7.872E+00	7.305E+00	6.611E+00	6.537E+00

LOG S/S' = -1.0

LOG K'F2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.571E-03	1.573E-03	1.592E-03	1.765E-03	3.217E-03	9.856E-03	2.919E-02	3.661E-02	6.936E-03	
3.162E-01	1.994E-02	2.000E-02	2.058E-02	2.603E-02	6.285E-02	1.978E-01	4.738E-01	3.412E-01	2.506E-02	
1.000E+00	6.594E-02	6.641E-02	7.099E-02	1.107E-01	3.159E-01	9.637E-01	1.593E+00	6.757E-01	8.534E-02	
3.162E+00	1.283E-01	1.310E-01	1.517E-01	3.023E-01	9.191E-01	2.444E+00	2.699E+00	8.772E-01	3.425E-01	
1.000E+01	1.968E-01	2.067E-01	2.773E-01	6.758E-01	2.053E+00	4.141E+00	3.241E+00	1.311E+00	9.982E-01	
1.000E+02	3.515E-01	4.294E-01	8.832E-01	2.540E+00	5.510E+00	5.983E+00	4.109E+00	3.135E+00	3.050E+00	
1.000E+03	5.759E-01	1.040E+00	2.761E+00	6.026E+00	7.372E+00	6.930E+00	6.102E+00	5.393E+00	5.333E+00	
1.000E+04	1.187E+00	2.921E+00	6.253E+00	7.892E+00	8.272E+00	8.892E+00	8.382E+00	7.698E+00	7.641E+00	

TABLEAU F F

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG K ¹ R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	1.230E-01	1.229E-01	1.229E-01	1.227E-01	1.211E-01	1.144E-01	9.324E-02	4.643E-02	7.272E-03
3.162E-01	1.560E+00	1.560E+00	1.559E+00	1.554E+00	1.517E+00	1.381E+00	9.711E-01	3.899E-01	1.483E-02
1.000E+00	5.155E+00	5.155E+00	5.150E+00	5.110E+00	4.906E+00	4.224E+00	2.500E+00	7.292E-01	1.534E-02
3.162E+00	1.006E+01	1.006E+01	1.004E+01	9.887E+00	9.270E+00	7.328E+00	3.759E+00	7.723E-01	1.681E-02
1.000E+01	1.548E+01	1.547E+01	1.540E+01	1.501E+01	1.358E+01	9.675E+00	4.303E+00	7.784E-01	2.172E-02
1.000E+02	2.673E+01	2.665E+01	2.620E+01	2.449E+01	1.959E+01	1.169E+01	4.364E+00	8.563E-01	1.121E-01
1.000E+03	3.801E+01	3.754E+01	3.577E+01	3.056E+01	2.164E+01	1.176E+01	4.479E+00	1.458E+00	1.075E+00
1.000E+04	4.892E+01	4.713E+01	4.185E+01	3.261E+01	2.170E+01	1.188E+01	5.274E+00	3.274E+00	3.139E+00

LOG K'R2/KR2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A R A T T E M E N T S					R E D U I T S			
1.000E-01	1.230E-01	1.229E-01	1.229E-01	1.227E-01	1.211E-01	1.144E-01	9.324E-02	4.643E-02	7.280E-03
3.162E-01	1.560E+00	1.560E+00	1.559E+00	1.554E+00	1.517E+00	1.381E+00	9.711E-01	3.899E-01	1.509E-02
1.000E+00	5.155E+00	5.155E+00	5.150E+00	5.110E+00	4.906E+00	4.224E+00	2.500E+00	7.298E-01	1.661E-02
3.162E+00	1.006E+01	1.006E+01	1.004E+01	9.887E+00	9.270E+00	7.328E+00	3.759E+00	7.768E-01	2.149E-02
1.000E+01	1.548E+01	1.547E+01	1.540E+01	1.501E+01	1.358E+01	9.675E+00	4.304E+00	7.960E-01	3.911E-02
1.000E+02	2.673E+01	2.665E+01	2.620E+01	2.449E+01	1.959E+01	1.169E+01	4.390E+00	1.026E+00	3.941E-01
1.000E+03	3.801E+01	3.754E+01	3.577E+01	3.056E+01	2.164E+01	1.178E+01	4.720E+00	2.246E+00	2.045E+00
1.000E+04	4.892E+01	4.713E+01	4.185E+01	3.261E+01	2.173E+01	1.213E+01	6.167E+00	4.383E+00	4.269E+00

LOG K *R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.230E-01	1.229E-01	1.229E-01	1.227E-01	1.211E-01	1.144E-01	9.324E-02	4.644E-02	7.309E-03	
3.162E-01	1.560E+00	1.560E+00	1.559E+00	1.554E+00	1.517E+00	1.381E+00	9.711E-01	3.899E-01	1.592E-02	
1.000E+00	5.155E+00	5.155E+00	5.150E+00	5.110E+00	4.906E+00	4.224E+00	2.500E+00	7.317E-01	2.076E-02	
3.162E+00	1.006E+01	1.006E+01	1.004E+01	9.887E+00	9.270E+00	7.328E+00	3.759E+00	7.910E-01	3.813E-02	
1.000E+01	1.548E+01	1.547E+01	1.540F+01	1.501E+01	1.358E+01	9.675E+00	4.307E+00	8.497E-01	1.098E-01	
1.000E+02	2.673F+01	2.665E+01	2.620E+01	2.449E+01	1.959E+01	1.170E+01	4.477E+00	1.451E+00	1.068F+00	
1.000E+03	3.801E+01	3.754E+01	3.577E+01	3.056E+01	2.164E+01	1.187E+01	5.265E+00	3.265E+00	3.130E+00	
1.000E+04	4.892E+01	4.713E+01	4.185E+01	3.261E+01	2.181E+01	1.269E+01	7.231E+00	5.515E+00	5.407E+00	

LOG K ^{R2/KR2}	-7.0			-6.0			-5.0			-4.0			-3.0			-2.0			-1.0			0.0			1.0		
TT/R2S	R	A	B	A	T	T	E	M	E	N	T	S	R	E	D	U	I	T	S								
1.000E-01	1.230E-01			1.229E-01				1.229E-01			1.227E-01		1.211E-01			1.144E-01			9.324E-02			4.643E-02			7.398E-03		
3.162E-01	1.560E+00			1.560E+00				1.559E+00			1.554E+00		1.517E+00			1.381E+00			9.711E-01			3.901E-01			1.855E-02		
1.000E+00	5.155E+00			5.155E+00				5.150E+00			5.110E+00		4.906E+00			4.224E+00			2.500E+00			7.376E-01			3.518E-02		
3.162E+00	1.006E+01			1.006E+01				1.004E+01			9.887E+00		9.270E+00			7.328E+00			3.760E+00			8.341E-01			1.044E-01		
1.000E+01	1.548E+01			1.547E+01				1.540E+01			1.501E+01		1.358E+01			9.675E+00			4.318E+00			1.005E+00			3.798E-01		
1.000E+02	2.673E+01			2.665E+01				2.620E+01			2.449E+01		1.959E+01			1.171E+01			4.693E+00			2.220E+00			2.019E+00		
1.000E+03	3.801E+01			3.754E+01				3.577E+01			3.056E+01		2.165E+01			1.210E+01			6.139E+00			4.356E+00			4.242E+00		
1.000E+04	4.892E+01			4.713E+01				4.185E+01			3.262E+01		2.205E+01			1.357E+01			8.349E+00			6.653E+00			6.537E+00		

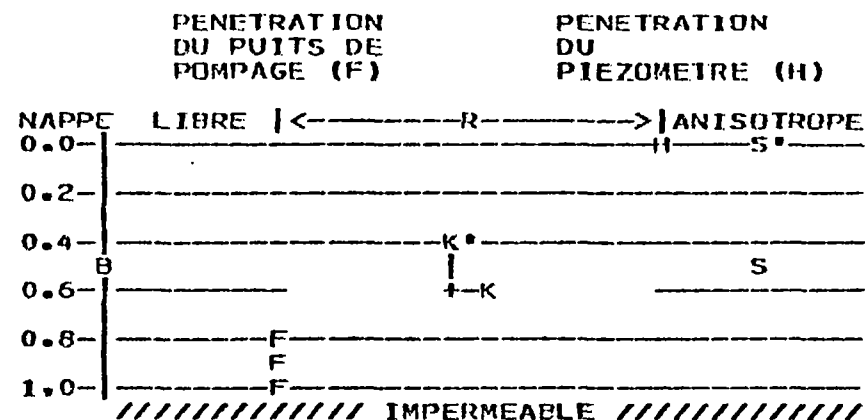
LOG K ^{R2} /KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0
TT/R2S	R A B A T T E M E N T S					R E D U I T S			
1.000E-01	1.230E-01	1.229E-01	1.229E-01	1.227E-01	1.211E-01	1.144E-01	9.324E-02	4.643E-02	7.640E-03
3.162E-01	1.560E+00	1.560E+00	1.559E+00	1.554E+00	1.517E+00	1.381E+00	9.711E-01	3.904E-01	2.700E-02
1.000E+00	5.155E+00	5.155E+00	5.150E+00	5.110E+00	4.906E+00	4.223E+00	2.500E+00	7.552E-01	8.897E-02
3.162E+00	1.006E+01	1.006E+01	1.004E+01	9.887E+00	9.270E+00	7.328E+00	3.760E+00	9.554E-01	3.475E-01
1.000E+01	1.548E+01	1.547E+01	1.540E+01	1.501E+01	1.358E+01	9.675E+00	4.349E+00	1.378E+00	1.001E+00
1.000E+02	2.673E+01	2.665E+01	2.620E+01	2.449E+01	1.959E+01	1.174E+01	5.180E+00	3.181E+00	3.050E+00
1.000E+03	3.801E+01	3.754E+01	3.577E+01	3.056E+01	2.168E+01	1.260E+01	7.146E+00	5.435E+00	5.323E+00
1.000E+04	4.892E+01	4.713E+01	4.185E+01	3.266E+01	2.254E+01	1.458E+01	9.422E+00	7.740E+00	7.641E+00

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.05

TABLEAU F H

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -2.0

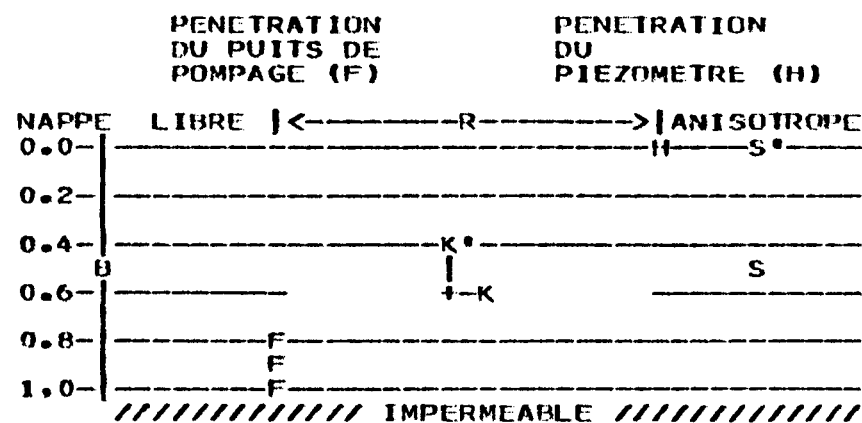
LOG K*R2/KB2	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.657E-05	2.663E-05	2.635E-05	2.389E-05	8.685E-06	0.0	5.756E-08	1.496E-03	6.175E-04	
1.000E+00	1.116E-03	1.108E-03	1.035E-03	5.534E-04	2.550E-05	0.0	2.987E-02	5.935E-02	3.929E-03	
1.000E+01	3.340E-03	3.211E-03	2.307E-03	6.318E-04	2.528E-05	4.209E-02	1.788E-01	1.607E-01	6.525E-02	
1.000E+02	5.635E-03	4.621E-03	2.405E-03	6.314E-04	4.362E-02	2.088E-01	4.271E-01	9.459E-01	1.034E+00	
1.000E+03	7.058E-03	4.722E-03	2.406E-03	4.438E-02	2.123E-01	4.894E-01	1.792E+00	3.009E+00	3.126E+00	
1.000E+04	7.151E-03	4.723E-03	2.406E-03	2.133E-01	4.964E-01	1.952E+00	4.102E+00	5.299E+00	5.407E+00	

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.1

TABEAU F H

ABaque POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELITSOVA



LOG S/S' = -2.0

LOG K'R²/KB² -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

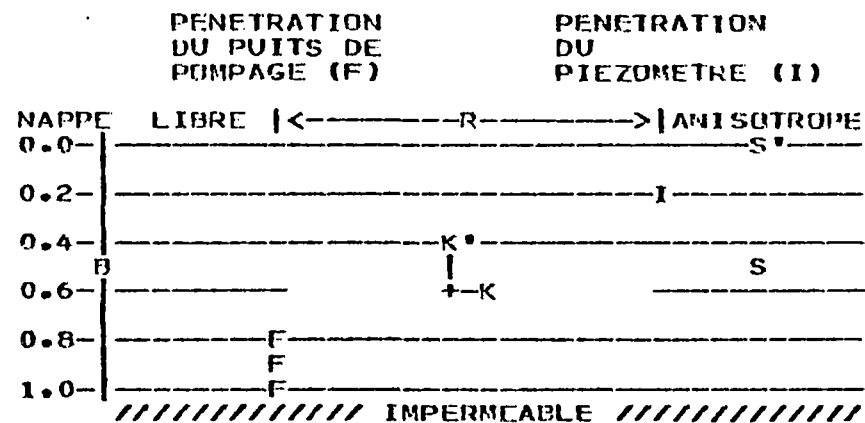
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	5.410E-05	5.439E-05	5.366E-05	4.828E-05	1.645E-05	1.854E-07	0.0	3.047E-03	1.200E-03	
1.000E+00	2.280E-03	2.264E-03	2.112E-03	1.128E-03	5.307E-05	9.941E-07	6.178E-02	1.119E-01	5.431E-03	
1.000E+01	6.822E-03	6.557E-03	4.707E-03	1.294E-03	5.483E-05	8.744E-02	3.366E-01	2.150E-01	6.969E-02	
1.000E+02	1.151E-02	9.435E-03	4.902E-03	1.296E-03	9.067E-02	3.938E-01	5.706E-01	9.814E-01	1.037E+00	
1.000E+03	1.442E-02	9.636E-03	4.903E-03	9.223E-02	4.004E-01	6.549E-01	1.861E+00	3.018E+00	3.126E+00	
1.000E+04	1.462E-02	9.639E-03	4.904E-03	4.025E-01	6.646E-01	2.031E+00	4.132E+00	5.303E+00	5.407E+00	

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.2

TABLEAU F 1

ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE.

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



$\text{LOG } S/S' = -2.0$

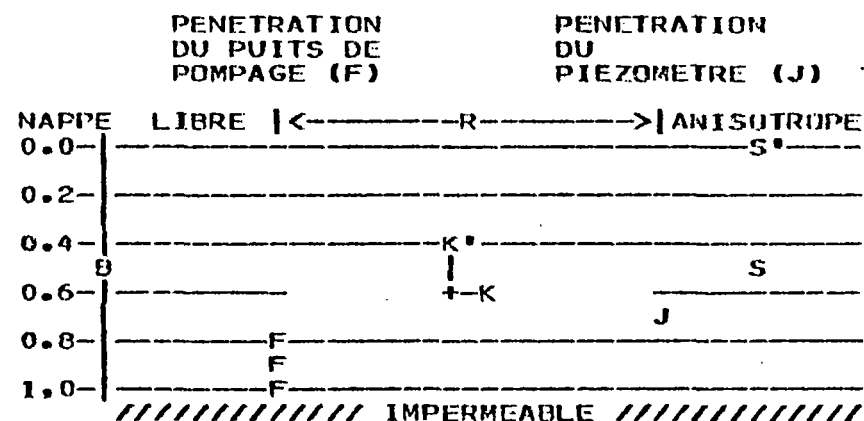
$\text{LOG } K^*R^2/KR^2$ -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S R A B A T T E M E N T S R E D U I T S

1.000E-01	1.169E-04	1.169E-04	1.148E-04	1.029E-04	3.401E-05	2.394E-07	1.047E-06	6.551E-03	2.334E-03
1.000E+00	4.895E-03	4.861E-03	4.533E-03	2.416E-03	1.068E-04	4.473E-06	1.413E-01	2.160E-01	8.334E-03
1.000E+01	1.465E-02	1.408E-02	1.009E-02	2.760E-03	1.132E-04	2.039E-01	6.671E-01	3.221E-01	7.794E-02
1.000E+02	2.471E-02	2.024E-02	1.050E-02	2.767E-03	2.119E-01	7.890E-01	8.786E-01	1.053E+00	1.044E+00
1.000E+03	3.095E-02	2.065E-02	1.050E-02	2.153E-01	8.034E-01	1.020E+00	2.042E+00	3.040E+00	3.127E+00
1.000E+04	3.137E-02	2.065E-02	1.050E-02	8.078E-01	1.037E+00	2.251E+00	4.244E+00	5.318E+00	5.407E+00

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.7
 ABAQUE POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,
 DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELITSOVA

TABLEAU F J



LOG S/S' = -2.0

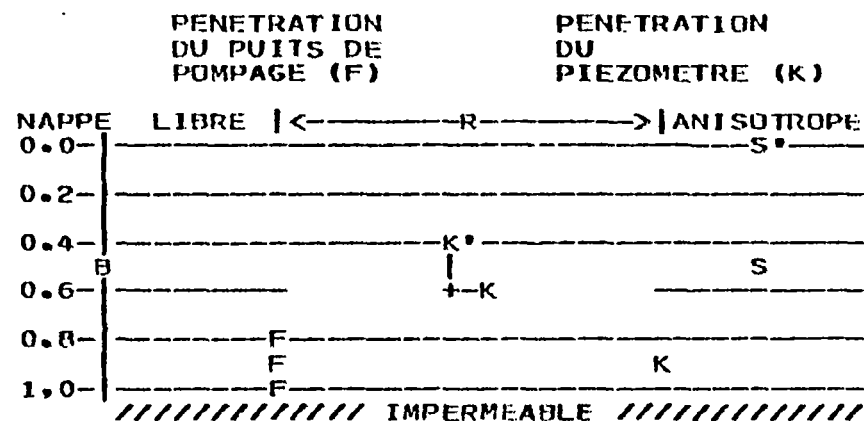
LOG K'R ² /K ²	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	0.0	1.0	
TT/R ² S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	2.429E-03	2.426E-03	2.394E-03	2.135E-03	6.601E-04	8.368E-04	2.628E-02	3.670E-02	6.626E-03	
1.000E+00	1.018E-01	1.011E-01	9.415E-02	4.897E-02	1.449E-02	7.415E-01	1.585E+00	6.521E-01	1.908E-02	
1.000E+01	3.046E-01	2.925E-01	2.077E-01	7.165E-02	1.224E+00	3.888E+00	3.191E+00	7.684E-01	1.058E-01	
1.000E+02	5.136E-01	4.185E-01	2.319E-01	1.349E+00	4.643E+00	5.684E+00	3.358E+00	1.385E+00	1.065E+00	
1.000E+03	6.410E-01	4.429E-01	1.516E+00	4.797E+00	6.460E+00	5.858E+00	4.191E+00	3.220E+00	3.130E+00	
1.000E+04	6.654E-01	1.730E+00	4.971E+00	6.617E+00	6.635E+00	6.718E+00	6.184E+00	5.474E+00	5.407E+00	

PUITS CREPINE DE 0.8 A 1. ET PIEZOMETRE PONCTUEL A LA PROFONDEUR 0.9

TABLEAU F K

ABaque POUR L'INTERPRETATION DE POMPAGES EN NAPPE LIBRE ANISOTROPE,

DANS L'HYPOTHESE DE NEUMAN, SELON FORMULES DE BOULTON - STRELTSOVA



LOG S/S' = -2.0

LOG K'R2/KB2 -7.0 -6.0 -5.0 -4.0 -3.0 -2.0 -1.0 0.0 1.0

TT/R2S	R A B A T T E M E N T S					R E D U I T S				
1.000E-01	1.203E-01	1.203E-01	1.204E-01	1.208E-01	1.233E-01	1.234E-01	9.692E-02	4.701E-02	7.340E-03	
1.000E+00	5.045E+00	5.046E+00	5.058E+00	5.135E+00	5.205E+00	4.462E+00	2.545E+00	7.353E-01	2.084E-02	
1.000E+01	1.515E+01	1.517E+01	1.532E+01	1.557E+01	1.443E+01	1.003E+01	4.360E+00	8.534E-01	1.100E-01	
1.000E+02	2.619E+01	2.635E+01	2.669E+01	2.567E+01	2.057E+01	1.206E+01	4.524E+00	1.454E+00	1.068E+00	
1.000E+03	3.747E+01	3.782E+01	3.688E+01	3.186E+01	2.263E+01	1.223E+01	5.317E+00	3.267E+00	3.130E+00	
1.000E+04	4.896E+01	4.803E+01	4.309E+01	3.392E+01	2.280E+01	1.305E+01	7.282E+00	5.517E+00	5.407E+00	